

11:35:11

## OCA PAD INITIATION - PROJECT HEADER INFORMATION

08/23/88

Active

Project #: E-21-F21  
Center # : R6571-OA0Cost share #:  
Center shr #:Rev #: 0  
OCA file #:  
Work type : RES  
Document : CONT  
Contract entity: GTRCContract#: MDA970-88-C-8145  
Prime #:

Mod #:

Subprojects ? : N  
Main project #:

Project unit:	EE	Unit code: 02.010.118
Project director(s):		
HERTLING D R	EE	
FEENEY R K	EE	
JOY E B	EE	

Sponsor/division names: US DEPT OF DEFENSE  
Sponsor/division codes: 101/ MARYLAND PROCUREMENT OFF  
/ 010

Award period: 880628 to 890627 (performance) 890627 (reports)

Sponsor amount	New this change	Total to date
Contract value	290,666.00	290,666.00
Funded	290,666.00	290,666.00
Cost sharing amount		0.00

Does subcontracting plan apply ? : N

Title: PLANE SURFACE, DIPOLE, PHASED ARRAY COMPUTER AIDED DESIGN AND LAYOUT PROG.



## PROJECT ADMINISTRATION DATA

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894-4820

Sponsor technical contact

Sponsor issuing office

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SAME

Security class (U,C,S,TS) : U  
Defense priority rating : DO-A7  
Equipment title vests with: Sponsor X  
IN ACCORDANCE WITH FAR 52.245-5, ALT 1ONR resident rep. is ACO (Y/N): N  
GOVT supplemental sheet  
GITAdministrative comments -  
PROJECT INITIATION

GEORGIA INSTITUTE OF TECHNOLOGY  
OFFICE OF CONTRACT ADMINISTRATION

NOTICE OF PROJECT CLOSEOUT

Closeout Notice Date 04/30/90

Project No. E-21-F21

Center No. R6571-OA0

Project Director HERTLING, D R

School/Lab EE

Sponsor US DEPT OF DEFENSE/MARYLAND PROCUREMENT OFF

Contract/Grant No. MDA904-88-C-8145

Contract Entity GTRC

Prime Contract No.

Title A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER AIDED DESIGN AND LAYOUT P

Effective Completion Date 890930 (Performance) 890930 (Reports)

Closeout Actions Required:	Y/N	Date Submitted
Final Invoice or Copy of Final Invoice	Y	
Final Report of Inventions and/or Subcontracts	Y	
Government Property Inventory & Related Certificate	Y	
Classified Material Certificate	N	
Release and Assignment	Y	
Other	N	

Comments

Subproject Under Main Project No.

Continues Project No.

Distribution Required:

Project Director	Y
Administrative Network Representative	Y
GTRI Accounting/Grants and Contracts	Y
Procurement/Supply Services	Y
Research Property Management	Y
Research Security Services	N
Reports Coordinator (OCA)	Y
GTRC	Y
Project File	Y
Other	N
	N

NOTE: Final Patent Questionnaire sent to PDPI.



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SR-300

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the periods

7/1/88 - 8/1/88

and

8/2/88 - 9/1/88

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, the project has been initialized and progress has been made on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. This report covers the first two months of the project. Accomplished work includes literature searches and preliminary calculations of antenna self- and mutual-impedances and prototype feed configurations and circuits. Various copper foil tape on mylar transmission line structures are currently being constructed and tested. Currently, an antenna is being designed which will be constructed and tested. The project is on schedule.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on project initialization, literature searches, and preliminary calculations. The project is currently on schedule. We have met with Mr. Joe Zimmerman on two occasions and have reported our efforts and have discussed planned efforts toward completion of the project goals and objectives. Work has been accomplished in two of the three major tasks, the Antenna Design and Analysis Task and the Feed and Filter Design Task. A summary of activity is presented below.

## Antenna Design and Analysis Task

1. A literature search has been conducted to find equations and computation techniques for the calculation of self- and mutual-impedance of dipoles. Three results were obtained.
  - A. The Numerical Electromagnetic Code (NEC) is a computer algorithm which uses the method of moments to solve for the current distributions and self- and mutual-impedances of wire structures, such as dipoles. The code is quite lengthy and thus requires a very large amount of computer time and memory to solve a large array of dipoles.
  - B. Equations were found for the self- (R. W. P. King, Kraus, and others) impedance of circular cylindrical dipoles and the mutual impedance (Howard King) of infinitely thin, parallel, center-fed dipoles. The equations are very lengthy and contain terms which are integrals.
  - C. Simplified equations for infinitely thin, widely spaced, dipoles have also been found. The accuracy of these equations is unknown for the required spacing of approximately one-half wavelength used in this application.
2. The NEC code has been obtained and the key self- and mutual-impedance portions of the code have been extracted. The code has been translated from BASIC to Fortran V computer language. The code has been tested for various dipole



spacings and locations and results are in agreement with the mutual impedance graphs given in the Kraus and Howard King papers.

3. An array analysis methodology has been formulated which uses the power of the method of moments NEC code yet reduces the required computer memory and run time requirements. The array will be composed of identical dipoles: identical in length and identical in diameter (width of tape). The array will be laid out on a regularly spaced rectangular lattice. The self-impedance of the dipoles is calculated with the NEC code assuming they all are equal, thus only one self-impedance is calculated. The mutual impedances between dipoles is calculated between each pairs of dipoles using the NEC code. Since the mutual impedance between any two dipoles in the array which have the same geometrical relationship is the same, the number of calculations and computer storage requirements can be reduced from a number proportional to the square of the number of dipoles to a number proportional to the number of dipoles.
4. Work is underway to develop the array design program which specifies the number of dipoles, the rectangular lattice spacing, the dipole currents, the dipole lengths, and the dipole widths (diameters) required to achieve the desired main beam direction(s) with maximum gain. The program interfaces between the user of the program and outputs information to be used by the feed, matching and filter program and to the array layout program. Several test cases have been designed and are currently being tested against known solutions.

#### Feed and Filter Design Task

1. A literature search has been conducted to find design and analysis equations for various transmission line structures which can be easily constructed with copper foil tape on mylar. Several different sets of equations have been found.
2. Current work includes the construction of transmission lines on mylar and the measurement of their characteristic impedances and velocity factors to check the accuracy of the describing equations.

3. Various feed configurations for the antenna columns are being designed and evaluated. These networks provide the magnitude and phase for the antenna currents for the array.

#### FUTURE PLANS

During the next reporting period, work will continue on the antenna impedance calculations and on the design of the feed networks. More measurements will be made of the characteristic impedance and velocity factor of various copper foil tape on mylar transmission lines. Work on the design, construction, and testing of a prototype antenna will begin.

# EXPENDITURES

## Personal Services

D. R. Hertling, Professor	\$ 10,500
E. B. Joy, Professor	\$ 8,978
R. E. Wilson, Electronic Eng.	\$ 4,867
Michael Guler, Grad. Res. Asst.	\$ 2,160
David Camp, Grad. Res. Asst.	\$ 1,860

Fringe Benefits (25.5% of personal services excluding grad. strudents)	\$ 6,208
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## Materials and Supplies

Copper foil tape	\$ 132
Computer programs	\$ 200

Overhead (60% of direct costs)	\$ 20,943
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Total Expenditures	\$ 55,848
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Remaining funds as of 9/1/88	\$234,818
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E-21-F-21

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

9/1/88 -10/1/88

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. Accomplished work includes progress on the software which calculates antenna self- and mutual-impedances and designs the antenna array. Construction and testing of various copper tape on mylar transmission line structures continued. The project is on schedule.

We have not yet received the government furnished property as per section H.7A of the contract. In particular, we need the computers and plotter to begin testing the software. We will also need the amplifiers as soon as possible to test in prototype antenna arrays.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software and the design and testing of copper foil on mylar transmission line structures. Work has been accomplished in two of the three major tasks, the Antenna Design and Analysis Task and the Feed and Filter Design Task. Some preliminary literature search work has been accomplished on the layout and routing task. The project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. The antenna design and analysis computer program main framework has been completed. The work now centers on development of the following main components.
  1. Array size program.
  2. Array spacing program.
  3. Pointing geometry program.
  4. Element length program.
  5. Element polarization program.
  6. Element width program.
  7. Self-impedance program.
  8. Mutual-impedance program.
  9. Matrix inversion program.
  10. User interface program.
  11. Point source far-field pattern program.
  12. Element pattern program.
  13. Far-field polarization program.
  14. Element excitation program.
  15. Data output program to the feed and filter program and the automated plotting program.

Programs 1-10 are approximately 70% complete and are being tested and packaged. Several versions of the key self- and mutual-impedance programs are being tested against each other.

A simple test case of a broadside array has been designed and will be constructed.



### Feed and Filter Design Task

1. Copper foil on mylar transmission line structures which can be implemented on one side of the mylar and structures which can be implemented on both sides of the mylar have been analyzed. Several of these transmission lines have been constructed and measurements of characteristic impedance and velocity factor have been made.
2. Considerable effort has been spent on evaluation of different feed and filter networks. Various combinations of matching networks and splitter/combiner networks are being considered. Prototype feed and filter networks are currently being designed to be used on a prototype antenna array.

### FUTURE PLANS

During the next reporting period, work will continue on the antenna impedance calculations and on the design of the feed networks. Work on the design, construction, and testing of a prototype antenna will continue.

# EXPENDITURES

## Personal Services

D. R. Hertling, Professor	\$ 5,250
E. B. Joy, Professor	\$ 4,489
R. E. Wilson, Electronic Eng.	\$ 2,496
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. strudents)	\$ 3,120
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## Materials and Supplies

Copper foil tape	\$ 155
Computer programs	\$ 6

Overhead (60% of direct costs)	\$ 10,516
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Total Expenditures	\$ 28,042
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Remaining funds as of 9/1/88	\$234,818
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E-21-F21

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

10/1/88 -10/31/88

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia



## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. Accomplished work includes progress on the software which calculates antenna self- and mutual-impedances and designs the antenna array. In particular, the speed of this program has been greatly increased and the capability to automatically select copper foil widths has been added. Construction and testing of various copper tape on mylar transmission line structures continued. The project is on schedule.

We have not yet received the government furnished property as per section H.7A of the contract. In particular, we need the computers and plotter to begin testing the software. We will also need the amplifiers as soon as possible to test in prototype antenna arrays.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software and the design and testing of copper foil on mylar transmission line structures. Work has been accomplished in two of the three major tasks, the Antenna Design and Analysis Task and the Feed and Filter Design Task. Some preliminary literature search work has been accomplished on the layout and routing task. The project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. The computation time was greatly reduced by taking advantage of the symmetry in the mutual-impedance matrix. There are  $N \times N$  impedance (self and mutual) entries in the impedance matrix for an  $N$  element array. Taking full advantage of the matrix symmetry reduces this number to  $N$  for a rectangularly spaced array of equal sized dipoles, such as ours. For a 25 element array, the number of entries (and associated computation time) decreases from 625 to 25, a factor of 25. Computation time for a 12 element array is now 12 seconds on the campus mainframe and 12 minutes on an IBM-XT.
2. The width of the copper foil tape used to make the dipole antennas is now automatically selected from a list of standard widths.

### Feed and Filter Design Task

1. Copper foil on mylar transmission line structures which can be implemented on one side of the mylar and structures which can be implemented on both sides of the mylar have been analyzed. Several of these transmission lines have been constructed and measurements of characteristic impedance and velocity factor have been made.
2. Considerable effort has been spent on evaluation of different feed and filter networks. Various combinations of matching networks and splitter/combiner networks are being considered. Prototype feed and filter networks are currently being designed to be used on a prototype antenna array.

### FUTURE PLANS

During the next reporting period, work will continue on the antenna impedance calculations and on the design of the feed networks. In particular, the capability to automatically calculate the horizontal and vertical spacings of the array dipoles will be added. Work on the design, construction, and testing of a prototype antenna will continue.

# EXPENDITURES

## Personal Services

E. B. Joy, Professor	\$ 1,901
R. E. Wilson, Electronic Eng.	\$ 2,496
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 1,121
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Materials and Supplies	\$ 360
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Overhead (60% of direct costs)	\$ 4,732
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Total Expenditures	\$ 12,621
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Remaining funds as of 10/30/88	\$194,155
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E21-F21

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

11/1/88 -11/30/88

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. The capability to automatically calculate horizontal and vertical spacings of the array dipoles has been added to the program which calculates the mutual impedances of the array dipoles. A new self- and mutual-impedance algorithm has also been developed. The project is on schedule.

We have not yet received the government furnished property as per section H.7A of the contract. In particular, we need the computers and plotter to begin testing the software. We will also need the amplifiers as soon as possible to test in prototype antenna arrays.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software and the design and testing of copper foil on mylar transmission line structures. Work has been accomplished in all three major tasks. The literature search for routing and placement algorithms has continued. Additional references have been found and evaluated. The project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. The horizontal and vertical spacings of the array dipoles are now automatically determined such that the widest possible spacings are used for maximum gain, but less than that which would produce a grating lobe.
2. A new self- and mutual impedance algorithm has been developed, implemented and partially tested based on the equations of H. E. King. The calculated self- and mutual-impedances of and between parallel and offset dipoles is being tested against data measured by R. W. P. King. This new form has great computational advantages over the MININEC code previously used. Work continues in the testing and in the calculation of the mutual impedance of electrically thick dipoles, such as the dipoles we are using.

### Feed and Filter Design Task

Work continued on the evaluation of feed and filter networks. Additional feed and filter network designs have been considered.

### Routing and Layout Design Task



The literature search for existing layout algorithms continued. One program which uses a simple routing algorithm has been acquired and preliminary testing on an IBM-XT as performed.

#### FUTURE PLANS

During the next reporting period, work will continue on the antenna design software. The ability to tilt the array face in elevation will be added. Calculation and display of azimuth cuts and elevation cuts for the far-field pattern of the array antenna will be added to the program. The accuracy of the new self- and mutual-impedance algorithm will be evaluated. Work on the design, construction, and testing of a prototype antenna will also continue.

# EXPENDITURES

## Personal Services

E. B. Joy, Professor	\$ 1,901
R. E. Wilson, Electronic Eng.	\$ 2,496
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 1,121
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Materials and Supplies	\$ 106
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Overhead (60% of direct costs)	\$ 4,580
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Total Expenditures	\$ 12,214
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Remaining funds as of 12/1/88	\$181,941
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

12/1/88 - 12/31/88

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. In particular, the ability to tilt the array face in elevation has been implemented and azimuth and elevation cuts of the far-field pattern of the array antenna are now calculated and displayed. The new self- and mutual-impedance algorithm has been tested. The project is on schedule.

We have received part of the government furnished property as per section H.7A of the contract. We have received the computer and plotter. We have not yet received the magnetic media for the hard disk or the amplifiers.

On December 14, 1988 we met at Georgia Tech with Joe Zimmerman. During the meeting a review of the project was given and goals for the next month were discussed.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software and the design and testing of copper foil on mylar transmission line structures. The literature search for routing and placement algorithms has continued. Additional references have been found and evaluated. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. The ability to tilt the array face in elevation has been implemented. The user specifies the angular tilt in degrees.
2. Azimuth cuts (for a fixed elevation angle) of the far-field pattern of the array antenna and elevation cuts (for a fixed azimuth angle) of the far-field pattern of the array antenna are now calculated and displayed for horizontally oriented infinitesimal dipole element arrays.
3. The new self- and mutual-impedance algorithm has been tested and found to give accurate results for dipoles with thicknesses over a range of two orders of magnitude, but not as large as needed in the required array. Initial work on representing a single fat wire with 2, 4, or 8 slender wires looks very promising and is being pursued. Accuracy studies are also underway to examine the effect of length to diameter ratio and number of segments on the accuracy of self-impedance determination.

### Feed and Filter Design Task

Work continued on the evaluation of feed and filter networks. Additional feed and filter network designs have been considered.

### Routing and Layout Design Task

The literature search for existing layout algorithms continued. Preliminary considerations of how to interface with the plotter have been considered.

### FUTURE PLANS

During the next reporting period, work will continue on the antenna design software. Work will continue to upgrade the capability of computing and displaying the azimuth and elevation cuts for full length dipoles with arbitrary orientation on the tilted array face.

# EXPENDITURES

## Personal Services

E. B. Joy, Professor	\$ 1,901
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 1,057
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Materials and Supplies	\$ 227
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Computer Software	\$ 680
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Overhead (60% of direct costs)	\$ 4,873
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Total Expenditures	\$ 12,994
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Remaining funds as of 1/1/89	\$168,947
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

1/1/89 -1/31/89

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on all tasks of the project. The self impedance algorithm has been successfully implemented on the personal computer. Accuracy studies have shown the self impedance of dipoles with lengths from 0.3 to 0.5 wavelengths can be accurately computed using our method of moments algorithm. A feed and filter network using only transmission lines and capacitors has been designed. The project is on schedule.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software and the design of feed and filter networks. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. Implementation of the self impedance algorithm on an IBM-XT computer resulted in a numerical problem associated with the small number of significant digits used in such microcomputers. The numerical problem was solved using a closed form equation for the unstable computation. The self impedance algorithm is now running successfully on the microcomputer.
2. Accuracy studies on the self impedance show that the self impedance of dipoles with length in the range of 0.3 to 0.5 wavelengths can be accurately computed using our method of moments algorithm. The accuracy has been compared to R. W. P. King's published data and to the NEC algorithm. Our method of moments algorithm has a great computational speed advantage as compared to the NEC algorithm.
3. Work continues on the calculation of the self impedance of the electrically large diameter dipoles.
4. Work continues on the accuracy of mutual impedance calculation using our method of moments algorithm.

### Feed and Filter Design Task

1. A feed and filter network containing only transmission lines and capacitors has been designed. This network will be much easier to construct than a network containing both inductors and capacitors. Another advantage is lower loss since only high Q capacitors are used. Routing and placement will also be simplified with this feed network.

2. A survey of the various thicknesses of mylar sheets which are readily available has been made. We have also learned that Mylar is available in 10 foot rolls which makes it possible to fabricate many of the antennas without seams.

#### FUTURE PLANS

During the next reporting period, work will continue on the calculation of the self impedance of electrically large diameter dipoles and on improvement of the accuracy of the method of moments algorithm. Further refinement of the design procedures for the feed and filter network will also continue. The first design was performed using manual optimization of the feed network parameters. An optimizer is currently being written to automatically optimize the feed and filter network. An antenna using the first feed and filter network design will be constructed.

## EXPENDITURES

## Personal Services

R. K. Feeney, Professor	\$ 4,493
E. B. Joy, Professor	\$ 2,333
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 2,313
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Materials and Supplies	\$ 0
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Computer Software	\$ 0
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Overhead (60% of direct costs)	\$ 8,037
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Total Expenditures	\$ 21,432
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Remaining funds as of 2/1/89	\$147,515
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

3/1/89 -3/31/89

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on all tasks of the project. The method of moments algorithm is now running on the government furnished PC and several improvements to the algorithm have been made to improve accuracy. A new technique for the numerical evaluation of mutual impedance has been developed which does not require the use of a load impedance on one of the two dipoles. A program which deterministically designs matching networks rather than using an optimizer has been written. Work on the layout and plotting task has also been accomplished. The project is on schedule.

## TASK STATUS

During the period covered by this report, efforts have concentrated on the refinement of the antenna design software and the design of feed and filter networks. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. Several of the sine and cosine integral routines and associated approximate series have been modified to obtain the desired accuracy using 16 bit words (word length of the PC).
2. Accuracy studies have been successfully carried out to verify the PC version accuracy.
3. Accuracy studies of the self impedance determinations as compared to measured data of R. W. P. King show that high accuracy is obtained for the following lengths and radii of dipole antennas:

Length:	0.3 to 0.5 wavelengths
Radius:	0.000001 to 0.01 wavelengths

These accuracies are obtained using six segments per dipole. These ranges are of importance and are used in this project.

4. A new technique for the numerical evaluation of mutual impedance has been developed which does not require the use of a load impedance on one of the two dipoles. This load impedance must be set to a very large value and is a source of some numerical instability. Without the need for this load impedance numerical results are shown to be highly stable. The effect of dipole thickness can now be more easily calculated using the new formulation.



### Feed and Filter Design Task

1. It was found that the feed and filter network containing only transmission lines and capacitors would not work for all antenna impedances and electrical line lengths. A computer program which deterministically designs matching and phasing networks for the dipole antennas has been written.
2. The construction of lumped capacitors and inductors using the copper foil tape are being developed. Both series and shunt capacitors and inductors will be needed in general. Methods of interfacing the feed and filter design software with the layout and plotting software are being developed.
3. We are also in the process of designing standard T and PI networks using copper foil tape on MYLAR. Once these have been designed, any T and PI network needed can be easily realized.

### FUTURE PLANS

During the next reporting period work will continue on all tasks. In particular, work will concentrate on the building and testing antennas. The interfacing of the various computer programs will also begin. That is, the self and mutual impedance algorithm must pass its output to the feed and filter design program which must then pass data on to the routing and layout program.

## EXPENDITURES

## Personal Services

R. K. Feeney, Professor	\$ 4,493
E. B. Joy, Professor	\$ 2,333
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 2,313
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Materials and Supplies	\$ 0
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Computer Software	\$ 0
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Overhead (60% of direct costs)	\$ 8,037
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Total Expenditures	\$ 21,432
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Remaining funds as of 4/1/89	\$104,651
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

4/1/89 - 4/30/89

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

### SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task and on the Feed and Filter Design Task. Work was also accomplished on the Routing and Layout Design Task. In particular, improvements have been made to the software which calculates antenna impedances and to the software which designs the feed and filter networks. The project is on schedule.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software, the feed and filter design software and on the interfacing of the these programs. The feed and filter design program has been improved and its results checked with a circuit simulator to verify that the feed and filter networks are correct. The writing of the routing and placement software has begun. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. An error in the computation of the dipole length was corrected. This occurred if the dipole tilt put the end of the dipole in any quadrant except quadrant one.
2. The wording of the prompt for dipole tilt was changed to include a description of what the program considers positive. A positive dipole tilt angle is considered to be in a counter-clockwise direction when looking in the same direction as the array.
3. The prompt for location of the filter network was changed so that it is dependant on the dipole tilt angle. For

$$0^{\circ} < \text{Dipole Tilt} < 45^{\circ}$$

only left or right are allowed positions. For

$$45^{\circ} \leq \text{Dopole tilt} < 90^{\circ}$$

only top or bottom are allowed positions. Here the angle supplied by the user has been adjusted so that dipole tilt is between  $0^{\circ}$  and  $90^{\circ}$ .

4. It is possible that the desired combination of frequency and panel size will result in more elements being required than can be handled by the program. The error handling for this condition was changed so that the user is apprised of the situation and asked to specify a smaller panel size. Previously, the program generated an error message and aborted.
5. The computation of the driving point impedances was modified so that it is necessary to store only one row/column of the system impedance matrix. This makes it possible to allow the design of up to 20 x 20 element array including a ground plane on the PC.

#### Feed and Filter Design Task

1. Work continued on the program which deterministically designs the antenna feed networks. This program accepts data from the self and mutual impedances and then designs the antenna feed networks. A circuit simulator was used to verify that the feed networks designed by this program are correct. This program can calculate both balanced T networks and balanced PI networks. Whenever possible, balanced PI network are used since they contain fewer elements and are thus easier to construct.
2. A 491 MHz single column with three dipoles has been constructed. We are currently in the process of making impedance and pattern measurements of this antenna.
3. More work has been accomplished on the practical realization of the various T and PI feed networks. There are a total of 16 (eight T and eight PI) possible feed networks. Work is currently underway to realize each one of these networks using copper foil tape on mylar.

### Routing and Layout Design Task

1. The software which accepts data from both the antenna impedance program and the feed network program has been written and is in the process of being de-bugged. This program will route and plot the feed networks and the antennas.
2. Preliminary work has been accomplished to interface this program to the antenna impedance and the feed and filter design programs.

### FUTURE PLANS

During the next reporting period, work will concentrate on the completion and the interfacing of the the programs. Work will also continue on the construction and testing of antenna arrays.

# EXPENDITURES

## Personal Services

R. K. Feeney, Professor	\$ 4,493
D. R. Hertling	\$ 3,450
E. B. Joy, Professor	\$ 2,519
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930
Joseph Epple, Grad. Res. Asst.	\$ 720

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 3,241
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Materials and Supplies	\$ 0
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Computer Software	\$ 0
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Overhead (60% of direct costs)	\$ 11,207
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Total Expenditures	\$ 29,886
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Remaining funds as of 5/1/89	\$ 74,765
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E-21-F21

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period  
5/1/89 - 5/31/89

Contract Number: MDA970-88-C-8145

Prepared by  
Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

### SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task, on the Feed and Filter Design Task, and on the Routing and Layout Design Task. In particular, improvements have been made to all three programs and to interfacing them. On May 11 and May 12 we met at Georgia Tech with Mr. Joe Zimmerman and Dr. Bob Collier. During their visit, several antennas were designed using the software developed on the project. Bob Collier is currently building and testing several antennas which have been designed with the software. We are also working on developing the capability to etch antennas using conventional printed circuit board techniques.

## TASK STATUS

During the period covered by this report, efforts have been concentrated on the refinement of the antenna design software, the feed and filter design software and on the interfacing of the these programs. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. Handling of a ground plane was added to the program. The user is asked if a ground plane is desired. If a ground plane is desired, the program computes the required spacing between the array panel and the ground plane.
2. If a ground plane is requested, the user is also asked for the value of the dielectric constant for the spacer material. This is used in the computation of the spacing between the array panel and the ground plane.
3. The list of standard tape widths used in determining the dipole width was changed to readily available, off the shelf values. The current tape widths used by the program are 0.125", 0.25", 0.375", 0.5", 0.75", and 1.0" .
4. Interface routines were added to prompt for the dielectric constant and thickness of the Mylar, and to write the design parameters to disk. This disk file is used by the Feed and Filter Network and Routing and Placement programs.
5. "Please Wait" messages were added during the computation of the driving point impedances and the generation of pattern plots to assure the user that the program is executing and has not "locked up". Also, if plots are to be sent to the HP plotter, the program prompts the user to load paper and waits for user confirmation.

### Feed and Filter Design Task

1. The Feed and Filter design program now automatically reads data from the file generated by the Antenna Design and Analysis program and designs the feed networks for all dipoles.
2. Impedance measurements on the 491 MHz single column with three dipoles have been made. These impedances differ from the predicted values and we are currently in the process of resolving the discrepancy.
3. More work has been accomplished on the practical realization of the various T and PI feed networks. All of the basic networks have been laid out. Work is currently underway to measure the various series and shunt inductors and capacitors required for the networks.
4. Work has been accomplished on the interfacing of the Feed and Filter design program to the Placement and Routing program.

### Routing and Layout Design Task

1. The capability has been added to meander the transmission lines in order to change their physical lengths. This provides the capability to set the electrical length between dipoles.
2. We have begun to incorporate the various T and PI networks into the Routing and Layout program.

### FUTURE PLANS

During the next reporting period, work will concentrate on the completion and the interfacing of the the programs. Work will also continue on the construction and testing of antenna arrays. We will also continue to design antennas specified by Joe Zimmerman.

# EXPENDITURES

## Personal Services

R. K. Feeney, Professor	\$ 4,493
D. R. Hertling	\$ 3,450
E. B. Joy, Professor	\$ 2,519
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930
Joseph Epple, Grad. Res. Asst.	\$ 720

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 3,241
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Materials and Supplies	\$ 0
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Computer Software	\$ 0
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Overhead (60% of direct costs)	\$ 11,207
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Total Expenditures	\$ 29,886
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Remaining funds as of 6/1/89	\$ 44,879
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period  
6/1/89 - 6/30/89

Contract Number: MDA970-88-C-8145

Prepared by  
Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task, on the Feed and Filter Design Task, and on the Routing and Layout Design Task. In particular, improvements have been made to all three programs and to interfacing them. Several antennas have been built and tested. Additionally, we have been working with Dr. Bob Collier who has been building and testing antennas. Additional work on developing the capability to etch antennas using conventional printed circuit board techniques has been accomplished. Mr. Joe Zimmerman, Dr. Bob Collier, and Mr. Richard Wilson visited Buckbee Mears in St. Paul, MN on 8 June to discuss the fabrication of etched antennas on microwave substrate PC board material.

Problems with the lossy adhesive on the copper foil tape were identified and copper foil tape with a low loss adhesive has been obtained. It has also been found that the loss of Mylar is significant in the UHF range. Identification of these problems caused delays in antenna fabrication and testing and a no-cost extension (1 Sep 89) of the contract was requested.

## TASK STATUS

During the period covered by this report, efforts have concentrated on the refinement of the antenna design software, the feed and filter design software, the routing and placement software and on the interfacing of these programs. In particular, considerable progress has been made on the routing and antenna layout software. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. An error was found in our method of computing the mutual impedances in the system impedance matrix. The error occurred only when the dipoles were tilted (i.e. when the dipoles were not horizontal or vertical). This error was corrected without a major impact on the computation time or on the maximum size of the array which can be accommodated. The program can still handle a 20 x 20 element array.
2. Since, in the future, the array panel may be something other than Mylar, references to Mylar in the program prompts were changed to "substrate".
3. In addition to the required distance to the ground plane computed by the program, the output printout now includes the value of the spacer dielectric constant which is used in that computation and specified by the user.
4. Drafts of the user's manual for DIPARA were written.
5. The program now writes the data required by the feed and filter design and the routing and layout programs to the current default drive rather than to the A: drive. This facilitates running all three programs from a batch file.
6. A batch file was written to run the array design program, the feed and filter design program, and the routing and layout program with one command from the command line. The batch file method has been tested and works.



### Feed and Filter Design Task

1. The feed and filter design program now automatically reads data from the file generated by the antenna design and analysis program and writes to a file to be read by the routing and layout program.
2. The discrepancies in the impedance measurements on the 491 MHz single column with three dipoles have been traced to the loss in the copper foil tape adhesive and in the Mylar. The transmission lines which used the adhesive and the Mylar as a dielectric were replaced with coplanar strip transmission lines and the impedance measurements remade. These impedances agreed much better with the predicted values. The column impedance was approximately  $75 + j30$  ohms at 491 MHz and was  $50 + j0$  ohms at 508 MHz.
3. Pattern measurements on the 491 MHz column antenna were made. The measured pattern agreed fairly well with the predicted values. The nulls in the pattern and sidelobes were approximately at the correct angles but were not the correct levels. We are currently making additional measurements with this antenna.
4. We are currently measuring various series and shunt inductors and capacitors required for the feed networks networks. These measurements are being made on several substrate materials including Mylar, teflon-glass, and epoxy glass. This data on the capacitors and inductors is needed by the routing and placement program.
5. Work has been accomplished on the interfacing of the feed and filter design program to the routing and placement program.

### Routing and Layout Design Task

1. The routing and layout program can now plot the dipole array and the antenna feed networks. Additional work needs to be accomplished so that the capacitors and inductors for all the possible feed networks can be automatically plotted.

2. The routing and layout program has been interfaced to the feed and filter design program.

#### FUTURE PLANS

During the next reporting period, work will concentrate on the completion of the software and its documentation. Work will also continue on the construction and testing of antenna arrays. In particular, both copper foil on Mylar and etched antennas on teflon-glass PC board will be built and tested. We will also continue to design antennas specified by Mr. Joe Zimmerman and will continue to send antenna designs to Dr. Bob Collier.

## EXPENDITURES

### Personal Services

R. K. Feeney, Professor	\$ 4,493
D. R. Hertling	\$ 3,450
E. B. Joy, Professor	\$ 2,519
R. E. Wilson, Electronic Eng.	\$ 2,246
Michael Guler, Grad. Res. Asst.	\$ 1,080
David Camp, Grad. Res. Asst.	\$ 930
Joseph Epple, Grad. Res. Asst.	\$ 720

Fringe Benefits (25.5% of personal services excluding grad. students)	\$ 3,241
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Materials and Supplies	\$ 26
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Travel	\$ 850
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Overhead (60% of direct costs)	\$ 11,733
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Total Expenditures	\$ 31,288
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Remaining funds as of 7/1/89	\$ 13,591
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E-21-F21

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

7/1/89 - 7/31/89

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

## SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task, on the Feed and Filter Design Task, and on the Routing and Layout Design Task. In particular, significant improvements have been made to the layout and routing program and to the interfacing of the three major programs. Several antennas have been built and tested. We have continued to work with Dr. Bob Collier who has been building and testing antennas.

On July 20 and 21, Mr. Joe Zimmerman, Ms. Leslie Mathias, and Mr. Bob Geissler visited Georgia Tech for an project review. We discussed the remainder of the project delivered the two element 1990 MHz antenna to them. Subsequent testing of the antenna showed it to agree very well with theoretical predictions.

## TASK STATUS

During the period covered by this report, efforts have concentrated on the refinement of the antenna design software, the feed and filter design software, the routing and placement software and on the interfacing of these programs. In particular, considerable progress has been made on the routing and antenna layout software. Work has been accomplished in all of the three major tasks and the project is currently on schedule. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. The programs were demonstrated to Joe Zimmerman, Leslie Mathias, and Bob Geissler who had several suggestions for changes to the program DIPARA. The following are their recommended changes.
  - a) Re-ordering of the units in the units prompt at the beginning of the program.
  - b) Changing the response to the units prompt from letters to numbers.
  - c) Changing the input routines so that a typing mistake would not abort the program.
  - d) Staggering the plotting of the array so that they would not overwrite each other.
  - e) Changing the prompt for the beam position to more clearly indicate to the user that the azimuth angle and the elevation angle are required and in what order.
  - f) Changing the informative message displayed while the pattern cuts are being computed so that the user is not mislead into thinking that the plotter should be doing something when, in fact, it should not.
2. Low level formatting, partitioning, and formatting of a blank Q-pak was demonstrated. The array design programs and required utilities were loaded onto the freshly formatted Q-pak and several designs were performed using that Q-pak as the boot disk.

3. Something happened to the Q-pak referred to in 2) after being transported to Bendix and it would not initialize. Bob Collier sent another blank Q-pak which was formatted and loaded with the required programs and utilities. This disk was duplicated using a Q-pak which was already at Georgia Tech and both were returned to Bendix.
4. A batch file was written which automatically handles low level formatting and partitioning of a Q-pak. This will facilitate the process of setting up new disk packs in the future.

#### Feed and Filter Design Task

1. The feed and filter design program has been used to design several antennas. Work has continued on its interfacing to the other programs.
2. The 491 MHz single column with three dipoles was sent to Bendix where its impedance was measured. This was the antenna for which we had to remake the transmission lines because of the lossy coplanar strip lines. The measured input impedance was  $112 + j6.8$  ohms with an SWR of 2.24. They also measured the antenna at 451 and 530 MHz where the SWR dipped and got 1.074 and 1.615, respectively. We had measured the antenna impedance to be approximately  $75 + j30$  ohms at 491 MHz and  $50 + j0$  ohms at 508 MHz. Our measurement was not made on a proper range and the antenna impedance was influenced by surrounding objects. The Bendix measurement was made under better conditions and is, therefore, more accurate.
3. Gain measurements on the 491 MHz column antenna were also made at Bendix. The measured pattern agreed fairly well with the predicted values.
4. Considerable progress has been made on characterizing inductors and capacitors required for the feed networks. Measurements are being made on several substrate materials including Mylar, teflon-glass, and epoxy glass. From this data, the routing and placement program calculates the physical dimensions of the required capacitors and inductors.

### Routing and Layout Design Task

1. The routing and layout program can now plot the dipole array and the antenna feed networks. It has also been modified to plot on different layers to facilitate antenna construction on both Mylar substrates or for etched circuit board construction.
2. The routing and layout program has been made more user friendly.

### FUTURE PLANS

During the next reporting period, work will concentrate on the completion of the software and its documentation. Work will also continue on the construction and testing of antenna arrays. In particular, both copper foil on Mylar and etched antennas on teflon-glass PC board will be built and tested. The placement and routing program will be modified to plot antennas too large for one plot on multiple plots to be pieced together. We will also continue to design antennas specified by Mr. Joe Zimmerman and will continue to send antenna designs to Dr. Bob Collier.



# EXPENDITURES

## Personal Services

R. E. Wilson, Electronic Eng.	\$ 2,381
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Fringe Benefits (26.3% of personal services excluding grad. students)	\$ 626
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Materials and Supplies	\$ 846
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Overhead (62.5% of direct costs)	\$ 2,408
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Total Expenditures	\$ 6,261
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Remaining funds as of 8/1/89	\$ 7,330
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A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period  
8/1/89 - 8/31/89

Contract Number: MDA970-88-C-8145

Prepared by  
Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

### SUMMARY

During the reporting period, progress has continued on the Antenna Design and Analysis Task, on the Feed and Filter Design Task, and on the Routing and Layout Design Task. In particular, significant improvements have been made to the layout and routing program and to the interfacing of the three major programs. Several antennas have been built and tested. We have continued to work with Dr. Bob Collier who has been building and testing antennas. A delay in the work was caused by an equipment failure on our HP-8510 network analyzer.

## TASK STATUS

During the period covered by this report, efforts have concentrated on the refinement of the antenna design software, the feed and filter design software, the routing and placement software and on the interfacing of these programs. In particular, considerable progress has been made on the routing and antenna layout software. Work has been accomplished in all of the three major tasks and the project is currently on schedule for completion by 1 October. A summary of activity is presented below.

### Antenna Design and Analysis Task

1. A routine was added which improves the prompting for the name of the file to contain the design summary. The routine first checks the command line for the name. If the name is not found there, it prompts the user for the name. This capability was previously provided by the FORTRAN library routines, but the prompt was not very informative - except to the programmer. In addition, the new routine checks for the existence of the specified file. The program informs the user if a file already exists and asks for permission to overwrite the file. This provides some protection from inadvertently destroying an important file.
2. The writing of the design summary was moved from the main program to a subroutine to improve the modularity of the program.
3. Code was added to allow the user to check his inputs before the program continues with the design. If the displayed values for the inputs are not correct, the user can re-enter the inputs until satisfied with them.

### Feed and Filter Design Task

1. The feed and filter design program was modified to automatically change the phase shift of the matching networks to yield more easily realizable networks.

2. Work on the characterization of the feed networks was interrupted due to an equipment failure of the HP 8510 network analyzer. The analyzer had to be shipped to Texas for repair.

#### Routing and Layout Design Task

1. The routing and layout software was modified to draw meander lines with smooth corners. This facilitates the construction of etched antennas.
2. The software which plots the layouts for the matching networks was added to the program. Finishing the coding of the networks depends on network analyzer measurements.
3. Several minor software bugs were found and corrected.

#### FUTURE PLANS

During the next reporting period, work will concentrate on the completion of the software and its documentation. The remaining deliverable antennas will be built and sent to Bendix for testing. The placement and routing program will be modified to plot antennas too large for one plot on multiple plots to be pieced together.

EXPENDITURES

Personal Services

R. E. Wilson, Electronic Eng. \$ 2,381

Fringe Benefits (26.3% of personal  
services excluding  
grad. students) \$ 626

Materials and Supplies \$ 0

Overhead (62.5% of direct costs) \$ 1,879

Total Expenditures \$ 4,886

Remaining funds as of 9/1/89 \$ 2,444

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

Monthly Status Report

For the period

9/1/89 - 9/30/89

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

#### SUMMARY

During the reporting period, work has concentrated on finishing the three tasks and completing the project. Several small software changes and corrections have been made. The measurements needed to finish the feed networks have been completed. The project has been completed.



## TASK STATUS

During the period covered by this report, efforts have concentrated on de-bugging and finishing the antenna design software, the feed and filter design software. The three tasks have been completed.

### Antenna Design and Analysis Task

1. During Mr. Joe Zimmerman's visit on September 14 - 15, several changes were made to the program prompts at his request.
  - a) The prompt for the dipole tilt was improved by mentioning **polarity**, indicating the reason for tilting the dipoles was to adjust polarization.
  - b) Since polystyrene is a commonly used spacer material between the array panel and a ground plane, the dielectric constant for polystyrene is now included in the prompt for the dielectric constant of the spacer material.
  - c) Two common materials used for the array substrate are Teflon glass and Mylar. For the user's convenience, the dielectric constants of these two materials are included in the prompt for the substrate dielectric constant.
2. The user's guide has been updated to include these changes and those described in the July 1989 monthly report. Joe Zimmerman was given a copy of the new user's guide so that he could photocopy it and distribute it during his demonstration of the program.
3. The new versions of the programs were put on two new Q-paks supplied by Joe Zimmerman. DOS and the necessary utilities were also loaded and the Q-paks were made to be able to boot the computer.

### Feed and Filter Design Task

1. The final necessary measurements for the completion of the feed networks were made using the network analyzer.

### Routing and Layout Design Task

1. The routing and layout software was modified to draw large antennas in several smaller pieces which can be assembled. A smaller scaled drawing is also provided to assist in the assemble of the pieces into the total antenna.
2. The routing and layout software was modified to be made more user-friendly. In particular, either manual or auto-scaling of the plots can now be selected by the user.
3. Software bugs found by Joe Zimmerman in the plotting software were found and corrected.

EXPENDITURES

Personal Services

R. E. Wilson, Electronic Eng.	\$ 1,191
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Fringe Benefits (26.3% of personal services excluding grad. students)	\$ 313
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Materials and Supplies	\$ 0
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Overhead (62.5% of direct costs)	\$ 940
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Total Expenditures	\$ 2,444
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Remaining funds as of 10/1/89	\$ 0
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E-21-F21

DIPARA: a strip dipole array design program

User's Guide

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## Introduction

**DIPARA** is a strip dipole array design program. The user inputs the source frequency, main beam directions, array panel tilt, dipole tilt, location of a filter network, ground plane information, size of the array panel, and panel substrate dielectric constant and thickness. From this information the program determines the number of dipoles, their locations, and the driving point currents required to produce the desired beam direction. Also, the driving point impedances are determined for use in design of the matching and filter networks.

This user's manual describes how to run the program. To this end the reader is taken step by step through an example design.

### Running the Program: an example design

The example design is for a single beam antenna with the beam broadside to the array. The frequency of operation will be 491 MHz which is the frequency of TV channel 17.

To start the program type:

**DIPARA [File\_Name]**

at the DOS command prompt. **File\_Name** is the name of a file to receive the programs output summarizing the design. **File\_Name** is optional, the program will prompt for a file name if it is missing. It can be any valid DOS file name, including the reserved names **PRN** (output will go to the standard printer), **CON** (output will go to the console), or **NUL** (output is discarded). As with any alphanumeric input to the program, case is not important. The program will accept either upper or lower case.

### Program Input

#### Units for Linear Dimensions

The first request the program makes is for the units the user wants to use for linear dimensions. The prompt is shown in Figure 1. The program can handle units of **inches**, **feet**, **centimeters**, or **meters**. As described in the prompt, one of these is selected by typing **0**, **1**, **2**, or **3**, respectively. The program will only accept these four entries. If anything else is input an error message will be displayed and the user will be asked to try again. As shown in Figure 1, for this example **inches** will be used.

#### Source Frequency

Next the program requests the source frequency. This should be

Please specify the units you want to use for the array size and element position from one of the following:

- 0 - inches,
- 1 - feet,
- 2 - centimeters,
- 3 - meters.

Make your selection by entering the number corresponding to your choice.

I want to use: 0

**Figure 1 Prompt for units**

Enter the desired source frequency (in GHz): .491

**Figure 2 Prompt for Source Frequency**

specified in GHz, as indicated in the prompt shown in Figure 2. For this example the desired source frequency is .491 GHz (491 MHz).

### **Beam Locations**

The program next asks for the number of beams and their locations as shown in Figure 3.

When prompted enter the desired number of beams, and the AZIMUTH and ELEVATION angle (in degrees) for each beam.

Enter desired number of beams (1-3): 1  
Enter desired position of beam #1 (AZ, EL): 0. 0.

**Figure 3 Prompt for number of beams and their locations**

As indicated in the prompt for the number of beams, at least one beam is required and no more than three is allowed. If the number of beams is not in this range an error message is displayed and the user is asked to try again.

The beam locations are entered as azimuth and elevation angles in degrees. 0° azimuth, 0° elevation is perpendicular to the array panel, assuming no panel tilt (see below). Positive azimuth is clockwise (to your right) when looking in the direction of the beam. A positive elevation angle is up. These definitions correspond to those used in surveying. Although, there are no traps in the program to prevent you from doing so, it does not make sense to specify an azimuth or elevation angle outside the range  $\pm 90^\circ$ . The program will not allow overlapping main beam directions and will display an error message if this is attempted.



When entering the position of each beam the azimuth angle should be entered first, then the elevation angle. The user is reminded of this by the **AZ**, **EL** symbols shown in parenthesis in the prompt. The numbers may be entered both on the same line (without an intervening carriage return) or on separate lines. If the entries are on the same line separate them with a space or a comma. If a carriage return does separate the entries no additional prompts, indicating that an incomplete beam position has been entered, will be output by the program.

As shown in the figure, the beam is to be pointed perpendicular to the panel for the example design.

### Panel Tilt

The array panel can be tilted in elevation. As shown in Figure 4,

The panel containing the array may be tilted in elevation. At the prompt specify the desired panel tilt by entering the elevation angle of the panel normal.

Enter desired panel tilt (in degrees): 0.

Figure 4 Prompt for Panel Tilt

the program next asks for the desired panel tilt. This is specified by entering the elevation angle of the panel **normal** in degrees. As with the beam elevation angle, a positive panel tilt is up. A zero degree panel tilt is chosen for the example design. The array panel is, thus, vertical.

### Dipole Polarization

The polarization of the array is the next parameter requested as shown in Figure 5.

The dipoles making up the array can be tilted in the aperture. At the prompt enter the desired dipole tilt angle. The angle should be specified in degrees measured from the vertical. The dipoles will be vertical for a 0 degree tilt angle and horizontal for a 90 degree tilt angle. A positive tilt angle is assumed to be in a COUNTER-CLOCKWISE direction when looking in the same direction as the array.

Enter the desired dipole tilt (polarity): 90.

Figure 5 Prompt for array polarization

The polarization is specified by entering the dipole tilt angle in degrees. This tilt angle is in the plane of the panel. As indicated in the figure, the tilt angle is measured from vertical. That is, the dipoles will be vertical for a dipole tilt of 0° and horizontal for a dipole tilt of 90°. Both positive and negative tilt angles are allowed. A positive tilt angle is assumed to be in



- a **counter-clockwise** direction when looking in the same direction as the array. For the example design, the tilt angle is specified as 90°; the dipoles will be horizontal.

### The Filter Network

To allow for removal of signals which are off frequency, a filter network can be placed on the array panel. The desired location of

```
Space must be left for the filter network along the
      (T)op edge, or
      (B)ottom edge
of the array panel. Indicate your choice by typing the corresponding letter
shown in parenthesis. I want: B
```

**Figure 6 Prompt for Location of Filter Network**

the filter network is asked for next, as shown in Figure 6. The prompt for the filter network location is dependent upon the requested dipole tilt angle. For

$$45^\circ \leq \text{DipTilt} < 90^\circ$$

the prompt is as shown in the figure. For

$$0^\circ < \text{DipTilt} < 45^\circ$$

(L)eft edge and (R)ight edge would replace (T)op edge and (B)ottom edge respectively. Here the angle supplied by the user has been adjusted so that **DipTilt** is between 0° and 90°.

The desired location is chosen by entering the letter shown in the parenthesis as indicated in the prompt. More than one letter may be typed but only the first letter is used. The program only accepts T, B, L, or R, ignoring case. Any other letters will result in an error message and a request to try again.

The filter network is to be placed along the bottom edge for the example design.

### Ground Plane Information

The program next asks if a ground plane is desired, as shown in Figure 7.

Do you want to use a ground plane (y or n)? Y

Please enter the dielectric constant of the SPACER material  
between the array substrate and ground plane  
(typically 1.033 for polystyrene): 1.033

**Figure 7 Prompt for Ground Plane Information**

As indicated in the prompt, enter either Y or N (again, case is ignored) in response to the prompt.

Responding with Y indicates that a ground plane is desired. The program will then ask for the dielectric constant of the material between the array panel and the ground plane. This value is used to compute the physical distance to the ground plane needed to build the array. This distance is recorded in the output file. Typical dielectric constants are less than 2.0 but no validation of the entered value is performed. For the user's convenience, the program lists the measured dielectric constant for polystyrene, a common spacer material.

For the example design polystyrene was chosen for the spacer material.

If a ground plane is not required the spacer dielectric constant is not requested.

### **Panel Size**

The program next asks for the desired size of the panel as shown in Figure 8.

At the prompt enter the desired dimensions for the array panel, including the filter network. The array will be centered within this area after leaving space for the filter network.

Enter desired HORIZONTAL dimension (in in.): 65.

Enter desired VERTICAL dimension (in in.): 65.

The actual array size is 65.000000 by 65.000000

The active array size is 65.000000 by 52.980800

There are 3 elements HORIZONTALLY and 3 elements VERTICALLY

HORIZONTAL spacing= 16.025600 VERTICAL spacing= 16.025600

Is this OK (y or n)? Y

**Figure 8 Prompt for Panel Size**

The panel size should include the space for the filter network. The area containing the dipoles will be centered within the specified area after leaving space for the filter network.

The horizontal dimension is entered first and then the vertical dimension. The prompt includes the units requested earlier in the session. If the filter network is to be placed along the top or bottom edge the program checks the vertical dimension to insure

enough space is present for the network. If not, an error message is displayed with a request to try again. A similar check is made when the filter network is to be along the left or right edge.

For the example design the array is to be 65 in. by 65 in. square. The horizontal and vertical dimensions, however, need not be the same.

Using the requested dimensions, the program computes the number and spacing of the dipoles required to point the beams in the previously requested directions and avoid grating lobes. As shown in the figure, the program displays the results of these computations and waits for confirmation from the user that everything is okay. If the number or spacing of the dipoles is not to the user's liking, answering N will allow the panel size to be changed.

Currently, the largest number of dipoles allowed horizontally or vertically is 20. If the panel size and beam angles are such that the computed number of dipoles exceeds 20 the program will issue an error message and allow the user to decrease the size of the panel.

### Substrate Parameters

The final set of parameters requested by the program are the dielectric constant and thickness of the substrate material. The program prompt is shown in Figure 9.

In order to design the filter network the dielectric constant and thickness of the SUBSTRATE must be specified. Please enter these values at the prompts.  
(Teflon glass= 2.76 Mylar=2.25)

Enter substrate DIELECTRIC CONSTANT: 2.25  
Enter substrate THICKNESS (in in.): 0.005

**Figure 9 Prompt for Substrate Parameters**

These parameters are required for the design of the matching and filter networks. The program lists the dielectric constant for Teflon glass and for Mylar, two common substrate materials. Also, the program, again, includes the required units in the prompt for the substrate thickness.

For the example design the substrate has a dielectric constant of 2.25 and is 5 mils thick. These values were measured from the mylar drafting film used in building this antenna.

### Input Check

Before proceeding with the design of the array, the program next displays a summary showing the values of the previously entered parameters to be used in the design. As shown in Figure 10, the



The parameters which will be used in the design of the array are as follows:

Source Frequency .....	0.491 GHz
Position of Beam #1 (Az El) .....	0 0 degrees
Panel Tilt .....	0 degrees
Dipole Tilt .....	90 degrees
Location of the Filter Network .....	Bottom
Gnd Plane Spacer Dielectric Constant ..	1.03300000
Panel horizontal dimension .....	65 in.
Panel vertical dimension .....	65 in.
Substrate Dielectric Constant .....	2.25
Substrate thickness .....	0.005 in.

Are these parameters ok (y or n)? Y

**Figure 10 Prompt for Input Parameter Verification**

user is then asked to verify that these values are correct. As indicated in the prompt, enter either Y or N (again, case is ignored) in response to the prompt.

Responding with N indicates that one or more of the parameters was incorrect. The program will return to the Figure 1 prompt and proceed to ask for each of the input parameters again. Answering Y to the Figure 10 prompt will cause the program to proceed with the design.

### Program Output

The program now has all the information required to compute the driving point currents, the driving point impedances, and the principal plane patterns.

### Computation of Pattern Cuts

The program is now ready to compute and display cuts of the radiation pattern. Since this is not always desired, the program asks the user if pattern plots are desired as shown in Figure 11.

Do you want to see the pattern plots (y or n)? Y

**Figure 11 Prompt for Pattern Plots**

As indicated in the prompt, the user should respond with either Y, to see the patterns, or N, to skip the pattern computation. Any other response will result in an error message and a request to try again.

If the patterns are desired the user is presented with a menu of allowed hard-copy devices as shown in Figure 12.

Graphics can be displayed on the following devices:

- 0 - an EGA monochrome display,
- 1 - an IBM CGA display,
- 2 - an HP 7470A plotter, or
- 3 - an HP LaserJet printer.

Please enter the number corresponding to your choice: 0

**Figure 12 Prompt for Hard Copy device**

The desired output device is chosen by entering the corresponding number. If something other than these numbers are entered an error message is displayed and the user is asked to try again. No checking for the existence of the selected device is performed so the user should be sure that the selected device is present.

The program expects the LaserJet printer to be connected as **PRN** or **LPT1** (they are equivalent). If the LaserJet is connected to the serial port the appropriate DOS **MODE** commands should have been executed before running the program.

The program expects the HP 7470A plotter to be connected to **COM1** and setup to run at 9600 bps, no parity, 8 data bits, 1 stop bit. The **Y/D** switch should be set to **D**. No DOS **MODE** command is necessary to initialize the **COM1** port.

If the CGA is selected as the hardcopy device the graphics will be displayed in the CGA monochrome graphics mode even if a color monitor is being used. The PLOT88 package being used to provide graphics only supports the monochrome mode in graphics since it provides the highest resolution. The color graphics modes are not high enough in resolution to be of much use for this application anyway. Some graphics cards allow running CGA modes on a monochrome monitor. In order to display graphics on the monitor it may be necessary to put the card in CGA mode, using the DOS command, **MODE CO80**, before running the program.

Once the hard-copy device is selected, the user is prompted for the elevation angle desired for the azimuth cut, and the azimuth angle desired for the elevation cut, as shown in Figure 13.

Beginning AZIMUTH pattern plot. Please enter the ELEVATION angle desired for the cut (ELBeam=0): 0.

Please wait - Computing the AZIMUTH pattern...

Beginning ELEVATION pattern plot. Please enter the AZIMUTH angle desired for the cut (AZBeam=0): 0.

Please wait - Computing the ELEVATION pattern...

**Figure 13 Prompt for Constant Angles for Patterns**

For the user's convenience, the prompts include the beam angles, requested earlier, in parenthesis. Since the computation of the patterns takes some time, the program displays the **Please wait** messages while computing each cut. Also, the wording of these messages changes as the computations progress as an added assurance that the program is running and all is well. The program beeps the speaker when it is ready for more input.

After computation of the patterns, the program will display a message either requesting the user strike a key, or informing the user to wait while the hard-copy is made. The exact wording of the message is dependant upon the particular hard-copy device selected.

In the case of either the EGA or CGA displays the user should strike a key (the space bar is a good choice) to display the azimuth pattern plot. After completing the plot, the program will wait for the user to finish studying the pattern. When ready strike the space bar (or any other key) to display the elevation pattern. When the user is finished studying the elevation pattern again strike the space bar.

If the HP 7470A plotter is selected as the hard-copy device the program will prompt the user to load paper and strike any key to begin plotting. When the plotter is finished the program will stop and, again, wait for a key press to continue.

If the HP LaserJet printer is selected as the hard-copy device the program will display a **Please wait** message indicating that data is being sent to the printer. The printer **READY** light should be blinking during the transfer. The paper is automatically ejected from the printer when the plot is complete.

Once the hard-copy plots have been completed the program asks the user if another cut is desired, as shown in Figure 14. Responding with **Y** the user is again presented with the menu in Figure 12.



Do you want to see another cut (y or n)? N

**Figure 14 Prompt for Another Cut**

This allows the user to select either the laser printer or the plotter to get a paper copy of the patterns previously displayed on an EGA or CGA display, for example. The program then, again, asks for the elevation and azimuth angles for the cuts, recomputes the patterns, and displays them on the selected output device. When the program receives a **N** to the prompt in Figure 14 it begins the computation of the driving point impedances.

The patterns for the example design are shown in Figure 15. These patterns were produced on the HP LaserJet printer. Similar results are obtained when using the HP 7470A plotter.



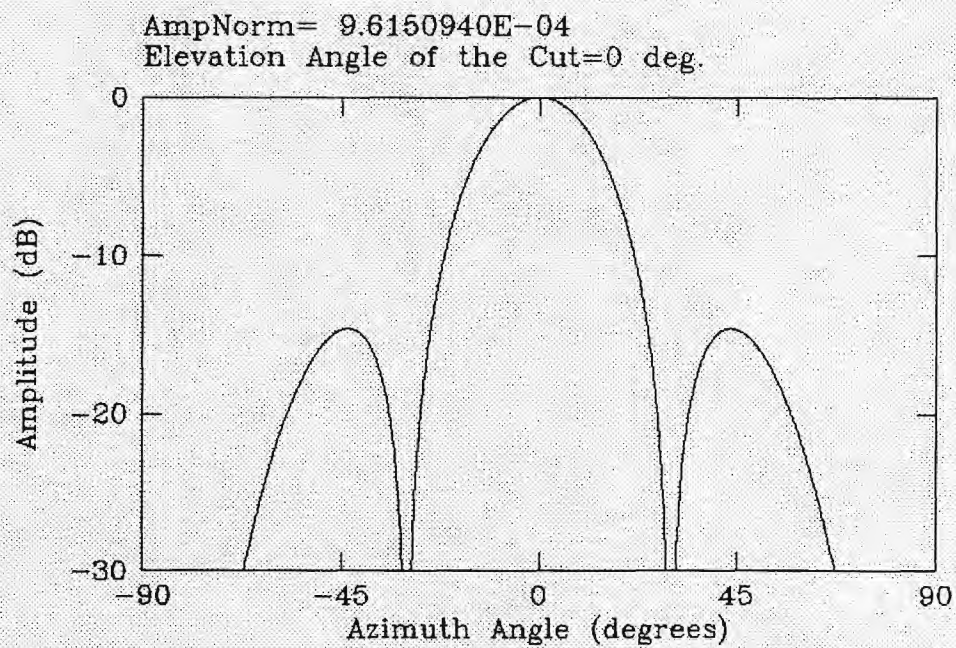
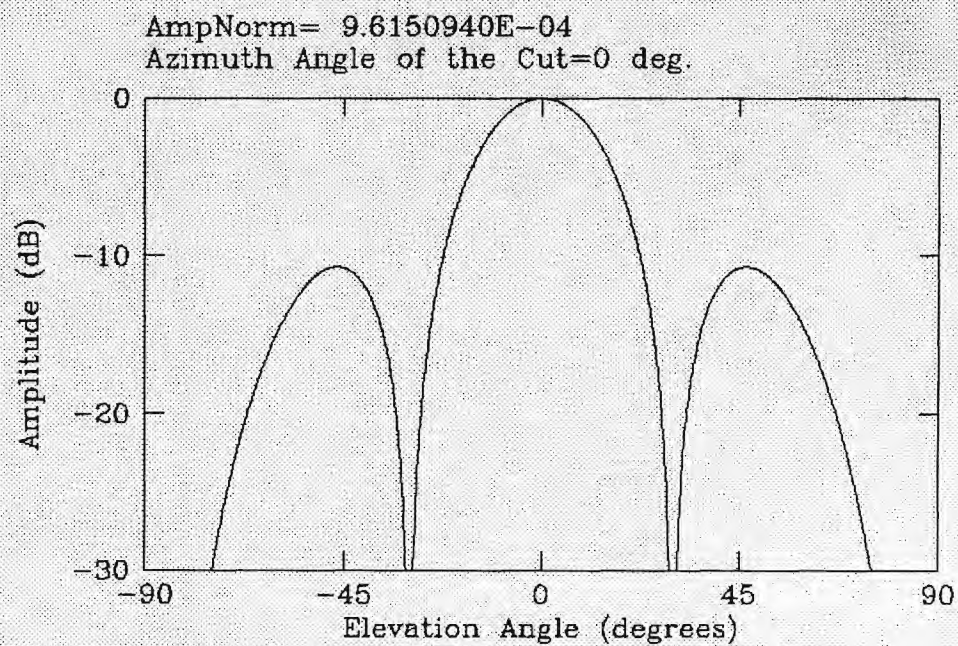


Figure 15 Pattern Cuts for Example Design

### Computation of Driving Point Impedances

Depending on the size of the array, the computation of the driving point impedances may take some time. The example design, with 3 elements by 3 elements, takes approximately 20 seconds for this computation on an IBM XT. To reassure the user that the machine has not locked up, the program displays a **Please wait** while it computes the impedances. The speaker is sounded when the computation has finished.

### Summary of Array Design

At this point, the program is ready to write a summary of the design to a file. If **File\_Name** was specified on the DOS command line the program will write the data to **File\_Name**. If **File\_Name** was not specified the program will prompt for a file name as shown in Figure 16.



Enter name of file to receive design summary: PRN

**Figure 16 Prompt for Output Filename**

Any valid DOS file name is an acceptable answer to this prompt, including the DOS reserved names **PRN**, **CON**, or **NUL**.

If a disk file is specified as the output file, either on the command line or in answer to the Figure 16 prompt, the program checks to see if the file already exists. If it does the program will warn the user and ask if it is okay to overwrite the file. If the user indicates that the file should **not** be overwritten the program will ask for a new filename.

If the summary data is sent to a disk file the program displays a message to remind the user of the name of the file containing the data. This is especially helpful when the file name is entered on the command line.

The summary data for the example design is shown in Figure 17.



```

DIPOLE ARRAY DESIGN          9/14/1989  14:48:50
*****
The operating frequency is  4.910000E-01 GHz  (Lambda=  24.038400 in.)
The beam is pointed at    0.000000E+00 deg. AZIMUTH  0.000000E+00 deg. ELEVATION
*****
The array panel is tilted   0.000000E+00 degrees in ELEVATION
The array is 65.000000 in. by 65.000000 in.
There are 3 elements in the HORIZONTAL direction
        3 elements in the VERTICAL direction
The dipole elements are spaced 16.025600 in. apart HORIZONTALLY
        16.025600 in. apart VERTICALLY
Each dipole is 11.177860 in. long and 2.500000E-01 in. wide
Each dipole is tilted 90.000000 degrees from VERTICAL
*****
The filter network is located along the BOTTOM edge of the substrate
The substrate dielectric constant is 2.250000
The substrate is 5.000000E-03 in. thick
*****
A ground plane is to be used 5.912830 in. from the array panel
The dielectric constant of the spacer material is 1.033000
*****

  Array      Location      Driving Point
Column Row Horizontal Vertical Current Impedance
  1 1 16.5 22.5 1.00 /-.000 87.4 /-7.09
  2 1 32.5 22.5 1.00 /-.000 101. /-14.3
  3 1 48.5 22.5 1.00 /-.000 87.4 /-7.09
  1 2 16.5 38.5 1.00 /-.000 65.1 /-24.4
  2 2 32.5 38.5 1.00 /-.000 68.8 /-37.1
  3 2 48.5 38.5 1.00 /-.000 65.1 /-24.4
  1 3 16.5 54.5 1.00 /-.000 87.4 /-7.09
  2 3 32.5 54.5 1.00 /-.000 101. /-14.3
  3 3 48.5 54.5 1.00 /-.000 87.4 /-7.09
*****
Azimuth Elevation Gain dBi
.000 .000 17.350
*****

```

Figure 17 Summary Data for Example Design

### Layout Data

To interface to the layout programs DIPARA next writes data required by these programs to a disk file on the current drive. The data is written to the file **LAYOUT.DAT**. Any old data which might exist in that file is overwritten.

### Display of Array Schematic

Finally, the program can plot a schematic of the array. This is useful for checking the locations of the dipoles and that the tilt angle was entered correctly. The program asks the user if the display schematic is desired, as shown in Figure 18.

```

Do you want to see the array schematic (y or n)? Y

```

Figure 18 Prompt for Array Schematic

Answering Y to the prompt results in the Figure 12 prompt for selection of the graphics hard-copy device. The details of using

this menu were described in the section on plotting the pattern cuts and will not be repeated here.

After the user chooses a hard-copy device the program displays a **Please wait** message while it makes the computations to plot the array schematic. When it is ready to display the schematic it will sound the speaker, display a message, and wait for the user to strike a key if the EGA, CGA or HP 7470A plotter was chosen as the hard-copy device. Just a message will be displayed if the laser printer is the hard-copy device.

Once the hard-copy has been finished the program will terminate and return to the DOS command line. It may be necessary to strike a key first, in which case a message to that effect will be displayed.

The array schematic for the example design is shown in Figure 19. It was produced on the laser printer but similar results will be obtained using the HP plotter.

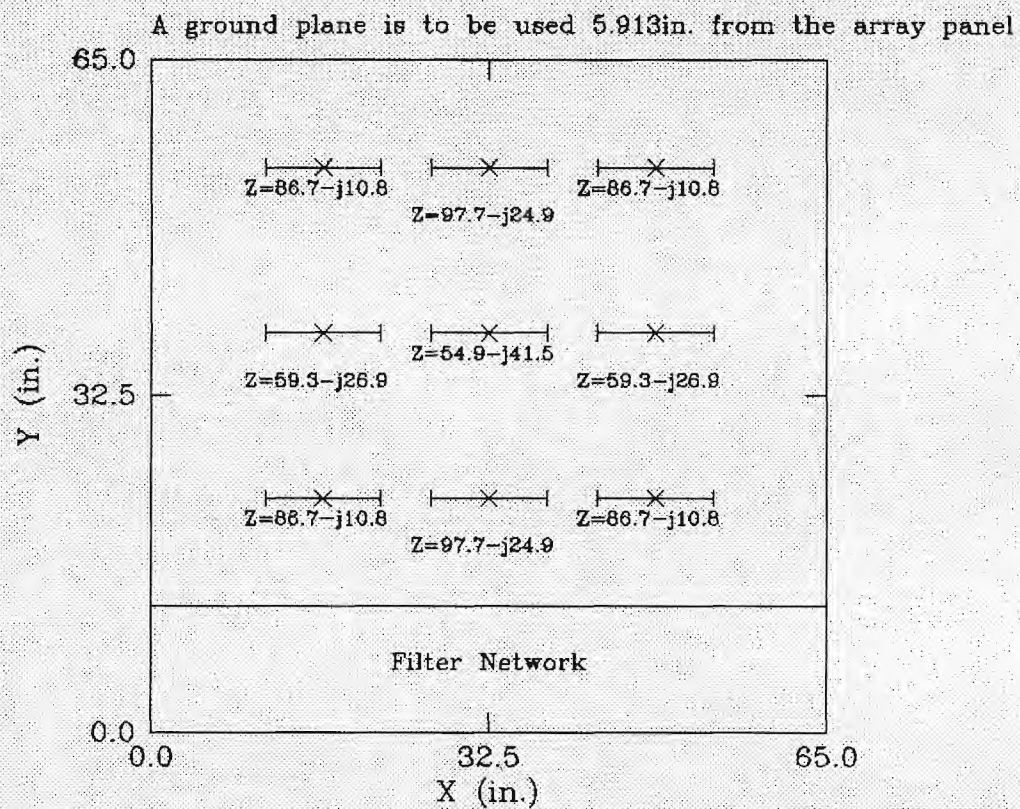


Figure 19 Array Schematic for the Example Design

E-21-F-21

Draft  
Computer Operator  
Manual (AA002)



## Introduction

**DIPARA** is a strip dipole array design program. The user inputs the source frequency, main beam directions, array panel tilt, dipole tilt, location of a filter network, ground plane information, size of the array panel, and panel substrate dielectric constant and thickness. From this information the program determines the number of dipoles, their locations, and the driving point currents required to produce the desired beam direction. Also, the driving point impedances are determined for use in design of the matching and filter networks.

This user's manual describes how to run the program. To this end the reader is taken step by step through an example design.

### Running the Program: an example design

The example design is for a single beam antenna with the beam broadside to the array. The frequency of operation will be 491 MHz which is the frequency of TV channel 17.

To start the program type:

**DIPARA [File\_Name]**

at the DOS command prompt. **File\_Name** is the name of a file to receive the programs output summarizing the design. **File\_Name** is optional, the program will prompt for a file name if it is missing. It can be any valid DOS file name, including the reserved names **PRN** (output will go to the standard printer), **CON** (output will go to the console), or **NUL** (output is discarded). As with any alphanumeric input to the program, case is not important. The program will accept either upper or lower case.

### Program Input

#### Units for Linear Dimensions

The first request the program makes is for the units the user wants to use for linear dimensions. The prompt is shown in Figure 1. The program can handle units of **inches**, **feet**, **centimeters**, or **meters**. As described in the prompt, one of these is selected by typing **0**, **1**, **2**, or **3**, respectively. The program will only accept these four entries. If anything else is input an error message will be displayed and the user will be asked to try again. As shown in Figure 1, for this example **inches** will be used.

#### Source Frequency

Next the program requests the source frequency. This should be

Please specify the units you want to use for the array size and element position from one of the following:

- 0 - inches,
- 1 - feet,
- 2 - centimeters,
- 3 - meters.

Make your selection by entering the number corresponding to your choice.

I want to use: 0

Figure 1 Prompt for units

Enter the desired source frequency (in GHz): .491

Figure 2 Prompt for Source Frequency

specified in GHz, as indicated in the prompt shown in Figure 2. For this example the desired source frequency is .491 GHz (491 MHz).

### Beam Locations

The program next asks for the number of beams and their locations as shown in Figure 3.

When prompted enter the desired number of beams, and the AZIMUTH and ELEVATION angle (in degrees) for each beam.

Enter desired number of beams (1-3): 1  
Enter desired position of beam #1 (AZ, EL): 0. 0.

Figure 3 Prompt for number of beams and their locations

As indicated in the prompt for the number of beams, at least one beam is required and no more than three is allowed. If the number of beams is not in this range an error message is displayed and the user is asked to try again.

The beam locations are entered as azimuth and elevation angles in degrees. 0° azimuth, 0° elevation is perpendicular to the array panel, assuming no panel tilt (see below). Positive azimuth is clockwise (to your right) when looking in the direction of the beam. A positive elevation angle is up. These definitions correspond to those used in surveying. Although, there are no traps in the program to prevent you from doing so, it does not make sense to specify an azimuth or elevation angle outside the range  $\pm 90^\circ$ . The program will not allow overlapping main beam directions and will display an error message if this is attempted.

When entering the position of each beam the azimuth angle should be entered first, then the elevation angle. The user is reminded of this by the **AZ, EL** symbols shown in parenthesis in the prompt. The numbers may be entered both on the same line (without an intervening carriage return) or on separate lines. If the entries are on the same line separate them with a space or a comma. If a carriage return does separate the entries no additional prompts, indicating that an incomplete beam position has been entered, will be output by the program.

As shown in the figure, the beam is to be pointed perpendicular to the panel for the example design.

### Panel Tilt

The array panel can be tilted in elevation. As shown in Figure 4,

The panel containing the array may be tilted in elevation. At the prompt specify the desired panel tilt by entering the elevation angle of the panel normal.

Enter desired panel tilt (in degrees): 0.

Figure 4 Prompt for Panel Tilt

the program next asks for the desired panel tilt. This is specified by entering the elevation angle of the panel **normal** in degrees. As with the beam elevation angle, a positive panel tilt is up. A zero degree panel tilt is chosen for the example design. The array panel is, thus, vertical.

### Dipole Polarization

The polarization of the array is the next parameter requested as shown in Figure 5.

The dipoles making up the array can be tilted in the aperture. At the prompt enter the desired dipole tilt angle. The angle should be specified in degrees measured from the vertical. The dipoles will be vertical for a 0 degree tilt angle and horizontal for a 90 degree tilt angle. A positive tilt angle is assumed to be in a COUNTER-CLOCKWISE direction when looking in the same direction as the array.

Enter the desired dipole tilt (polarity): 90.

Figure 5 Prompt for array polarization

The polarization is specified by entering the dipole tilt angle in degrees. This tilt angle is in the plane of the panel. As indicated in the figure, the tilt angle is measured from vertical. That is, the dipoles will be vertical for a dipole tilt of 0° and

horizontal for a dipole tilt of 90°. Both positive and negative tilt angles are allowed. A positive tilt angle is assumed to be in a **counter-clockwise** direction when looking in the same direction as the array. For the example design, the tilt angle is specified as 90°; the dipoles will be horizontal.

### The Filter Network

To allow for removal of signals which are off frequency, a filter network can be placed on the array panel. The desired location of

Space must be left for the filter network along the

(T)op edge, or  
(B)ottom edge

of the array panel. Indicate your choice by typing the corresponding letter shown in parenthesis. I want: B

**Figure 6 Prompt for Location of Filter Network**

the filter network is asked for next, as shown in Figure 6. The prompt for the filter network location is dependent upon the requested dipole tilt angle. For

$$45^\circ \leq \text{DipTilt} < 90^\circ$$

the prompt is as shown in the figure. For

$$0^\circ < \text{DipTilt} < 45^\circ$$

(L)eft edge and (R)ight edge would replace (T)op edge and (B)ottom edge respectively. Here the angle supplied by the user has been adjusted so that **DipTilt** is between 0° and 90°.

The desired location is chosen by entering the letter shown in the parenthesis as indicated in the prompt. More than one letter may be typed but only the first letter is used. The program only accepts T, B, L, or R, ignoring case. Any other letters will result in an error message and a request to try again.

The filter network is to be placed along the bottom edge for the example design.

### Ground Plane Information

The program next asks if a ground plane is desired, as shown in Figure 7.



Do you want to use a ground plane (y or n)? Y

Please enter the dielectric constant of the SPACER material  
between the array substrate and ground plane  
(typically 1.033 for polystyrene): 1.033

**Figure 7 Prompt for Ground Plane Information**

As indicated in the prompt, enter either Y or N (again, case is ignored) in response to the prompt.

Responding with Y indicates that a ground plane is desired. The program will then ask for the dielectric constant of the material between the array panel and the ground plane. This value is used to compute the physical distance to the ground plane needed to build the array. This distance is recorded in the output file. Typical dielectric constants are less than 2.0 but no validation of the entered value is performed. For the user's convenience, the program lists the measured dielectric constant for polystyrene, a common spacer material.

For the example design polystyrene was chosen for the spacer material.

If a ground plane is not required the spacer dielectric constant is not requested.

### **Panel Size**

The program next asks for the desired size of the panel as shown in Figure 8.

At the prompt enter the desired dimensions for the array panel, including the filter network. The array will be centered within this area after leaving space for the filter network.

Enter desired HORIZONTAL dimension (in in.): 65.  
Enter desired VERTICAL dimension (in in.): 65.

The actual array size is        65.000000 by        65.000000  
The active array size is        65.000000 by        52.980800  
There are 3 elements HORIZONTALLY and 3 elements VERTICALLY  
HORIZONTAL spacing=        16.025600 VERTICAL spacing=        16.025600  
Is this OK (y or n)? Y

**Figure 8 Prompt for Panel Size**

The panel size should include the space for the filter network. The area containing the dipoles will be centered within the specified area after leaving space for the filter network.

The horizontal dimension is entered first and then the vertical dimension. The prompt includes the units requested earlier in the

session. If the filter network is to be placed along the top or bottom edge the program checks the vertical dimension to insure enough space is present for the network. If not, an error message is displayed with a request to try again. A similar check is made when the filter network is to be along the left or right edge.

For the example design the array is to be 65 in. by 65 in. square. The horizontal and vertical dimensions, however, need not be the same.

Using the requested dimensions, the program computes the number and spacing of the dipoles required to point the beams in the previously requested directions and avoid grating lobes. As shown in the figure, the program displays the results of these computations and waits for confirmation from the user that everything is okay. If the number or spacing of the dipoles is not to the user's liking, answering N will allow the panel size to be changed.

Currently, the largest number of dipoles allowed horizontally or vertically is 20. If the panel size and beam angles are such that the computed number of dipoles exceeds 20 the program will issue an error message and allow the user to decrease the size of the panel.

#### Substrate Parameters

The final set of parameters requested by the program are the dielectric constant and thickness of the substrate material. The program prompt is shown in Figure 9.

In order to design the filter network the dielectric constant and thickness of the SUBSTRATE must be specified. Please enter these values at the prompts.  
(Teflon glass= 2.76 Mylar=2.25)

Enter substrate DIELECTRIC CONSTANT: 2.25  
Enter substrate THICKNESS (in in.): 0.005

**Figure 9 Prompt for Substrate Parameters**

These parameters are required for the design of the matching and filter networks. The program lists the dielectric constant for Teflon glass and for Mylar, two common substrate materials. Also, the program, again, includes the required units in the prompt for the substrate thickness.

For the example design the substrate has a dielectric constant of 2.25 and is 5 mils thick. These values were measured from the mylar drafting film used in building this antenna.

### Input Check

Before proceeding with the design of the array, the program next displays a summary showing the values of the previously entered parameters to be used in the design. As shown in Figure 10, the

```
The parameters which will be used in the design of the array are as follows:

Source Frequency ..... 0.491 GHz
Position of Beam #1 (Az El) ..... 0 0 degrees
Panel Tilt ..... 0 degrees
Dipole Tilt ..... 90 degrees
Location of the Filter Network ..... Bottom
Gnd Plane Spacer Dielectric Constant .. 1.03300000
Panel horizontal dimension ..... 65 in.
Panel vertical dimension ..... 65 in.
Substrate Dielectric Constant ..... 2.25
Substrate thickness ..... 0.005 in.

Are these parameters ok (y or n)? Y
```

**Figure 10 Prompt for Input Parameter Verification**

user is then asked to verify that these values are correct. As indicated in the prompt, enter either Y or N (again, case is ignored) in response to the prompt.

Responding with N indicates that one or more of the parameters was incorrect. The program will return to the Figure 1 prompt and proceed to ask for each of the input parameters again. Answering Y to the Figure 10 prompt will cause the program to proceed with the design.

### Program Output

The program now has all the information required to compute the driving point currents, the driving point impedances, and the principal plane patterns.

### Computation of Pattern Cuts

The program is now ready to compute and display cuts of the radiation pattern. Since this is not always desired, the program asks the user if pattern plots are desired as shown in Figure 11.

```
Do you want to see the pattern plots (y or n)? Y
```

**Figure 11 Prompt for Pattern Plots**

As indicated in the prompt, the user should respond with either Y, to see the patterns, or N, to skip the pattern computation. Any other response will result in an error message and a request to try again.



If the patterns are desired the user is presented with a menu of allowed hard-copy devices as shown in Figure 12.

```
Graphics can be displayed on the following devices:

    0 - an EGA monochrome display,
    1 - an IBM CGA display,
    2 - an HP 7470A plotter, or
    3 - an HP LaserJet printer.

Please enter the number corresponding to your choice: 0
```

Figure 12 Prompt for Hard Copy device

The desired output device is chosen by entering the corresponding number. If something other than these numbers are entered an error message is displayed and the user is asked to try again. No checking for the existence of the selected device is performed so the user should be sure that the selected device is present.

The program expects the LaserJet printer to be connected as **PRN** or **LPT1** (they are equivalent). If the LaserJet is connected to the serial port the appropriate DOS **MODE** commands should have been executed before running the program.

The program expects the HP 7470A plotter to be connected to **COM1** and setup to run at 9600 bps, no parity, 8 data bits, 1 stop bit. The **Y/D** switch should be set to **D**. No DOS **MODE** command is necessary to initialize the **COM1** port.

If the CGA is selected as the hardcopy device the graphics will be displayed in the CGA monochrome graphics mode even if a color monitor is being used. The PLOT88 package being used to provide graphics only supports the monochrome mode in graphics since it provides the highest resolution. The color graphics modes are not high enough in resolution to be of much use for this application anyway. Some graphics cards allow running CGA modes on a monochrome monitor. In order to display graphics on the monitor it may be necessary to put the card in CGA mode, using the DOS command, **MODE CO80**, before running the program.

Once the hard-copy device is selected, the user is prompted for the elevation angle desired for the azimuth cut, and the azimuth angle desired for the elevation cut, as shown in Figure 13.

Beginning AZIMUTH pattern plot. Please enter the ELEVATION angle desired for the cut (ELBeam=0): 0.

Please wait - Computing the AZIMUTH pattern...

Beginning ELEVATION pattern plot. Please enter the AZIMUTH angle desired for the cut (AZBeam=0): 0.

Please wait - Computing the ELEVATION pattern...

Figure 13 Prompt for Constant Angles for Patterns

For the user's convenience, the prompts include the beam angles, requested earlier, in parenthesis. Since the computation of the patterns takes some time, the program displays the **Please wait** messages while computing each cut. Also, the wording of these messages changes as the computations progress as an added assurance that the program is running and all is well. The program beeps the speaker when it is ready for more input.

After computation of the patterns, the program will display a message either requesting the user strike a key, or informing the user to wait while the hard-copy is made. The exact wording of the message is dependant upon the particular hard-copy device selected.

In the case of either the EGA or CGA displays the user should strike a key (the space bar is a good choice) to display the azimuth pattern plot. After completing the plot, the program will wait for the user to finish studying the pattern. When ready strike the space bar (or any other key) to display the elevation pattern. When the user is finished studying the elevation pattern again strike the space bar.

If the HP 7470A plotter is selected as the hard-copy device the program will prompt the user to load paper and strike any key to begin plotting. When the plotter is finished the program will stop and, again, wait for a key press to continue.

If the HP LaserJet printer is selected as the hard-copy device the program will display a **Please wait** message indicating that data is being sent to the printer. The printer **READY** light should be blinking during the transfer. The paper is automatically ejected from the printer when the plot is complete.

Once the hard-copy plots have been completed the program asks the user if another cut is desired, as shown in Figure 14. Responding with **Y** the user is again presented with the menu in Figure 12.

Do you want to see another cut (y or n)? **N**

Figure 14 Prompt for Another Cut

This allows the user to select either the laser printer or the plotter to get a paper copy of the patterns previously displayed on an EGA or CGA display, for example. The program then, again, asks for the elevation and azimuth angles for the cuts, recomputes the patterns, and displays them on the selected output device. When the program receives a N to the prompt in Figure 14 it begins the computation of the driving point impedances.

The patterns for the example design are shown in Figure 15. These patterns were produced on the HP LaserJet printer. Similar results are obtained when using the HP 7470A plotter.

### Computation of Driving Point Impedances

Depending on the size of the array, the computation of the driving point impedances may take some time. The example design, with 3 elements by 3 elements, takes approximately 20 seconds for this computation on an IBM XT. To reassure the user that the machine has not locked up, the program displays a **Please wait** while it computes the impedances. The speaker is sounded when the computation has finished.

### Summary of Array Design

At this point, the program is ready to write a summary of the design to a file. If **File\_Name** was specified on the DOS command line the program will write the data to **File\_Name**. If **File\_Name** was not specified the program will prompt for a file name as shown in Figure 16.



Enter name of file to receive design summary: PRN

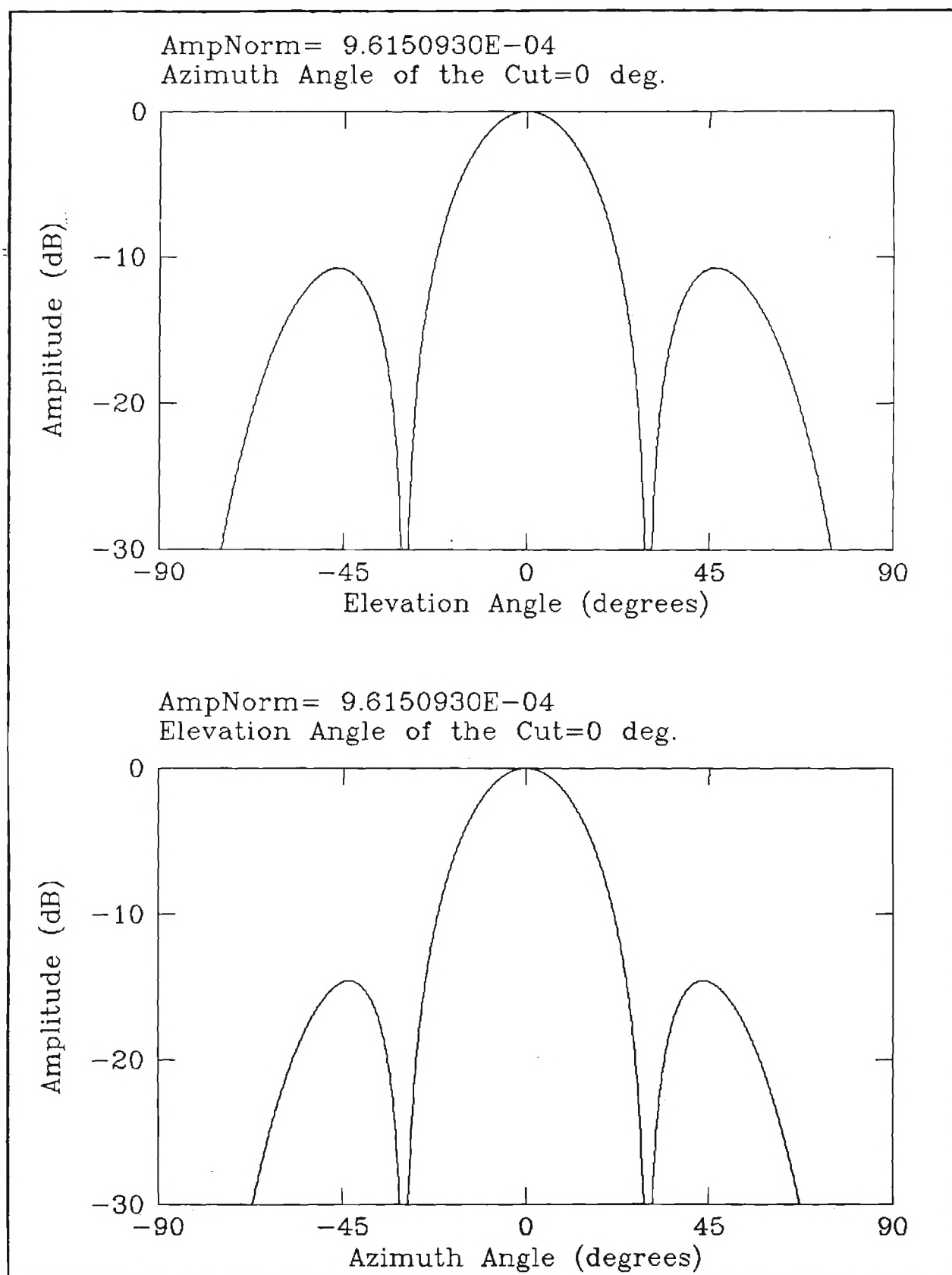
**Figure 16 Prompt for Output Filename**

Any valid DOS file name is an acceptable answer to this prompt, including the DOS reserved names **PRN**, **CON**, or **NUL**.

If a disk file is specified as the output file, either on the command line or in answer to the Figure 16 prompt, the program checks to see if the file already exists. If it does the program will warn the user and ask if it is okay to overwrite the file. If the user indicates that the file should **not** be overwritten the program will ask for a new filename.

If the summary data is sent to a disk file the program displays a message to remind the user of the name of the file containing the data. This is especially helpful when the file name is entered on the command line.

The summary data for the example design is shown in Figure 17.



**Figure 15 Pattern Cuts for Example Design**



```

DIPOLE ARRAY DESIGN          9/14/1989  14:48:50
*****
The operating frequency is  4.910000E-01 GHz (Lambda=  24.038400 in.)
The beam is pointed at    0.000000E+00 deg. AZIMUTH  0.000000E+00 deg. ELEVATION
*****
The array panel is tilted   0.000000E+00 degrees in ELEVATION
The array is               65.000000 in. by  65.000000 in.
There are                  3 elements in the HORIZONTAL direction
                        3 elements in the VERTICAL direction
The dipole elements are spaced  16.025600 in. apart HORIZONTALLY
                        16.025600 in. apart VERTICALLY
Each dipole is            11.177860 in. long and  2.500000E-01 in. wide
Each dipole is tilted      90.000000 degrees from VERTICAL
*****
The filter network is located along the BOTTOM edge of the substrate
The substrate dielectric constant is  2.250000
The substrate is          5.000000E-03 in. thick
*****
A ground plane is to be used  5.912830 in. from the array panel
The dielectric constant of the spacer material is  1.033000
*****

      Array      Location      Driving Point
Column Row Horizontal Vertical Current Impedance
1      1      16.5      22.5      1.00 /_ .000      87.4 /_ -7.09
2      1      32.5      22.5      1.00 /_ .000      101. /_ -14.3
3      1      48.5      22.5      1.00 /_ .000      87.4 /_ -7.09
1      2      16.5      38.5      1.00 /_ .000      65.1 /_ -24.4
2      2      32.5      38.5      1.00 /_ .000      68.8 /_ -37.1
3      2      48.5      38.5      1.00 /_ .000      65.1 /_ -24.4
1      3      16.5      54.5      1.00 /_ .000      87.4 /_ -7.09
2      3      32.5      54.5      1.00 /_ .000      101. /_ -14.3
3      3      48.5      54.5      1.00 /_ .000      87.4 /_ -7.09
*****
Azimuth Elevation Gain dBi
.000 .000 17.350
*****

```

Figure 17 Summary Data for Example Design

### Layout Data

To interface to the layout programs DIPARA next writes data required by these programs to a disk file on the current drive. The data is written to the file **LAYOUT.DAT**. Any old data which might exist in that file is overwritten.

### Display of Array Schematic

Finally, the program can plot a schematic of the array. This is useful for checking the locations of the dipoles and that the tilt angle was entered correctly. The program asks the user if the display schematic is desired, as shown in Figure 18.

```

Do you want to see the array schematic (y or n)? Y

```

Figure 18 Prompt for Array Schematic



Answering **Y** to the prompt results in the Figure 12 prompt for selection of the graphics hard-copy device. The details of using this menu were described in the section on plotting the pattern cuts and will not be repeated here.

After the user chooses a hard-copy device the program displays a **Please wait** message while it makes the computations to plot the array schematic. When it is ready to display the schematic it will sound the speaker, display a message, and wait for the user to strike a key if the EGA, CGA or HP 7470A plotter was chosen as the hard-copy device. Just a message will be displayed if the laser printer is the hard-copy device.

Once the hard-copy has been finished the program will terminate and return to the DOS command line. It may be necessary to strike a key first, in which case a message to that effect will be displayed.

The array schematic for the example design is shown in Figure 19. It was produced on the laser printer but similar results will be obtained using the HP plotter.

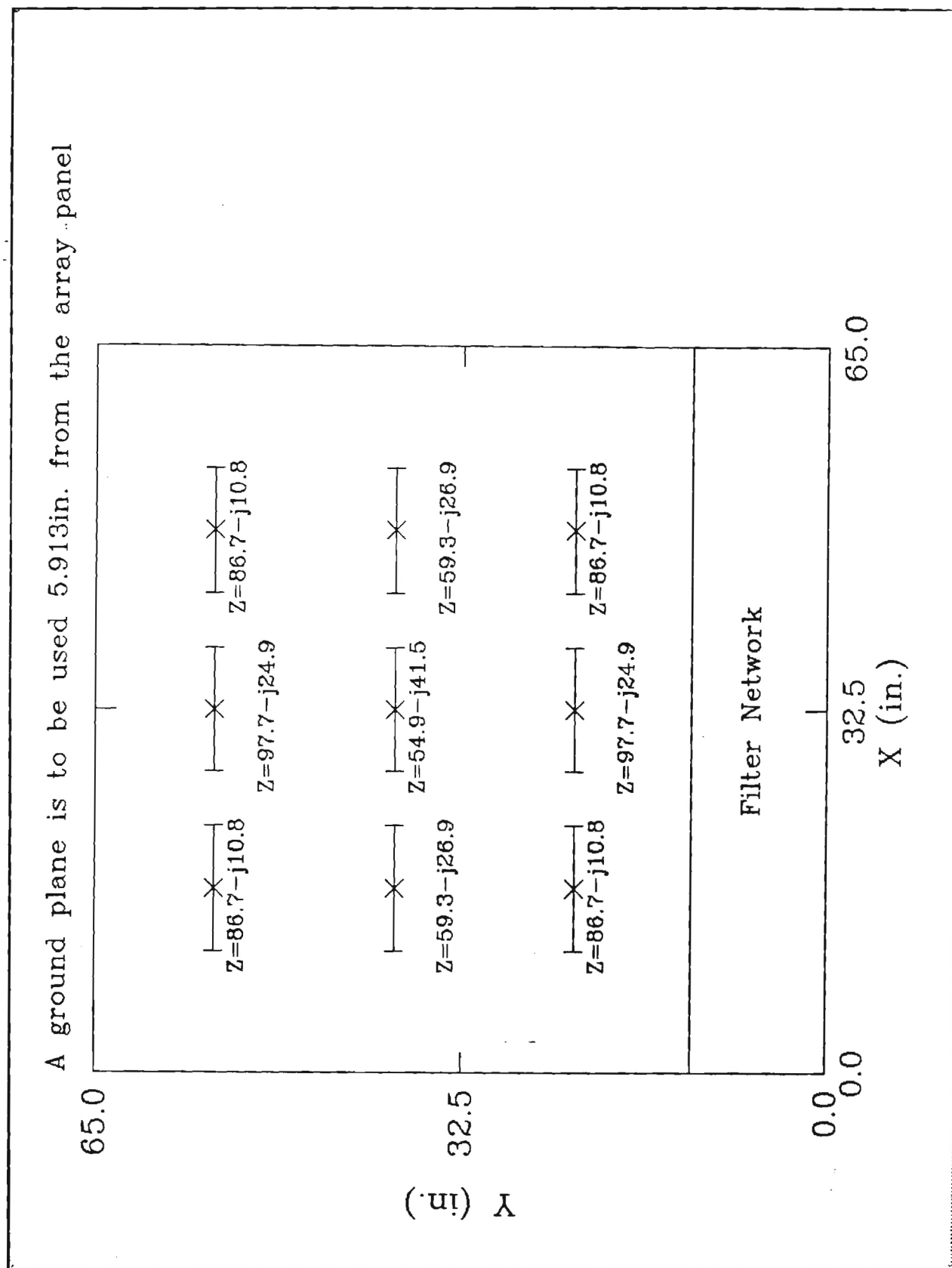


Figure 19 Array Schematic for the Example Design

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
AIDED DESIGN AND LAYOUT PROGRAM

COMPUTER PROGRAM

Contract Number: MDA970-88-C-8145

Prepared by

Georgia Institute of Technology  
School of Electrical Engineering  
Atlanta, Georgia

A PLANAR SURFACE, DIPOLE, PHASED ARRAY COMPUTER  
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```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling PROGRAM DIPARA'
4  $TITLE: 'PROGRAM DIPARA.FOR'
5  $PAGE
6  $NOTRUNCATE
7  PROGRAM DIPARA
8  C
9  C  LAST MODIFIED  8/22/88.  BY R. WILSON.
10 C  *****  9/27/88.  BY R. WILSON.
11 C      1) Added call to "DRWARA" to plot a picture of the array.
12 C  *****  11/01/88.  BY R. WILSON.
13 C      1) Changed from using "THBEAM" and "PHIBEAM" (spherical angles to
14 C        directly using "AZBEAM" and "ELBEAM".
15 C      2) Added call to "ARAPAT" to plot array azimuth and elevation
16 C        patterns.
17 C  *****  12/11/88.  BY R. WILSON.
18 C      1) Added handling of dipole tilt (Tilt of Linear Polarization).
19 C  *****  3/09/89.  BY R. WILSON.
20 C      1) Added handling of multiple beams.
21 C  *****  4/04/89.  BY R. WILSON.
22 C      1) Added handling of ground plane.
23 C  *****  4/23/89.  BY R. WILSON.
24 C      1) Moved computation of "DRVVOLT" and "ZDRVIMP" into "DRVPNT".
25 C      2) This allows the program to work for large arrays on the PC since
26 C        only one row/column of the system impedance matrix is stored.
27 C  *****  5/08/89.  BY R. WILSON.
28 C      1) Removed computation of "DRVVOLT" since it is not used.
29 C  *****  5/11/89.  BY R. WILSON.
30 C      1) Added computation of gain at main beam locations.
31 C  *****  5/16/89.  BY R. WILSON.
32 C      1) Added compensation for non-air spacer material in the
33 C        computed value of the ground plane distance.
34 C      2) Two distances are now computed, "DGNDPLD", and "DGNDPLA".
35 C  *****  6/06/89.  BY R. WILSON.
36 C      1) Corrected method of loading impedances in "DRVPNT" to account
37 C        for the fact that when the dipoles are tilted (not 0 or 90 degrees)
38 C        the impedances are functions of SIGN(IVOL-ICUR)*SIGN(JVOL-JCUR)
39 C        not ABS(IVOL-ICUR)*ABS(JVOL-JCUR).
40 C  *****  6/21/89.  BY R. WILSON.
41 C      1) Changed to using an array, "GNDPLN", to hold the two ground plane
42 C        distances and added the spacer dielectric constant as the third
43 C        value stored in "GNDPLN".
44 C  *****  8/08/89.  BY R. WILSON.
45 C      1) Added call to OPNFILE to open the output file.
46 C      2) OPNFILE can get the name of the file to open from the
47 C        command line. If it doesn't find the name on the command line
48 C        it prompts the user for the name.
49 C      3) This capability is provided by the fortran library, however,
50 C        the prompt provided is not very flexible. The prompt from
51 C        OPNFILE is programmer changeable.
52 C  *****  9/13/89.  BY R. WILSON.
53 C      1) Added call to SHOWIN to allow the user to check his inputs to
54 C        the program before the design is performed.
55 C      2) Moved writing the design summary from the main program to SUMMARY.
56 C
57 C  "DIPARA" designs a two dimensional dipole array. The size of the array,
58 C  the frequency of operation, and the main beam direction are specified by
59 C  the user.
60 C
61 C  PARAMETER (NXELMX=20,NYELMX=20,NXYELMX=NXELMX*NYELMX)
62 C  PARAMETER (MXNBEAM=3)
63 C  COMPLEX ZDRVIMP(NXELMX,NYELMX),ZSYSROW(NXYELMX,2)
64 C  COMPLEX DRVCURR(NXELMX,NYELMX)
65 C  COMPLEX REC2POL
66 C  REAL XLOCATE(NXELMX),YLOCATE(NYELMX)
67 C  REAL AZBEAM(MXNBEAM),ELBEAM(MXNBEAM),GAIN(MXNBEAM),DIPTILT(3)
68 C  REAL GNDPLN(3),FREQ2K0,K0,LAMBDA
69 C  LOGICAL YESNOTF,INPUTOK

```

```

70      CHARACTER DATE*10,TIME*8,FNAME*32,UNITS*2,LFILNET*1
71      CHARACTER DATSTMP*20
72 C
73 C      Initialize the date and time stamp for the output.
74 C
75      DATSTMP=DATE(//)' '//TIME( )
76      INPUTOK=.FALSE.
77      DO WHILE (.NOT. INPUTOK)
78 C
79 C      Obtain the units desired for length and position specifications.
80 C
81      CALL GETUNIT(UNITS,FREQ2K0)
82 C
83 C      Obtain the operating frequency.
84 C
85      CALL GETFREQ(FREQGHZ,FREQ2K0,K0,LAMBDA)
86 C
87 C      Obtain direction of beam.
88 C
89      CALL GETBEAM(MXNBEAM,NUMBEAM,AZBEAM,ELBEAM)
90 C
91 C      Obtain the array geometry.
92 C
93      CALL GETGEOM(UNITS,LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,
94 $      DIPTILT,XSIZE,YSIZE,NXEL,NXELMX,NYEL,NYELMX,XLOCATE,YLOCATE,
95 $      DIPWID,DIPLNG,DX,DY,LFILNET,SFILNET,GNDPLN)
96 C
97 C      Obtain substrate dielectric constant and thickness.
98 C
99      CALL GSUBSTR(UNITS,ERSUB,THSUB)
100 C
101 C      Display the inputs for user approval.
102 C
103      CALL SHOWIN(UNITS,FREQGHZ,NUMBEAM,AZBEAM,ELBEAM,PANTILT,
104 $      DIPTILT(3),LFILNET,GNDPLN,XSIZE,YSIZE,ERSUB,THSUB,INPUTOK)
105      END DO
106 C
107 C      Load driving point current array.
108 C
109      CALL LDCURNT(K0,XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,NUMBEAM,AZBEAM,
110 $      ELBEAM,PANTILT,DRVCURR)
111 C
112 C      Plot the azimuth and elevation patterns.
113 C
114      WRITE(*,*)
115      IF(YesNOTF('Do you want to see the pattern plots'))THEN
116          CALL ARAPAT(K0,NUMBEAM,AZBEAM,ELBEAM,PANTILT,DIPLNG,DIPTILT,
117 $      GNDPLN(1),XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,DRVCURR)
118      ENDIF
119 C
120 C      Compute the driving point impedances.
121 C
122      WRITE(*,100)
123 100 FORMAT(/1X,'Please wait - computing the driving point',
124 $ 1X,'impedances...')
125      CALL DRVPNT(LAMBDA,NXEL,NXELMX,NYEL,XLOCATE,YLOCATE,DIPWID,
126 $      DIPLNG,DIPTILT,GNDPLN(1),DRVCURR,ZDRVIMP,ZSYSROW,NXYELMX)
127      CALL BEEP
128 C
129 C      Compute the main beam gain.
130 C
131      CALL ARAGAIN(K0,NUMBEAM,AZBEAM,ELBEAM,PANTILT,DIPLNG,DIPTILT,
132 $      GNDPLN(1),XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,DRVCURR,ZDRVIMP,GAIN)
133 C
134 C      Write the array parameters to a file.
135 C
136      FNAME=' '
137      CALL OPNFILE(1,'OUTPUT',FNAME,NAMLGTH,
138 $      'Enter name of file to receive design summary:',1)

```

```

139      CALL SUMMARY(DATSTMP,UNITS,FREQGHZ,LAMBDA,NUMBEAM,AZBEAM,ELBEAM,
140      $ PANTILT,XSIZE,YSIZE,NXEL,NXELMX,NYEL,DX,DY,DIPLNG,DIPWID,
141      $ DIPTILT,LFILNET,ERSUB,THSUB,GNDPLN,XLOCATE,YLOCATE,DRVCURR,
142      $ ZDRVIMP,GAIN)
143 C
144 C
145 C WRITE THE FIRST AND "NXEL"TH ROW OF THE SYSTEM IMPEDANCE MATRIX TO THE
146 C FILE. CLOSE THE OUTPUT FILE ON TAPE1.
147 C
148 C     NXYEL=NXEL*NYEL
149 C     DO 5 J=1,2,1
150 C         WRITE(1,*)'ZSYSROW(I,','J,')'
151 C         WRITE(1,*)(ZSYSROW(I,J),I=1,NXYEL,1)
152 C     5 CONTINUE
153 C
154 C Close the output file on TAPE1. Remind the user to which file the output
155 C was written if the file is on disk. Send form-feed if file was sent to the
156 C printer (PRN or LPT1). BIOPR is a PLOT88 routine.
157 C
158 C     CLOSE(1)
159 C     IF(FNAME.NE.'CON' .AND. FNAME.NE.'PRN' .AND. FNAME.NE.'NUL')
160 C     $ WRITE(*,*)'Array data written to file ',FNAME
161 C     IF(FNAME .EQ. 'PRN')CALL BIOPR(0,CHAR(12),1)
162 C
163 C Write data to file for use by the layout programs.
164 C
165 C     OPEN(1,FILE='LAYOUT.DAT')
166 C     TOINCH=UNIT2IN(1.0,UNITS)
167 C
168 C     WRITE(1,*)FREQGHZ
169 C     WRITE(1,*)XSIZE*TOINCH,YSIZE*TOINCH
170 C     WRITE(1,*)ERSUB,THSUB*TOINCH
171 C     WRITE(1,*)DIPLNG*TOINCH,DIPWID*TOINCH,DIPTILT(3)
172 C     WRITE(1,('(1X,A1,1X,1PG15.6)')LFIENET,SFIENET*TOINCH
173 C     WRITE(1,*)NXEL,NYEL
174 C     DO 7 J=1,NYEL,1
175 C         Y=YLOCATE(J)*TOINCH
176 C         DO 6 I=1,NXEL,1
177 C             X=XLOCATE(I)*TOINCH
178 C             WRITE(1,('(2(1X,1PG15.6),4(1X,1PG15.6)')X,Y,
179 C             $ REC2POL(DRVCURR(I,J),.FALSE.),
180 C             $ REC2POL(ZDRVIMP(I,J),.FALSE.)
181 C         6 CONTINUE
182 C     7 CONTINUE
183 C     CLOSE(1)
184 C
185 C Draw the dipole array.
186 C
187 C     WRITE(*,*)
188 C     IF(YesNoTF('Do you want to see the array schematic'))THEN
189 C         CALL DRWARA(UNITS,XSIZE,YSIZE,NXEL,NYEL,DIPLNG,DIPTILT,LFILNET,
190 C         $ SFILNET,GNDPLN(2),XLOCATE,YLOCATE,ZDRVIMP,NXELMX)
191 C     ENDIF
192 C
193 C     END

```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling ARAFACT'
4 $SUBTITLE: '    FUNCTION ARAFACT'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION ARAFACT(K0,KDIR,DGNDPLN,XLOCATE,YLOCATE,DRVCURR,NXEL,
8         $ NXELMX,NYEL)
9 C
10 C LAST MODIFIED 1/26/89. BY R. WILSON.
11 C ***** 3/12/89. BY R. WILSON.
12 C     1) ADDED HANDLING OF A GROUND PLANE.
13 C
14 C "ARAFACT" COMPUTES THE ARRAY FACTOR FOR AN "NXEL" BY "NYEL" ARRAY OF
15 C POINT SOURCES. THE ARRAY MAY BE BACKED BY A GROUND PLANE.
16 C
17 C "K0" IS THE FREE SPACE WAVENUMBER.
18 C
19 C "KDIR" IS A UNIT VECTOR OF DIRECTION COSINES SPECIFYING THE DIRECTION
20 C TO THE FIELD POINT IN QUESTION.
21 C
22 C "DGNDPLN" IS THE DISTANCE TO THE GROUND PLANE. THE UNITS FOR "DGNDPLN"
23 C SHOULD BE COMPATIBLE WITH THOSE USED FOR "K0", I.E. K0*DGNDPLN SHOULD
24 C HAVE UNITS OF RADIAN. IF "DGNDPLN" .LE. 0.0 THEN "ARAFACT" ASSUMES THAT
25 C THERE IS NO GROUND PLANE PRESENT.
26 C
27 C "XLOCATE" AND "YLOCATE" ARE ARRAYS SPECIFYING THE X AND Y LOCATIONS,
28 C RESPECTIVELY, OF THE POINT SOURCES. THERE UNITS SHOULD BE COMPATIBLE WITH
29 C THOSE USED FOR "K0", I.E. K0*XLOCATE(.) SHOULD HAVE UNITS OF RADIAN.
30 C
31 C "DRVCURR" IS A TWO DIMENSIONAL ARRAY CONTAINING THE COMPLEX AMPLITUDES OF
32 C EACH OF THE POINT SOURCES.
33 C
34 C "NXEL" AND "NYEL" ARE THE NUMBER OF POINT SOURCES IN THE X AND Y DIRECTION,
35 C RESPECTIVELY. "NXELMX" IS THE ROW DIMENSION OF THE "DRVCURR" IN THE
36 C CALLING ROUTINE.
37 C
38     COMPLEX ARAFACT,DRVCURR(NXELMX,NYEL)
39     REAL XLOCATE(NXEL),YLOCATE(NYEL)
40     REAL KDIR(3),KODIR(2),K0,KXX,KYY
41 C
42 C COMPUTE THE ARRAY FACTOR SUM.
43 C
44     KODIR(1)=K0*KDIR(1)
45     KODIR(2)=K0*KDIR(2)
46     ARAFACT=CMPLX(0.0,0.0)
47     DO 2 J=1,NYEL,1
48         KYY=KODIR(2)*YLOCATE(J)
49         DO 1 I=1,NXEL,1
50             KXX=KODIR(1)*XLOCATE(I)
51             ARAFACT=ARAFACT+DRVCURR(I,J)*CEXP(CMPLX(0.0,(KXX+KYY)))
52     1 CONTINUE
53     2 CONTINUE
54 C
55 C INCLUDE FACTOR TO ACCOUNT FOR A GROUND PLANE.
56 C
57     IF(DGNDPLN .GT. 0.0)THEN
58         ARAFACT=(1.0-CEXP(CMPLX(0.0,-2.0*DGNDPLN*K0*KDIR(3))))*ARAFACT
59     ENDIF
60     RETURN
61     END
```



```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling ARAGAIN'
4 $SUBTITLE: ' SUBROUTINE ARAGAIN'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE ARAGAIN(K0,NUMBEAM,AZBEAM,ELBEAM,PANTILT,DIPLNG,
8 $ DIPTILT,DGNDPLN,XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,DRVCURR,
9 $ ZDRVIMP,GAIN)
10 C
11 C LAST MODIFIED 5/11/89. BY R. WILSON.
12 C
13 C "ARAGAIN" COMPUTES THE GAIN FOR AN "NXEL" BY "NYEL" ARRAY OF DIPOLES. THE
14 C THE ARRAY MAY HAVE MULTIPLE BEAMS AND BE BACKED BY A GROUND PLANE.
15 C
16 C "K0" IS THE FREE SPACE WAVENUMBER OF THE SOURCE.
17 C
18 C "NUMBEAM" IS THE NUMBER OF MAIN BEAMS GENERATED BY THE ARRAY.
19 C
20 C "AZBEAM" AND "ELBEAM" ARE ARRAYS WHICH HOLD THE AZIMUTH AND ELEVATION
21 C ANGLES, RESPECTIVELY, FOR EACH MAIN BEAM. THE ANGLES ARE ASSUMED TO BE IN
22 C DEGREES.
23 C
24 C "PANTILT" IS THE ELEVATION ANGLE OF THE PANEL NORMAL IN DEGREES. WHEN
25 C "PANTILT" IS 0 THE PANEL IS PERPENDICULAR TO THE GROUND.
26 C
27 C "DIPLNG" IS THE LENGTH OF EACH DIPOLE IN THE ARRAY. IT ASSUMED TO BE IN
28 C UNITS CONSISTENT WITH "K0".
29 C
30 C "DIPTILT" IS AN ARRAY CONTAINING A UNIT DIRECTION VECTOR SPECIFYING THE
31 C DIRECTION OF THE DIPOLES IN THE APERTURE PLANE. IT SHOULD BE DIMENSIONED
32 C THREE (3) IN THE CALLING PROGRAM. SINCE THE Z COMPONENT OF "DIPTILT" WILL
33 C ALWAYS BE 0 THE ANGLE OF THE DIPOLES, IN DEGREES, WITH RESPECT TO THE
34 C APERTURE VERTICAL IS STORED IN "DIPTILT(3)".
35 C
36 C "DGNDPLN" IS THE DISTANCE TO THE GROUND PLANE. THE UNITS FOR "DGNDPLN"
37 C SHOULD BE COMPATIBLE WITH THOSE USED FOR "K0", I.E. K0*DGNDPLN SHOULD
38 C HAVE UNITS OF RADIAN. IF "DGNDPLN" .LE. 0.0 THEN "ARAFAC" ASSUMES THAT
39 C THERE IS NO GROUND PLANE PRESENT.
40 C
41 C "XLOCATE" AND "YLOCATE" ARE ARRAYS SPECIFYING THE X AND Y LOCATIONS,
42 C RESPECTIVELY, OF THE POINT SOURCES. THERE UNITS SHOULD BE COMPATIBLE WITH
43 C THOSE USED FOR "K0", I.E. K0*XLOCATE(.) SHOULD HAVE UNITS OF RADIAN.
44 C
45 C "NXEL" AND "NYEL" ARE THE NUMBER OF POINT SOURCES IN THE X AND Y DIRECTION,
46 C RESPECTIVELY. "NXELMX" IS THE ROW DIMENSION OF THE "DRVCURR" IN THE
47 C CALLING ROUTINE.
48 C
49 C "DRVCURR" IS A TWO DIMENSIONAL ARRAY CONTAINING THE COMPLEX AMPLITUDES OF
50 C EACH OF THE POINT SOURCES.
51 C
52 C "ZDRVIMP" IS A TWO DIMENSIONAL COMPLEX ARRAY CONTAINING THE DRIVING POINT
53 C IMPEDANCES FOR EACH OF THE DIPOLES IN THE ANTENNA.
54 C
55 C COMPLEX ARAFACT,DIPPAT,DRVCURR(NXELMX,NYEL),ZDRVIMP(NXELMX,NYEL)
56 C REAL XLOCATE(NXEL),YLOCATE(NYEL)
57 C REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM),GAIN(NUMBEAM)
58 C REAL DIPTILT(3),KBEAM(3),K0
59 C
60 C COMPUTE THE INPUT POWER.
61 C
62 C POWERIN=0.0
63 C DO 1 J=1,NYEL,1
64 C DO 1 I=1,NXEL,1
65 C POWERIN=POWERIN+REAL(ZDRVIMP(I,J))*CABS(DRVCURR(I,J))**2
66 C 1 CONTINUE
67 C
68 C COMPUTE THE GAIN.
69 C

```

```
70      AMPNORM=DIPPM(KO,DIPLNG)
71      AMPNORM=120.0/AMPNORM**2
72      DO 2 I=1,NUMBEAM,1
73          CALL AZEL2K(AZBEAM(I),ELBEAM(I),PANTILT,KBEAM)
74          GAIN(I)=AMPNORM*CABS(DIPPM(KBEAM,DIPTILT)*
75      $      ARAFACT(KO,KBEAM,DGNDPLN,XLOCATE,YLOCATE,DRVCURR,NXEL,
76      $      NXELMX,NYEL))**2/POWERIN
77          GAIN(I)=10.0*ALOG10(GAIN(I))
78      2 CONTINUE
79      RETURN
80      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling ARAPAT'
4 $SUBTITLE: '    SUBROUTINE ARAPAT'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE ARAPAT(K0,NUMBEAM,AZBEAM,ELBEAM,PANTILT,DIPLNG,DIPTILT,
8       $  DGNDPLN,XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,DRVCURR)
9 C
10 C  LAST MODIFIED 11/01/88. BY R. WILSON.
11 C  ***** 3/09/89. BY R. WILSON.
12 C      1) Added handling of multiple beams.
13 C  ***** 4/12/89. BY R. WILSON.
14 C      1) Added handling of a ground plane.
15 C  ***** 7/20/89. BY R. WILSON.
16 C      1) Added trapping of operator data entry errors.
17 C      2) Previously a typing mistake would terminate the program with a
18 C         run-time error message and a return to DOS.
19 C
20 C  "ARAPAT" plots the array AZIMUTH and ELEVATION patterns.
21 C
22     PARAMETER (NPTS=1001)
23     COMPLEX DRVCURR(NXELMX,NYEL),ARAFAC,DIPTAT
24     REAL XLOCATE(NXEL),YLOCATE(NYEL),AMP(NPTS),AZEL(NPTS)
25     REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM)
26     REAL DIPTILT(3),BOXDIR(3),KDIR(3),K0
27     INTEGER OFFSET
28     LOGICAL YESNOTF
29     CHARACTER AXISLBL(2)*80
30     COMMON/LINAXC/MAXDIG
31     COMMON/PLOT88C/IOPORT,MODEL,FACTR
32 C
33 C  Initialize the pattern normalization factor, "AMPNORM", the maximum
34 C  number of digits to the right of the decimal place for the linear axis
35 C  labeling, and the size in inches of the X and Y axes.
36 C
37     AMPNORM=NUMBEAM*NXEL*NYEL*DIPTATM(K0,DIPLNG)
38     IF(DGNDPLN .GT. 0.0)AMPNORM=2.0*AMPNORM
39     MAXDIG=4
40     XSIZE=5.0
41     YSIZE=3.0
42 C
43     1 CONTINUE
44 C
45 C  Initialize the PLOT88 software. For plots on the HP Laser printer or the
46 C  HP7470A plotter the plots are rotated so the Y-axis is along the long edge
47 C  of the paper.
48 C
49     CALL GRAFHRD
50     CALL PLOTS(0,IOPORT,MODEL)
51     CALL COMPLX
52     IF(MODEL.EQ.96 .OR. MODEL.EQ.99)THEN
53         CALL PLOT(1.0,1.0,-3)
54         BOXDIR(1)=1.0
55         BOXDIR(2)=0.0
56         BOXDIR(3)=0.0
57     ELSEIF(MODEL.EQ.20 .OR. MODEL.EQ.62)THEN
58         CALL PLOT(1.0,XSIZE+1.0,-3)
59         BOXDIR(1)=0.0
60         BOXDIR(2)=-1.0
61         BOXDIR(3)=-90.0
62     ENDIF
63 C
64 C  Get the constant elevation angle desired for the azimuth cut.
65 C
66     OFFSET=0
67     DO 2 I=1,NUMBEAM,1
68         CALL NUMCHAR(ELBEAM(I),-2,OFFSET,AXISLBL(1),NCHAR)
69         OFFSET=NCHAR+1
```

```

70      AXISLBL(1)(OFFSET:)=', '
71      2 CONTINUE
72      WRITE(*,100)AXISLBL(1)(1:NCHAR)
73      100 FORMAT(/1X,'Beginning AZIMUTH pattern plot. Please enter the',
74      $ 1X,'ELEVATION angle desired'/1X,'for the cut (ELBeam=',A,'):', '\)
75      READ(*,*,IOSTAT=IOSTAT)ELCON
76      DO WHILE (IOSTAT .NE. 0)
77          CALL READERR
78          WRITE(*,100)AXISLBL(1)(1:NCHAR)
79          READ(*,*,IOSTAT=IOSTAT)ELCON
80      END DO
81      WRITE(*,101)'AZIMUTH'
82      101 FORMAT(/5X,'Please wait - Computing the ',A,' pattern...')
83  C
84  C   Compute the azimuth pattern.
85  C
86      AZELMX=90.0
87      AZELMN=-90.0
88      DAZEL=(AZELMX-AZELMN)/(NPTS-1)
89      DO 3 IPT=1,NPTS,1
90          AZEL(IPT)=(IPT-1)*DAZEL+AZELMN
91          CALL AZEL2K(AZEL(IPT),ELCON,PANTILT,KDIR)
92          AMP(IPT)=CABS(DIPPAT(KDIR,DIPILT))*
93      $      ARAFACT(K0,KDIR,DGNDPLN,XLOCATE,YLOCATE,DRVCURR,NXEL,
94      $      NXELMX,NYEL))
95      3 CONTINUE
96  C
97  C   Plot the db amplitude of the azimuth pattern.
98  C
99      WRITE(*,102)'AZIMUTH'
100     102 FORMAT('+',4X,'Please wait - Generating the ',A,' pattern',
101     $ 1X,'plot... ')
102     CALL DBAMP(AMP,NPTS,1,NPTS,AMPNORM,-30.0,20.0)
103     AXISLBL(1)='Azimuth Angle (degrees)'
104     AXISLBL(2)='Amplitude (dB)'
105     AMAX=0.0
106     AMIN=-30.0
107     ADEL=10.0
108     DAZEL=45.0
109     CALL GRAPH(AZEL,AMP,NPTS,NPTS,1,XSIZE,YSIZE,BOXDIR,AZELMX,AZELMN,
110     $ AMAX,AMIN,DAZEL,ADEL,AXISLBL,1,0)
111  C
112     AXISLBL(1)='Elevation Angle of the Cut='
113     CALL NUMCHAR(ELCON,-5,27,AXISLBL(1),NCHAR)
114     AXISLBL(1)(NCHAR+1:)= ' deg.'
115     XPAGE=-3.2*BOXDIR(2)
116     YPAGE=3.2*BOXDIR(1)
117     CALL SYMBOL(XPAGE,YPAGE,0.12,AXISLBL(1),BOXDIR(3),NCHAR+5)
118     AXISLBL(1)='AmpNorm='
119     WRITE(AXISLBL(1)(9:22),'(1PE14.7)')AMPNORM
120     XPAGE=-3.4*BOXDIR(2)
121     YPAGE=3.4*BOXDIR(1)
122     CALL SYMBOL(XPAGE,YPAGE,0.12,AXISLBL(1),BOXDIR(3),22)
123  C
124  C   If displaying plot on terminal print message on screen telling how
125  C   to proceed, terminate the plot and set up for elevation cut. If
126  C   plotting a hardcopy (e.g. HP Laser printer or HP 7470A plotter) reset
127  C   the plot origin to plot the elevation cut above the azimuth cut.
128  C
129     IF(MODEL.EQ.96 .OR. MODEL.EQ.99)THEN
130         AXISLBL(1)='Strike Any Key To Continue'
131         IF(MODEL .EQ. 96)CALL COLOR(4,IERR)
132         CALL SYMBOL(1.5,4.0,0.12,AXISLBL(1),0.0,26)
133         CALL PLOT(0.0,0.0,-999)
134         CALL COMPLX
135         CALL PLOT(1.0,1.0,-3)
136     ELSE
137         CALL PLOT(YSIZE+1.5,0.0,-3)
138     ENDIF

```

```

139 C
140 C   Get the constant azimuth angle desired for the elevation cut.
141 C
142     OFFSET=0
143     DO 4 I=1,NUMBEAM,1
144         CALL NUMCHAR(AZBEAM(I),-2,OFFSET,AXISLBL(1),NCHAR)
145         OFFSET=NCHAR+1
146         AXISLBL(1)(OFFSET:)=', '
147     4 CONTINUE
148     WRITE(*,103)'+'//CHAR(7),AXISLBL(1)(1:NCHAR)
149 103 FORMAT(A,'Beginning ELEVATION pattern plot. Please enter',
150 $ ' the AZIMUTH angle desired'/1X,'for the cut (AZBeam=',A,'): '\)
151     READ(*,*,IOSTAT=IOSTAT)AZCON
152     DO WHILE (IOSTAT .NE. 0)
153         CALL READERR
154         WRITE(*,103)'0',AXISLBL(1)(1:NCHAR)
155         READ(*,*,IOSTAT=IOSTAT)AZCON
156     END DO
157     WRITE(*,101)'ELEVATION'
158 C
159 C   Compute the elevation pattern.
160 C
161     DO 5 IPT=1,NPTS,1
162         CALL AZEL2K(AZCON,AZEL(IPT),PANTILT,KDIR)
163         AMP(IPT)=CABS(DIPPAT(KDIR,DIPTILT))*
164 $     ARAFACT(KO,KDIR,DGNDPLN,XLOCATE,YLOCATE,DRVCURR,NXEL,
165 $     NXELMX,NYEL))
166     5 CONTINUE
167 C
168 C   Plot the db amplitude of the elevation pattern.
169 C
170     WRITE(*,102)'ELEVATION'
171     CALL DBAMP(AMP,NPTS,1,NPTS,AMPNORM,-30.0,20.0)
172     AXISLBL(1)='Elevation Angle (degrees)'
173     AMAX=0.0
174     AMIN=-30.0
175     ADEL=10.0
176     DAZEL=45.0
177     CALL GRAPH(AZEL,AMP,NPTS,NPTS,1,XSIZE,YSIZE,BOXDIR,AZELMX,AZELMN,
178 $     AMAX,AMIN,DAZEL,ADEL,AXISLBL,1,0)
179 C
180     AXISLBL(1)='Azimuth Angle of the Cut='
181     CALL NUMCHAR(AZCON,-5,25,AXISLBL(1),NCHAR)
182     AXISLBL(1)(NCHAR+1:)= ' deg.'
183     XPAGE=-3.2*BOXDIR(2)
184     YPAGE=3.2*BOXDIR(1)
185     CALL SYMBOL(XPAGE,YPAGE,0.12,AXISLBL(1),BOXDIR(3),NCHAR+5)
186     AXISLBL(1)='AmpNorm='
187     WRITE(AXISLBL(1)(9:22), '(1PE14.7)')AMPNORM
188     XPAGE=-3.4*BOXDIR(2)
189     YPAGE=3.4*BOXDIR(1)
190     CALL SYMBOL(XPAGE,YPAGE,0.12,AXISLBL(1),BOXDIR(3),22)
191 C
192 C   If displaying plot on terminal print message on screen telling how
193 C   to proceed.
194 C
195     IF(MODEL.EQ.96 .OR. MODEL.EQ.99)THEN
196         AXISLBL(1)='Strike Any Key To Continue'
197         IF(MODEL .EQ. 96)CALL COLOR(4,1ERR)
198         CALL SYMBOL(1.5,4.0,0.12,AXISLBL(1),0.0,26)
199         model=-1
200     ENDIF
201 C
202 C   Close PLOT88 file.
203 C
204     CALL CLOSPLT
205 C
206 C   See if another cut is desired.
207 C

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```
208      if(YesNoTF('Do you want to see another cut'))go to 1
209  C
210      RETURN
211      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling AZEL2K'
4 $SUBTITLE: '    SUBROUTINE AZEL2K'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE AZEL2K(AZ,EL,ELTILT,K)
8 C
9 C     LAST MODIFIED 11/01/88. BY R. WILSON.
10 C     ***** 11/02/88. BY R. WILSON.
11 C         1) CHANGED K(3) COMPUTATION TO AVOID PROBLEMS WITH NEGATIVE
12 C             SQUARE ROOT ARGUMENTS RESULTING FROM ROUND OFF ERRORS.
13 C     ***** 11/08/88. BY R. WILSON.
14 C         1) ADDED ROTATING THE COORDINATE SYSTEM IN ELEVATION BY THE
15 C             ANGLE "ELTILT" DEGREES BEFORE EXITING.
16 C     ***** 3/14/89. BY R. WILSON.
17 C         1) ADDED CODE TO MAKE POSITIVE "AZ" TO BE FROM THE POSITIVE "Z"
18 C             AXIS TOWARD THE NEGATIVE "X" AXIS. THIS MAKES THE DEFINITION
19 C             OF AZIMUTH AGREE WITH THE 'SURVEYORS' DEFINITION.
20 C
21 C     "AZEL2K" COMPUTES THE DIRECTION COSINES "KX", "KY", AND "KZ" FOR A VECTOR
22 C     POINTING IN THE DIRECTION SPECIFIED BY "AZ" AND "EL". "AZ" AND "EL" ARE
23 C     ASSUMED TO BE IN DEGREES AND ARE INPUTS TO "AZEL2K". THE COORDINATE SYSTEM
24 C     ASSUMED IS WITH THE "Y-Z" PLANE THE VERTICAL PLANE AND THE "X-Z" PLANE THE
25 C     HORIZONTAL PLANE. "AZ" IS ASSUMED TO BE SPECIFIED IN THE "X-Z" PLANE
26 C     MEASURED FROM THE "Z" AXIS AND POSITIVE MOVING TOWARD THE NEGATIVE "X" AXIS
27 C     (SEE ABOVE). "EL" IS ASSUMED TO BE MEASURED FROM THE "X-Z" PLANE AND
28 C     POSITIVE MOVING TOWARD THE POSITIVE "Y" AXIS. "KX", "KY", AND "KZ" ARE
29 C     RETURNED IN THE VECTOR "K" WITH "K(1)"="KX", "K(2)"="KY" AND "K(3)"="KZ".
30 C     BEFORE RETURNING THE COORDINATE SYSTEM IS ROTATED IN ELEVATION (ABOUT THE X
31 C     AXIS) BY THE ANGLE "ELTILT".
32 C
33 C     REAL K(3),KY,KZ
34 C
35 C     COMPUTE THE DIRECTION COSINES.
36 C
37 C     K(1)=-COSD(EL)*SIND(AZ)
38 C     KY=SIND(EL)
39 C     KZ=COSD(EL)*COSD(AZ)
40 C
41 C     ROTATE THE COORDINATE SYSTEM AROUND THE X AXIS BY "ELTILT" MEASURED FROM
42 C     THE Z AXIS.
43 C
44 C     COSTILT=COSD(ELTILT)
45 C     SINTILT=SIND(ELTILT)
46 C     K(2)=KY*COSTILT-KZ*SINTILT
47 C     K(3)=KY*SINTILT+KZ*COSTILT
48 C     RETURN
49 C     END
```

```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling CSOLVE'
4  $SUBTITLE: '  SUBROUTINE CSOLVE'
5  $PAGE
6  $NOTRUNCATE
7  SUBROUTINE CSOLVE(A,MXDIMA,N,Y,PARPIV,P,X)
8  C
9  C  LAST MODIFIED 12/01/85.  BY R. WILSON.
10 C  ***** 8/30/88.  BY R. WILSON.
11 C      1) CHANGED SMALLNESS TEST IN SEARCHING FOR NON-ZERO ELEMENT IN
12 C         A COLUMN (TEST FOR .LE. EPSILON INSTEAD OF .NE. 0.0)
13 C      2) ADDED CHECK FOR SMALLNESS OF "A(ROW,N)" BEFORE USING AS DIVISOR
14 C         IN BACK SUBSTITUTION.
15 C
16 C  "CSOLVE" COMPUTES THE SOLUTION OF SIMULTANEOUS LINEAR EQUATIONS OF THE FORM
17 C  Y=AX USING GAUSS-JORDAN ELIMINATION WITH AN OPTION TO PARTIAL PIVOTING.
18 C
19 C  DEFINITION OF PARAMETERS.
20 C
21 C  "A" IS THE COMPLEX SYSTEM MATRIX.  THE SYSTEM MATRIX IS ASSUMED TO BE A
22 C  SQUARE MATRIX OF SIZE "N" BY "N".  "CSOLVE" DESTROYS THE "A" MATRIX.  "A" IS
23 C  AN INPUT TO "CSOLVE".
24 C
25 C  "MXDIMA" IS THE ROW DIMENSION OF THE ARRAY IN THE CALLING PROGRAM
26 C  CORRESPONDING TO THE "A" MATRIX.  IT IS ONLY USED IN "CSOLVE" FOR
27 C  DIMENSIONING "A".  "MXDIMA" IS AN INPUT TO "CSOLVE".
28 C
29 C  "N" IS THE NUMBER OF ROWS AND COLUMNS IN THE "A" MATRIX AND THE NUMBER
30 C  OF ROWS IN THE "X" AND "Y" COLUMN VECTORS.  IT MUST BE .LE. "MXDIMA".
31 C  "CSOLVE" CHECKS FOR THIS CONDITION AND TERMINATES THE PROGRAM WITH AN ERROR
32 C  MESSAGE IF IT IS NOT MET.  "N" IS AN INPUT TO "CSOLVE".
33 C
34 C  "Y" IS AN COMPLEX COLUMN ARRAY OF SIZE "N".  IT CORRESPONDS TO THE SYSTEM
35 C  OUTPUT VECTOR.  "CSOLVE" DESTROYS THE "Y" MATRIX.  IT IS AN INPUT TO
36 C  "CSOLVE".
37 C
38 C  "PARPIV" IS A LOGICAL VARIABLE INDICATING WHETHER PARTIAL PIVOTING IS
39 C  TO BE USED.  IF "PARPIV" IS .TRUE. THEN EACH COLUMN IS SEARCHED FOR THE
40 C  MAXIMUM ELEMENT WHEN SELECTING THE PIVOT ELEMENT.  IF "PARPIV" IS .FALSE.
41 C  THE FIRST NON-ZERO ELEMENT IN THE COLUMN IS USED AS THE PIVOT.  "PARPIV" IS
42 C  AN INPUT TO "CSOLVE".
43 C
44 C  "P" IS COLUMN VECTOR OF SIZE "N" USED AS A POINTER VECTOR USED FOR
45 C  EXCHANGING ROWS IN THE ELIMINATION ALGORITHM.  RATHER THAN ACTUALLY MOVING
46 C  DATA AROUND WHEN ROWS ARE EXCHANGED THE CORRESPONDING ELEMENTS IN "P" ARE
47 C  EXCHANGED.  "P" IS INITIALIZED BY "CSOLVE" AND THEN CHANGED BY "CSOLVE" IF
48 C  NECESSARY.  NORMALLY THE CALLING PROGRAM MAKES NO USE OF "P" AFTER CALLING
49 C  "CSOLVE" AND THE CALLING ROUTINE DOES NOT INITIALIZE "P".  "P" IS INCLUDED
50 C  IN THE ARGUMENT LIST SO IT CAN BE AN ADJUSTABLE DIMENSIONED ARRAY.  IN THE
51 C  CALLING PROGRAM "P" SHOULD BE DIMENSIONED "MXDIMA", THAT IS, IT SHOULD HAVE
52 C  THE SAME DIMENSION AS THE ROW DIMENSION OF THE "A" MATRIX.
53 C
54 C  "X" IS A COMPLEX COLUMN VECTOR OF SIZE "N".  IT CORRESPONDS TO THE SYSTEM
55 C  INPUT VECTOR.  IT IS AN OUTPUT FROM "CSOLVE".
56 C
57 C  PARAMETER(EPSILON=1.0E-12)
58 C  COMPLEX A(MXDIMA,N),X(N),Y(N),AM
59 C  INTEGER P(N),ROW,PIVROW
60 C  LOGICAL PARPIV
61 C
62 C  CHECK FOR CORRECT INPUTS.
63 C
64 C  IF(N .GT. MXDIMA)THEN
65 C      CALL BEEP
66 C      WRITE(*,100)N,MXDIMA
67 100  FORMAT(/1X,'***** ERROR - Program terminated in CSOLVE.'/
68 C  $ 7X,'N(=',15,') .GT. MXDIMA(=',15,').')
69 C  STOP

```



```

70      ENDIF
71 C
72 C      INITIALIZE PIVOT POINTER VECTOR, P.
73 C
74      DO 1 I=1,N,1
75          P(I)=I
76      1 CONTINUE
77 C
78 C      UPPER TRIANGULARIZE A MATRIX.
79 C
80      NM1=N-1
81      DO 7 KCOL=1,NM1,1
82          KCOLP1=KCOL+1
83 C
84 C          SEARCH "KCOL" COLUMN OF "A" FROM THE "P(KCOL)"TH ROW TO THE "P(N)"TH
85 C          ROW FOR THE FIRST NON-ZERO ELEMENT.
86 C
87      DO 2 J=KCOL,N,1
88          NZROW=P(J)
89          NZJ=J
90          IF(ABS(A(NZROW,KCOL)) .GE. EPSILON)GO TO 3
91      2 CONTINUE
92      CALL BEEP
93      WRITE(*,101)
94      101 FORMAT(1X,'***** ERROR - program terminated in CSOLVE. /'
95      $      7X,'The "A" matrix is not invertible. ')
96      STOP
97      3 CONTINUE
98      IF(PARPIV)THEN
99 C
100 C          SEARCH "KCOL" COLUMN OF "A" FROM THE "NZROW"-TH ROW TO THE
101 C          "P(N)"-TH ROW FOR THE MAXIMUM ELEMENT.
102 C
103      MAXROW=NZROW
104      MAXPJ=NZJ
105      DO 4 J=NZJ+1,N,1
106          ROW=P(J)
107          IF(ABS(A(ROW,KCOL)) .GT. ABS(A(MAXROW,KCOL)))THEN
108              MAXROW=ROW
109              MAXPJ=J
110          ENDIF
111      4 CONTINUE
112      J=MAXPJ
113      ROW=MAXROW
114      ELSE
115          J=NZJ
116          ROW=NZROW
117      ENDIF
118 C
119 C      NON-ZERO (AND/OR MAXIMUM) ELEMENT FOUND, USE THIS ROW AS PIVOT.
120 C      EXCHANGE "P(KCOL)" WITH "P(J)" IN PIVOT POINTER VECTOR TO FACILITATE
121 C      ARRAY INDEXING LATER
122 C
123      P(J)=P(KCOL)
124      P(KCOL)=ROW
125 C
126 C      CALCULATE PIVOT MULTIPLIER, "AM", AND SET ARRAY ELEMENTS IN COLUMN
127 C      "KCOL" TO AM IF THEY HAVEN'T BEEN USED AS A PIVOT ACCORDING TO PIVOT
128 C      POINTER VECTOR "P".
129 C
130      DO 6 I=KCOLP1,N,1
131          PIVROW=P(KCOL)
132          ROW=P(I)
133          AM=A(ROW,KCOL)/A(PIVROW,KCOL)
134          A(ROW,KCOL)=AM
135 C
136 C      CALCULATE NEW VALUES OF COEFFCIENTS IN COLUMNS "KCOL+1" TO "N" OF
137 C      THE "A" MATRIX AND ROW "P(I)" OF THE "Y" ARRAY.
138 C

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```
139          DO 5 J=KCOLP1,N,1
140              A(ROW,J)=A(ROW,J)-AM*A(PIVROW,J)
141          5      CONTINUE
142              Y(ROW)=Y(ROW)-AM*Y(PIVROW)
143          6      CONTINUE
144          7      CONTINUE
145      C
146      C      SOLVE "TRIANGULARIZED" SYSTEM BY BACK SUBSTITUTION.
147      C
148          ROW=P(N)
149          IF(ABS(A(ROW,N)) .LT. EPSILON)THEN
150              CALL BEEP
151              WRITE(*,101)
152              STOP
153          ENDIF
154          X(N)=Y(ROW)/A(ROW,N)
155          DO 9 I=1,NM1,1
156              NMI=N-I
157              ROW=P(NMI)
158              X(NMI)=Y(ROW)
159              DO 8 J=1,I,1
160                  NMIPJ=NMI+J
161                  X(NMI)=X(NMI)-X(NMIPJ)*A(ROW,NMIPJ)
162          8      CONTINUE
163              X(NMI)=X(NMI)/A(ROW,NMI)
164          9      CONTINUE
165          RETURN
166      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling DIPPATM'
4 $SUBTITLE: '    FUNCTION DIPPATM'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION DIPPATM(K0,DIPLNG)
8 C
9 C   LAST MODIFIED 12/11/88.  BY R. WILSON.
10 C
11 C   "DIPPAT" IS A COMPLEX FUNCTION WHICH COMPUTES THE FAR-FIELD AMPLITUDE IN
12 C   THE DIRECTION "K" OF A DIPOLE OF LENGTH "DIPLNG" WHOSE AXIS IS ALONG THE
13 C   VECTOR "DIPTILT". "DIPPATM" IS THE FIRST ENTRY POINT AND INITIALIZES SOME
14 C   VALUES NEEDED BY THE ENTRY POINT "DIPPAT". "DIPPATM" RETURNS THE VALUE
15 C   OF THE MAGNITUDE OF THE PATTERN AT BROADSIDE.  THE EQUATION IMPLEMENTED IS
16 C   EQ. 4-62A FROM BALANIS, "ANTENNA THEORY - ANALYSIS AND DESIGN", PP. 120.
17 C
18     PARAMETER(PI=3.1415926535898,PIOVER2=PI/2.0,TWOPI=2.0*PI)
19     PARAMETER(ZERO=1.0E-12)
20     COMPLEX DIPPAT,DIPAMP
21     REAL KDIR(3),DIPTILT(3),K0,DIPLNG,FFRAD,KLOVER2
22 C
23 C   INITIALIZE VARIABLES USED BY "DIPPAT".  COMPUTE THE PATTERN MAGNITUDE AT
24 C   "THETA"=90.0 DEGREES.
25 C
26     KLOVER2=K0*DIPLNG/2.0
27     FFRAD=1.0E6
28     ETA=377.0
29     PHASE=-MOD(K0*FFRAD,TWOPI)+PIOVER2
30     COSKL2=COS(KLOVER2)
31     DIPAMP=ETA* CEXP(CMPLX(0.0,PHASE))/(TWOPI*FFRAD)
32     DIPPATM=ETA*(1.0-COSKL2)/(TWOPI*FFRAD)
33     RETURN
34 C
35 C   COMPUTE THE PATTERN IN THE DIRECTION "KBEAM".  NOTE: IT IS ASSUMED THAT
36 C   THE Z-COMPONENT OF THE DIPOLE TILT, "DIPTILT(3)", IS ZERO, SEE "GDTILT".
37 C
38     ENTRY DIPPAT(KDIR,DIPTILT)
39     COSTH=KDIR(1)*DIPTILT(1)+KDIR(2)*DIPTILT(2)
40     SINTH=SQRT(1.0-COSTH**2)
41     IF(ABS(SINTH) .GT. ZERO)THEN
42         DIPPAT=DIPAMP*(COS(KLOVER2*COSTH)-COSKL2)/SINTH
43     ELSE
44         DIPPAT=CMPLX(0.0,0.0)
45     ENDIF
46     RETURN
47     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling DRVNT'
4 $SUBTITLE: ' SUBROUTINE DRVNT'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE DRVNT(LAMBDA,NXEL,NXELMX,NYEL,XLOCATE,YLOCATE,DIPWID,
8 $ DIPLNG,DIPTILT,DGNDPLN,DRVCURR,ZDRVIMP,ZSYSROW,NXYELMX)
9 C
10 C LAST MODIFIED 4/23/89. BY R. WILSON.
11 C ***** 5/08/89. BY R. WILSON.
12 C 1) REMOVED COMPUTATION OF DRIVING POINT VOLTAGES.
13 C ***** 6/06/89. BY R. WILSON.
14 C 1) CORRECTED METHOD OF LOADING IMPEDANCES TO ACCOUNT FOR THE FACT
15 C THAT WHEN THE DIPOLES ARE TILTED (NOT 0 OR 90 DEGREES) THE
16 C IMPEDANCES ARE FUNCTIONS OF SIGN(IVOL-ICUR)*SIGN(JVOL-JCUR) NOT
17 C ABS(IVOL-ICUR)*ABS(JVOL-JCUR).
18 C
19 C "DRVNT" LOADS THE DRIVING POINT IMPEDANCE ARRAY, "ZDRVIMP", FOR AN ARRAY
20 C OF IDENTICAL EQUALLY SPACED DIPOLES. MAXIMUM USE IS MADE OF SYMMETRY,
21 C RESULTING IN IT BEING NECESSARY TO STORE ONLY TWO ROWS OF THE SYSTEM
22 C MATRIX (ONLY NECESSARY TO COMPUTE PART OF THE SECOND ROW).
23 C
24 C "LAMBDA" IS THE WAVELENGTH OF THE SOURCE. THE UNITS OF "LAMBDA" SHOULD
25 C BE CONSISTENT WITH THAT OF ALL OTHER LINEAR DIMENSIONS. IT IS AN INPUT
26 C TO "DRVNT".
27 C
28 C "NXEL" AND "NYEL" ARE THE NUMBER OF DIPOLES ELEMENTS IN THE HORIZONTAL AND
29 C VERTICAL DIRECTIONS RESPECTIVELY. THEY ARE INPUTS TO "DRVNT".
30 C
31 C "NXELMX" IS THE MAXIMUM NUMBER OF DIPOLES ELEMENTS IN THE HORIZONTAL
32 C DIRECTION. IT IS USED MAINLY FOR DIMENSIONING THE ARRAYS "DRVCURR",
33 C AND "ZDRVIMP". IT IS AN INPUT TO "DRVNT".
34 C
35 C "XLOCATE" AND "YLOCATE" ARE ONE DIMENSIONAL ARRAYS CONTAINING THE
36 C HORIZONTAL AND VERTICAL LOCATIONS OF EACH DIPOLE ELEMENT. FOR EXAMPLE, THE
37 C LOCATION OF THE (2,4)TH ELEMENT IN THE ARRAY IS (XLOCATE(2),YLOCATE(4)).
38 C "XLOCATE" AND "YLOCATE" ARE ASSUMED TO HAVE UNITS CONSISTENT WITH ALL OTHER
39 C LINEAR DIMENSIONS. THEY ARE INPUTS TO "DRVNT".
40 C
41 C "DIPWID" IS THE WIDTH OF THE CONDUCTORS MAKING UP EACH DIPOLE IN THE ARRAY.
42 C THE UNITS FOR "DIPWID" SHOULD BE CONSISTENT WITH ALL OTHER LINEAR
43 C DIMENSIONS. "DIPWID" IS AN INPUT TO "DRVNT".
44 C
45 C "DIPLNG" IS THE LENGTH OF EACH DIPOLE IN THE ARRAY. THE UNITS FOR "DIPLNG"
46 C SHOULD BE CONSISTENT WITH ALL OTHER LINEAR DIMENSIONS. "DIPLNG" IS AN
47 C INPUT TO "DRVNT".
48 C
49 C "DIPTILT" IS AN ARRAY CONTAINING A UNIT DIRECTION VECTOR SPECIFYING THE
50 C DIRECTION OF THE DIPOLES IN THE APERTURE PLANE. IT SHOULD BE DIMENSIONED
51 C THREE (3) IN THE CALLING PROGRAM. SINCE THE Z COMPONENT OF "DIPTILT" WILL
52 C ALWAYS BE 0 THE ANGLE OF THE DIPOLES, IN DEGREES WITH RESPECT TO THE
53 C APERTURE VERTICAL IS STORED IN "DIPTILT(3)". "DIPTILT" IS AN INPUT TO
54 C "DRVNT".
55 C
56 C "DGNDPLN", IF .GT. 0.0 SPECIFIES THE DISTANCE FROM THE ARRAY PANEL TO THE
57 C GROUND PLANE. IF "DGNDPLN" IS .LE. 0.0 THEN NO GROUND PLANE IS PRESENT.
58 C THE UNITS FOR "DGNDPLN" SHOULD BE CONSISTENT WITH ALL OTHER LINEAR
59 C DIMENSIONS. "DGNDPLN" IS AN INPUT TO "DRVNT".
60 C
61 C "DRVCURR" IS A TWO DIMENSIONAL COMPLEX ARRAY CONTAINING THE DRIVING POINT
62 C CURRENTS FOR EACH OF THE DIPOLES IN THE ARRAY. IT IS AN INPUT TO "DRVNT".
63 C
64 C "ZSYSROW" IS A COMPLEX ARRAY WHICH HOLDS THE FIRST AND "NXEL"TH ROW OF THE
65 C SYSTEM IMPEDANCE MATRIX. IT IS IN THE ARGUMENT LIST SO THAT ITS SIZE CAN
66 C BE MADE ADJUSTABLE. IT SHOULD BE DIMENSIONED ("NXYELMX",2). IT IS AN
67 C OUTPUT FROM "DRVNT".
68 C
69 C "NXYELMX" IS THE ROW DIMENSION OF "ZSYSROW". IT SHOULD .GE. "NXEL"*"NYEL".
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70 C   IT IS AN INPUT TO "DRV PNT".
71 C
72     COMPLEX ZDRVIMP(NXELMX,NYEL),ZSYSROW(NXYELMX,2)
73     COMPLEX DRVCURR(NXELMX,NYEL),ZGRND,DRVVLT
74     REAL XLOCATE(NXEL),YLOCATE(NYEL),DIPTILT(3),DIPRAD(2)
75     REAL LAMBDAI,LAMBDAI,DIPLNG,DIPLNGW,DIPWID,DGNDPLN
76     LOGICAL UGNDPLN
77 C
78 C   CHECK FOR CORRECT INPUTS.
79 C
80     NXYEL=NXEL*NYEL
81     IF(NXYEL .GT. NXYELMX)THEN
82         CALL BEEP
83         WRITE(*,101)NXYEL,NXYELMX
84 101    FORMAT(/1X,'***** ERROR - program terminated in DRVIMP.'/
85         $      7X,'NXYEL(=',I3,') .GT. NXYELMX(=',I3,').')
86         STOP
87     ENDIF
88 C
89 C   COMPUTE THE DIPOLE RADII, "DIPRAD(I)", FROM THE DIPOLE WIDTHS, "DIPWID"
90 C   (THE CONVERSION FROM THE WIDTH OF A FLAT CONDUCTOR TO AN EQUIVALENT RADIUS
91 C   OF A ROUND CONDUCTOR IS FOUND IN C. A. BALANIS, "ANTENNA THEORY, ANALYSIS
92 C   AND DESIGN", PP. 337-339). NORMALIZE ALL LINEAR DIMENSIONS TO WAVELENGTH,
93 C   "LAMBDA". INITIALIZE "UGNDPLN" AND "ZIMAGE" FOR GROUND PLANE COMPUTATION.
94 C
95     LAMBDAI=1.0/LAMBDA
96     DIPRAD(1)=DIPWID*LAMBDAI*0.25
97     DIPRAD(2)=DIPRAD(1)
98     DIPLNGW=DIPLNG*LAMBDAI
99     DO 1 I=1,NXEL,1
100        XLOCATE(I)=XLOCATE(I)*LAMBDAI
101    1 CONTINUE
102    DO 2 I=1,NYEL,1
103        YLOCATE(I)=YLOCATE(I)*LAMBDAI
104    2 CONTINUE
105    UGNDPLN=DGNDPLN .GT. 0.0
106    ZIMAGE=-2.0*DGNDPLN*LAMBDAI
107 C
108 C   LOAD THE FIRST ROW/COLUMN OF THE SYSTEM IMPEDANCE MATRIX, "ZSYSROW".
109 C   IF A GROUND PLANE IS PRESENT ADJUST FOR ITS EFFECT.
110 C
111     CALL MOM(1,0.0,0.0,0.0,DIPLNGW,DIPLNGW,DIPRAD,ZSYSROW(1,1))
112     IF(UGNDPLN)THEN
113         CALL MOM(2,0.0,ZIMAGE,0.0,DIPLNGW,DIPLNGW,DIPRAD,ZGRND)
114         ZSYSROW(1,1)=ZSYSROW(1,1)-ZGRND
115     ENDIF
116     IF(NXYEL .GT. 1)THEN
117         IF(NXEL.GT.1 .AND. NYEL.GT.1)THEN
118             NUNIQRW=2
119         ELSE
120             NUNIQRW=1
121         ENDIF
122         ICURX=1
123         DO 4 IUNIQRW=1,NUNIQRW,1
124             XCUR=XLOCATE(ICURX)
125             YCUR=YLOCATE(1)
126             DO 3 I=2,NXYEL,1
127                 JVOLY=(I-1)/NXEL+1
128                 IVOLX=I-(JVOLY-1)*NXEL
129                 IF(IUNIQRW.EQ.1 .OR.
130                 $      (IVOLX-ICURX)*(JVOLY-1) .LT. 0)THEN
131                     XDIFF=XLOCATE(IVOLX)-XCUR
132                     YDIFF=YLOCATE(JVOLY)-YCUR
133 C
134 C       ROTATE COORDINATES TO ALLOW "MOM" TO SEGMENT ALONG THE X-AXIS.
135 C
136         XOFFSET=XDIFF*DIPTILT(1)+YDIFF*DIPTILT(2)
137         YOFFSET=-XDIFF*DIPTILT(2)+YDIFF*DIPTILT(1)
138 C

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139 C          COMPUTE THE MUTUAL IMPEDANCE BETWEEN REAL DIPOLES.
140 C
141          CALL MOM(2,YOFFSET,0.0,XOFFSET,DIPLNGW,DIPLNGW,DIPRAD,
142          $      ZSYSROW(I,IUNIQRW))
143 C
144 C          ADJUST THE IMPEDANCE FOR PRESENCE OF A GROUND PLANE.
145 C
146          IF(UGNDPLN)THEN
147              CALL MOM(2,YOFFSET,ZIMAGE,XOFFSET,DIPLNGW,DIPLNGW,
148          $      DIPRAD,ZGRND)
149              ZSYSROW(I,IUNIQRW)=ZSYSROW(I,IUNIQRW)-ZGRND
150          ENDIF
151      ENDIF
152  3      CONTINUE
153          ICURX=NXEL
154  4      CONTINUE
155      ENDIF
156 C
157 C          COMPUTE THE DRIVING POINT VOLTAGES AND DRIVING POINT IMPEDANCES.
158 C          ASSUME ALL DIPOLES ARE IDENTICAL AND SPACING BETWEEN DIPOLES IS
159 C          IDENTICAL.
160 C
161          DO 6 I=1,NXYEL,1
162              JVOLY=(I-1)/NXEL+1
163              IVOLX=1-(JVOLY-1)*NXEL
164              DRVVLTCMPLX(0.0,0.0)
165              DO 5 J=1,NXYEL,1
166                  JCURY=(J-1)/NXEL+1
167                  ICURX=J-(JCURY-1)*NXEL
168                  IDIFX=IVOLX-ICURX
169                  JDIFY=JVOLY-JCURY
170                  IF((IDIFX*JDIFY) .GE. 0)THEN
171                      IFSTROW=ABS(IDIFX)+ABS(JDIFY)*NXEL+1
172                      DRVVLTCMPLX=DRVVLTCMPLX+ZSYSROW(IFSTROW,1)*DRVCURR(ICURX,JCURY)
173                  ELSE
174                      IFSTROW=-ABS(IDIFX)+ABS(JDIFY)*NXEL+NXEL
175                      DRVVLTCMPLX=DRVVLTCMPLX+ZSYSROW(IFSTROW,2)*DRVCURR(ICURX,JCURY)
176                  ENDIF
177              5      CONTINUE
178              ZDRVIMP(IVOLX,JVOLY)=DRVVLTCMPLX/DRVCURR(IVOLX,JVOLY)
179          6      CONTINUE
180 C
181 C          DENORMALIZE THE LOCATION ARRAYS.
182 C
183          DO 7 I=1,NXEL,1
184              XLOCATE(I)=XLOCATE(I)*LAMBDA
185          7      CONTINUE
186          DO 8 I=1,NYEL,1
187              YLOCATE(I)=YLOCATE(I)*LAMBDA
188          8      CONTINUE
189          RETURN
190      END

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1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling DRWARA'
4 $SUBTITLE: '    SUBROUTINE DRWARA'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE DRWARA(UNITS,XSIZE,YSIZE,NXEL,NYEL,DIPLNG,DIPTILT,
8         $ LFILNET,SFILNET,DGNDPLN,XLOCATE,YLOCATE,ZDRVIMP,NXELMX)
9 C
10 C LAST MODIFIED 9/27/88. BY R. WILSON.
11 C ***** 11/08/88. BY R. WILSON.
12 C 1) Added handling of panel tilt.
13 C ***** 11/15/88. BY R. WILSON.
14 C 1) Plotting of title block now handled by "ARATITL".
15 C ***** 11/22/88. BY R. WILSON.
16 C 1) Changed so that if array panel is rectangular the
17 C box representing the panel edge will be rectangular.
18 C ***** 12/11/88. BY R. WILSON.
19 C 1) Added handling of dipole tilt.
20 C ***** 4/04/89. BY R. WILSON.
21 C 1) Added handling of a ground plane.
22 C ***** 8/08/89. BY R. WILSON.
23 C 1) Changed the plotting of the impedance values so that they are
24 C staggered, thus preventing overwriting.
25 C
26 C "DRWARA" draws a scaled version of the dipole array, showing the location
27 C of each dipole.
28 C
29     COMPLEX ZDRVIMP(NXELMX,NYEL)
30     REAL XLOCATE(NXEL),YLOCATE(NYEL),XORIGIN(2),DIPTILT(3)
31     REAL BOXDIR(3),MAXDIM,LBLLLOC
32     INTEGER OFFSET,MAXDIG
33     CHARACTER AXISLBL(2)*80,UNITS*2,LFILNET*1
34     COMMON/LINAXC/MAXDIG
35     COMMON/PLOT88C/IOPORT,MODEL
36 C
37 C Initialize the maximum number of digits to the right of the decimal
38 C place shown on the linear axis labels, "MAXDIG", the size, in inches, of
39 C the X and Y axes, "XSIZEPL" and "YSIZEPL", and the direction vector for
40 C the X axis of the box, "BOXDIR".
41 C
42     MAXDIG=2
43     MAXDIM=MAX(XSIZE,YSIZE)
44     XSIZEPL=5.0*XSIZE/MAXDIM
45     YSIZEPL=5.0*YSIZE/MAXDIM
46     BOXDIR(1)=1.0
47     BOXDIR(2)=0.0
48     BOXDIR(3)=0.0
49 C
50 C Initialize the PLOT88 software.
51 C
52     CALL GRAFHRO
53     CALL PLOTS(0,IOPORT,MODEL)
54     IF(IOPORT.EQ.96 .OR. IOPORT.EQ.99)CALL FACTOR(0.8)
55     CALL COMPLX
56     CALL PLOT(1.5,1.5,-3)
57     WRITE(*,100)
58 100 FORMAT(/5X,'Please wait - generating the array schematic...')
59 C
60 C Draw the outside border of the array.
61 C
62     AXISLBL(1)='X ( '//UNITS//'. )'
63     AXISLBL(2)='Y ( '//UNITS//'. )'
64     DELTAX=XSIZE/2
65     DELTAY=YSIZE/2
66     CALL AXISXY(1,XSIZEPL,YSIZEPL,BOXDIR,XSIZE,0.0,YSIZE,0.0,DELTAX,
67         $ DELTAY,AXISLBL,XSCALE,YSCALE)
68 C
69 C If a ground plane is used plot legend showing its location.

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70 C
71 IF(DGNDPLN .GT. 0.0)THEN
72   AXISLBL(1)='A ground plane is to be used'
73   OFFSET=29
74   CALL NUMCHAR(DGNDPLN,-3,OFFSET,AXISLBL(1),NCHAR)
75   AXISLBL(1)(NCHAR+1:)=UNITS//'. from the array panel'
76   NCHAR=NCHAR+24
77   XPAGE=-(YSIZEPL+0.2)*BOXDIR(2)
78   YPAGE=(YSIZEPL+0.2)*BOXDIR(1)
79   CALL SYMBOL(XPAGE,YPAGE,0.12,AXISLBL(1),BOXDIR(3),NCHAR)
80   ENDIF
81 C
82 C Draw the dipoles.
83 C
84   DIPLNG2=(DIPLNG/2)*XSCALE
85   DIPLNGS=DIPLNG*XSCALE
86   HGHTX=MIN(0.12,DIPLNG2)
87   ANGLE=90.0-DIPTILT(3)
88   DO 1 J=1,NYEL,1
89     XORIGIN(2)=-DIPLNG2*DIPTILT(2)+YLOCATE(J)*YSCALE
90     IF( (J/2)*2 .EQ. J)THEN
91       LBLLOC=-0.2
92       DELTA=-0.2
93     ELSE
94       LBLLOC=-0.4
95       DELTA=0.2
96     ENDIF
97     DO 2 I=1,NXEL,1
98       LBLLOC=LBLLOC+DELTA
99       DELTA=-DELTA
100      XORIGIN(1)=-DIPLNG2*DIPTILT(1)+XLOCATE(I)*XSCALE
101 C
102 C Left end of dipole (assuming horizontal dipoles).
103 C
104   CALL SYMBOL(XORIGIN(1),XORIGIN(2),HGHTX,CHAR(13),ANGLE,-1)
105   CALL PLOT(XORIGIN(1),XORIGIN(2),3)
106 C
107 C Right end of dipole (assuming horizontal dipoles).
108 C
109   XPAGE=DIPLNGS*DIPTILT(1)+XORIGIN(1)
110   YPAGE=DIPLNGS*DIPTILT(2)+XORIGIN(2)
111   CALL PLOT(XPAGE,YPAGE,2)
112   CALL SYMBOL(XPAGE,YPAGE,HGHTX,CHAR(13),ANGLE,-1)
113 C
114 C Indicate the center of the dipole.
115 C
116   XPAGE=DIPLNG2*DIPTILT(1)+XORIGIN(1)
117   YPAGE=DIPLNG2*DIPTILT(2)+XORIGIN(2)
118   CALL SYMBOL(XPAGE,YPAGE,HGHTX,CHAR(4),ANGLE,-1)
119 C
120 C Label with element driving point impedance.
121 C
122   AXISLBL(1)='Z='
123   CALL NUMCHAR(REAL(ZDRVIMP(I,J)),-1,2,AXISLBL(1),NCHAR)
124   AXISLBL(1)(NCHAR+1:)='+j'
125   OFFSET=NCHAR+2
126   CALL NUMCHAR(AIMAG(ZDRVIMP(I,J)),-1,OFFSET,
127   $   AXISLBL(1),NCHAR)
128   IF(AXISLBL(1)(OFFSET+1:OFFSET+1) .EQ. '-')THEN
129     AXISLBL(1)(OFFSET-1:OFFSET+1)='-j'//CHAR(0)
130   ENDIF
131   CALL TITLE(AXISLBL(1),ANGLE,1,LBLLOC,0.1,DIPLNGS,XORIGIN)
132 2 CONTINUE
133 1 CONTINUE
134 C
135 C Show location of the filter network.
136 C
137   AXISLBL(1)='Filter Network'
138   IF(LFILNET .EQ. 'B')THEN

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139      FSPACE=SFILNET*YSCALE
140      CALL PLOT(0.0,FSPACE,3)
141      CALL PLOT(XSIZEPL,FSPACE,2)
142      XORIGIN(1)=0.0
143      XORIGIN(2)=FSPACE/2.0
144      CALL TITLE(AXISLBL(1),0.0,1,0.0,0.12,XSIZEPL,XORIGIN)
145      ELSEIF(LFILNET .EQ. 'T')THEN
146          FSPACE=SFILNET*YSCALE
147          XORIGIN(2)=YSIZEPL-FSPACE
148          CALL PLOT(0.0,XORIGIN(2),3)
149          CALL PLOT(XSIZEPL,XORIGIN(2),2)
150          XORIGIN(1)=0.0
151          XORIGIN(2)=YSIZEPL-FSPACE/2.0
152          CALL TITLE(AXISLBL(1),0.0,1,0.0,0.12,XSIZEPL,XORIGIN)
153      ELSEIF(LFILNET .EQ. 'L')THEN
154          FSPACE=SFILNET*XSCALE
155          CALL PLOT(FSPACE,0.0,3)
156          CALL PLOT(FSPACE,YSIZEPL,2)
157          XORIGIN(1)=FSPACE/2.0
158          XORIGIN(2)=0.0
159          CALL TITLE(AXISLBL(1),90.0,1,0.0,0.12,YSIZEPL,XORIGIN)
160      ELSEIF(LFILNET .EQ. 'R')THEN
161          FSPACE=SFILNET*XSCALE
162          XORIGIN(1)=XSIZEPL-FSPACE
163          CALL PLOT(XORIGIN(1),0.0,3)
164          CALL PLOT(XORIGIN(1),YSIZEPL,2)
165          XORIGIN(1)=XSIZEPL-FSPACE/2.0
166          XORIGIN(2)=0.0
167          CALL TITLE(AXISLBL(1),90.0,-1,0.0,0.12,YSIZEPL,XORIGIN)
168      ENDIF
169  C
170  C If displaying plot on terminal print message on screen telling how
171  C to proceed.
172  C
173      IF(MODEL.EQ.96 .OR. MODEL.EQ.99)THEN
174          AXISLBL(1)='Strike Any Key to Continue'
175          IF(MODEL .EQ. 96)CALL COLOR(4,IERR)
176          call factor(1.0)
177  C      CALL SYMBOL(1.5,-1.25,0.12,AXISLBL(1),0.0,26)
178          call symbol(1.2,-1.0,0.12,AXISLBL(1),0.0,26)
179          model=-1
180      ENDIF
181  C
182  C Close PLOT88 files.
183  C
184      CALL CLOSPLT
185  C
186      RETURN
187      END
```

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1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GDLNGTH'
4 $SUBTITLE: '    SUBROUTINE GDLNGTH'
5 $PAGE
6 $NOTRUNCATE
7   SUBROUTINE GDLNGTH(LAMBDA,NXEL,NYEL,DX,DY,DIPWID,DIPTILT,
8     $ XACTIVE,YACTIVE,DIPLNG)
9 C
10 C  LAST MODIFIED 12/14/88. BY R. WILSON.
11 C  ***** 4/03/89. BY R. WILSON.
12 C      1) CORRECTED ERROR WHICH WAS CAUSED BY "LNGTHX" AND/OR "LNGTHY"
13 C         BEING NEGATIVE. THIS HAPPENED IF "DIPTILT(3)" ENDED IN A QUADRANT
14 C         OTHER THAN THE FIRST.
15 C
16 C  "GDLNGTH" DETERMINES THE LENGTHS OF THE DIPOLES IN THE ARRAY.  "GDLNGTH"
17 C  STANDS FOR Get_Dipole_Length.
18 C
19 C  "LAMBDA" IS THE WAVELENGTH OF THE SOURCE. IT IS AN INPUT TO "GDLNGTH".
20 C
21 C  "NXEL", AND "NYEL" ARE THE NUMBER OF ELEMENTS HORIZONTALLY AND VERTICALLY
22 C  IN THE ARRAY. THEY ARE INPUTS TO "GDLNGTH".
23 C
24 C  "DX" AND "DY" ARE THE HORIZONTAL AND VERTICAL SPACING BETWEEN THE CENTERS
25 C  OF THE DIPOLES IN THE ARRAY. THEY HAVE THE SAME UNITS AS "LAMBDA" AND ARE
26 C  INPUTS TO "GDLNGTH".
27 C
28 C  "DIPWID" IS THE WIDTH OF THE DIPOLES IN THE ARRAY. IT HAS THE SAME UNITS AS
29 C  "LAMBDA" AND IS AN INPUT TO "GDLNGTH".
30 C
31 C  "DIPTILT" IS AN ARRAY CONTAINING A UNIT DIRECTION VECTOR SPECIFYING THE
32 C  DIRECTION OF THE DIPOLES IN THE APERTURE PLANE. SEE "GDTILT" FOR A
33 C  DETAILED DESCRIPTION. "DIPTILT" IS AN INPUT TO "GDLNGTH".
34 C
35 C  "XACTIVE" AND "YACTIVE" ARE THE HORIZONTAL AND VERTICAL LENGTHS OF THE AREA
36 C  OF THE APERTURE WHICH CONTAINS THE DIPOLES. SEE "GFSIZE" FOR A DETAILED
37 C  DESCRIPTION. THEY ARE INPUTS TO "GDLNGTH".
38 C
39 C  "DIPLNG" IS THE LENGTH OF THE DIPOLES IN THE ARRAY. IT HAS THE SAME UNITS
40 C  AS "LAMBDA", ETC. IT IS THE OUTPUT FROM "GDLNGTH".
41 C
42     REAL DIPTILT(3)
43     REAL LAMBDA,LNGTHX,LNGTHY
44 C
45 C  "RESLNG" IS THE APPROXIMATE RESONANT LENGTH FOR DIPOLES WITH WIDTHS AS
46 C  RETURNED BY "DIPWID".
47 C
48     RESLNG=0.465*LAMBDA
49 C
50 C  COMPUTE THE DIPOLE LENGTH.
51 C
52     IF(NXEL .GT. 1)THEN
53         LNGTHX=DX*DIPTILT(1)
54     ELSE
55         LNGTHX=XACTIVE*DIPTILT(1)
56     ENDIF
57     IF(NYEL .GT. 1)THEN
58         LNGTHY=DY*DIPTILT(2)
59     ELSE
60         LNGTHY=YACTIVE*DIPTILT(2)
61     ENDIF
62     DIPLNG=MIN(ABS(LNGTHX)+ABS(LNGTHY)-DIPWID,RESLNG)
63     RETURN
64     END
```

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1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GDTILT'
4 $SUBTITLE: ' SUBROUTINE GDTILT'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GDTILT(DIPTILT)
8 C
9 C LAST MODIFIED 12/11/88. BY R. WILSON.
10 C ***** 4/03/89. BY R. WILSON.
11 C 1) Changed prompt for tilt angle to define the meaning of a positive
12 C tilt angle.
13 C ***** 7/20/89. BY R. WILSON.
14 C 1) Added trapping of operator data entry errors.
15 C 2) Previously a typing mistake would terminate the program with a
16 C run-time error message and a return to DOS.
17 C ***** 9/15/89. BY R. WILSON.
18 C 1) Added "polarity" in parenthesis to the user prompt as suggested by
19 C Joe Zimmerman.
20 C
21 C "GDTILT" prompts for the tilt angle of the dipoles in the array with
22 C respect to the panel vertical. The vector of direction cosines is then
23 C computed and stored in "DIPTILT(1)" and "DIPTILT(2)". The tilt angle
24 C itself is stored in "DIPTILT(3)". "GDTILT"=GetDipoleTILT"
25 C
26 C REAL DIPTILT(3)
27 C
28 C Obtain the desired tilt angle.
29 C
30 C WRITE(*,100)
31 100 FORMAT(/1X,'The dipoles making up the array can be tilted in the',
32 $ 1X,'aperture. At the prompt'/1X,'enter the desired dipole',
33 $ 1X,'tilt angle. The angle should be specified in degrees'/
34 $ 1X,'measured from the vertical. The dipoles will be vertical',
35 $ 1X,'for a 0 degree tilt'/1X,'angle and horizontal for a 90',
36 $ 1X,'degree tilt angle. A positive tilt angle is'/1X,'assumed',
37 $ 1X,'to be in a COUNTER-CLOCKWISE direction when looking in the',
38 $ 1X,'same'/1X,'direction as the array.'//5X,'Enter the desired',
39 $ 1X,'dipole tilt (polarity): '\)
40 READ(*,*,IOSTAT=IOSTAT)DIPTILT(3)
41 DO WHILE (IOSTAT .NE. 0)
42 CALL READERR
43 WRITE(*,100)
44 READ(*,*,IOSTAT=IOSTAT)DIPTILT(3)
45 END DO
46 C
47 C Compute the dipole direction vector.
48 C
49 DIPTILT(1)=SIND(DIPTILT(3))
50 DIPTILT(2)=COSD(DIPTILT(3))
51 RETURN
52 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GDWIDTH'
4 $SUBTITLE: ' SUBROUTINE GDWIDTH'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GDWIDTH(UNITS,LAMBDA,DIPWID)
8 C
9 C LAST MODIFIED 11/17/88. BY R. WILSON.
10 C ***** 5/08/89. BY R. WILSON.
11 C 1) SPLIT OFF CONVERSION TO INCHES INTO A SEPERATE FUNCTION.
12 C ***** 5/11/89. BY R. WILSON.
13 C 1) CHANGED THE VALUES IN "STDWID" TO MORE STANDARD VALUES.
14 C
15 C "GDWIDTH" RETURNS THE DIPOLE WIDTHS, "DIPWID", IN UNITS OF "UNITS". IT IS
16 C CHOSEN FROM A SET OF "STANDARD" WIDTHS CONTAINED IN THE ARRAY "STDWID".
17 C "LAMBDA" IS THE WAVELENGTH OF THE SOURCE IN UNITS OF "UNITS". "GDWIDTH"
18 C STANDS FOR Get_Dipole_WIDTH.
19 C
20 C PARAMETER(NUMWID=6)
21 C REAL STDWID(NUMWID),LAMBDA,DIPWID
22 C CHARACTER UNITS*2
23 C DATA STDWID/0.125,0.25,0.375,0.5,0.75,1.00/
24 C
25 C DETERMINE THE CONDUCTOR WIDTH, "DIPWID", TO BE USED FOR THE DIPOLES.
26 C THE STANDARD WIDTHS, "STDWID", ARE IN INCHES SO COMPUTE THE INITIAL
27 C GUESS IN INCHES.
28 C
29 C DIPWID=UNIT2IN(LAMBDA,UNITS)/120.0
30 C
31 C FIND THE CLOSEST STANDARD WIDTH.
32 C
33 C IF(DIPWID .LE. STDWID(1))THEN
34 C DIPWID=STDWID(1)
35 C ELSEIF(DIPWID .GE. STDWID(NUMWID))THEN
36 C DIPWID=STDWID(NUMWID)
37 C ELSE
38 C DO 1 I=2,NUMWID,1
39 C DELWID2=0.5*(STDWID(I)-STDWID(I-1))
40 C IF(DIPWID .LE. STDWID(I))THEN
41 C IF((DIPWID-STDWID(I-1)) .GT. DELWID2)THEN
42 C DIPWID=STDWID(I)
43 C ELSE
44 C DIPWID=STDWID(I-1)
45 C ENDIF
46 C GO TO 2
47 C ENDIF
48 C 1 CONTINUE
49 C 2 CONTINUE
50 C ENDIF
51 C
52 C CONVERT WIDTH BACK TO UNITS OF "UNITS".
53 C
54 C DIPWID=DIPWID/UNIT2IN(1.0,UNITS)
55 C RETURN
56 C END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GETBEAM'
4 $SUBTITLE: '    SUBROUTINE GETBEAM'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE GETBEAM(MXNBEAM,NUMBEAM,AZBEAM,ELBEAM)
8 C
9 C     LAST MODIFIED 10/18/88. BY R. WILSON.
10 C     ***** 11/01/88. BY R. WILSON.
11 C         1) Changed from using "THBEAM" and "PHIBEAM" (spherical angles)
12 C             to directly using "AZBEAM" and "ELBEAM".
13 C     ***** 3/09/89. BY R. WILSON.
14 C         1) Added handling of multiple beams.
15 C     ***** 3/14/89. BY R. WILSON.
16 C         1) Added protection from specifying duplicate beam positions when
17 C             specifying multiple beams.
18 C     ***** 7/20/89. BY R. WILSON.
19 C         1) Added trapping of operator data entry errors.
20 C         2) Previously a typing mistake would terminate the program with a
21 C             run-time error message and a return to DOS.
22 C
23 C     "GETBEAM" prompts for the desired number of main beams and direction for
24 C     for each of the beams.
25 C
26 C     "MXNBEAM" is the maximum number of beams allowed. It is used as the
27 C     dimension for "AZBEAM" and "ELBEAM" and as the upper limit for "NUMBEAM".
28 C     "MXNBEAM" is an input to "GETBEAM".
29 C
30 C     "NUMBEAM" is the number of main beams desired. "GETBEAM" checks to make
31 C     sure that "NUMBEAM" is at least 1 and no greater than "MXNBEAM". "NUMBEAM"
32 C     is an output from "GETBEAM".
33 C
34 C     "AZBEAM" and "ELBEAM" are arrays which hold the azimuth and elevation
35 C     angles, respectively, for each main beam. The angles are assumed to be in
36 C     degrees. The "AZBEAM(1)" and "ELBEAM(1)" are outputs from "GETBEAM".
37 C
38     REAL AZBEAM(MXNBEAM),ELBEAM(MXNBEAM)
39     INTEGER NUMBEAM
40 C
41 C     Display opening instructions.
42 C
43     WRITE(*,100)
44 100 FORMAT(/1X,'When prompted enter the desired number of beams,',
45     $ 1X,'and the AZIMUTH and ELEVATION'/1X,'angle (in degrees) for',
46     $ 1X,'each beam.')
```

```
47 C
48 C     Get desired number of beams.
49 C
50     NUMBEAM=0
51     DO WHILE (NUMBEAM.LT.1 .OR. NUMBEAM.GT.MXNBEAM)
52         WRITE(*,101)MXNBEAM
53 101    FORMAT(/5X,'Enter desired number of beams (1-',I1,'): '\)
54        READ(*,*,Iostat=Iostat)NUMBEAM
55        DO WHILE (Iostat .NE. 0)
56            CALL READERR
57            WRITE(*,101)MXNBEAM
58            READ(*,*,Iostat=Iostat)NUMBEAM
59        END DO
60        IF(NUMBEAM.GE.1 .AND. NUMBEAM.LE.MXNBEAM)EXIT
61        CALL BEEP
62        WRITE(*,102)MXNBEAM
63 102    FORMAT(/1X,'***** ERROR - Number of beams must be between',
64     $ 1X,'1 and ',I1, '. Try Again.')
```

```
65     END DO
66 C
67 C     Get desired direction of each beam.
68 C
69     DO 3 IBEAM=1,NUMBEAM,1
```

```
70      1  CONTINUE
71      WRITE(*,104)IBEAM
72      104  FORMAT(5X,'Enter desired position of beam #',I1,
73            $  '(AZ,EL): '\)
74      READ(*,*,IOSTAT=IOSTAT)AZBEAM(IBEAM),ELBEAM(IBEAM)
75      DO WHILE (IOSTAT .NE. 0)
76          CALL READERR
77          WRITE(*,104)IBEAM
78          READ(*,*,IOSTAT=IOSTAT)AZBEAM(IBEAM),ELBEAM(IBEAM)
79      END DO
80      C
81      C  Check for duplicate beam positions.
82      C
83          IF(IBEAM .GT. 1)THEN
84              DO 2 J=1,IBEAM-1,1
85                  IF(AZBEAM(IBEAM) .EQ. AZBEAM(J) .AND.
86                     $  ELBEAM(IBEAM) .EQ. ELBEAM(J))THEN
87                      CALL BEEP
88                      WRITE(*,105)
89                      105  FORMAT(/1X,'***** ERROR - You have duplicated a beam',
90                                $  1X,'position. Try again.'/)
91                      GO TO 1
92                  ENDIF
93              2  CONTINUE
94          ENDIF
95      3  CONTINUE
96      RETURN
97      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GETFREQ'
4 $SUBTITLE: ' SUBROUTINE GETFREQ'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GETFREQ(FREQGHZ,FREQ2K0,K0,LAMBDA)
8 C
9 C LAST MODIFIED 8/24/88. BY R. WILSON.
10 C ***** 7/20/89. BY R. WILSON.
11 C 1) Added trapping of operator data entry errors.
12 C 2) Previously a typing mistake would terminate the program with a
13 C run-time error message and a return to DOS.
14 C
15 C PARAMETER(PI=3.1415926535898,TWOPI=2.0*PI)
16 C REAL FREQGHZ,K0,LAMBDA
17 C
18 C Obtain the source frequency.
19 C
20 C WRITE(*,100)
21 100 FORMAT(/1X,'Enter the desired source frequency',
22 $ 1X,'(in GHz): '\)
23 READ(*,*,IOSTAT=IOSTAT)FREQGHZ
24 DO WHILE (IOSTAT.NE. 0)
25 CALL READERR
26 WRITE(*,100)
27 READ(*,*,IOSTAT=IOSTAT)FREQGHZ
28 END DO
29 K0=FREQ2K0*FREQGHZ
30 LAMBDA=TWOPI/K0
31 RETURN
32 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GETGEOM'
4 $SUBTITLE: ' SUBROUTINE GETGEOM'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GETGEOM(UNITS,LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,
8 $ DIPILT,XSIZE,YSIZE,NXEL,NXELMX,NYEL,NYELMX,XLOCATE,YLOCATE,
9 $ DIPWID,DIPLNG,DX,DY,LFILNET,SFILNET,GNDPLN)
10 C
11 C LAST MODIFIED 10/26/88. BY R. WILSON.
12 C ***** 10/27/88. BY R. WILSON.
13 C 1) ADDED CODE TO AUTOMATICALLY DETERMINE THE REQUIRED SPACING
14 C IN X AND Y TO PREVENT GRATING LOBES.
15 C 2) ADDED CODE TO AUTOMATICALLY DETERMINE THE REQUIRED NUMBER ARRAY
16 C ELEMENTS IN X AND Y.
17 C 3) ADDED CODE TO AUTOMATICALLY DETERMINE THE WIDTH OF THE DIPOLES.
18 C THE NEAREST "STANDARD" WIDTH IS USED.
19 C 4) ADDED CODE TO AUTOMATICALLY DETERMINE THE ELEMENT LENGTHS WHICH
20 C WILL FIT WITHIN THE CALCULATED SPACING.
21 C ***** 11/01/88. BY R. WILSON.
22 C 1) CHANGED FROM USING "THBEAM" AND "PHIBEAM" (SPHERICAL ANGLES) TO
23 C DIRECTLY USING "AZBEAM" AND "ELBEAM".
24 C ***** 11/08/88. BY R. WILSON.
25 C 1) ADDED HANDLING OF PANEL TILT.
26 C ***** 3/09/89. BY R. WILSON.
27 C 1) ADDED HANDLING OF MULTIPLE BEAMS.
28 C ***** 4/04/89. BY R. WILSON.
29 C 1) ADDED HANDLING OF A GROUND PLANE.
30 C ***** 4/25/89. BY R. WILSON.
31 C 1) MOVED CODE FOR CHOSING NUMBER OF ELEMENTS AND THEIR SPACING TO
32 C "GNMEL".
33 C 2) MOVED CODE FOR COMPUTING ELEMENT LOCATIONS TO "GLOCATE".
34 C ***** 5/08/89. BY R. WILSON.
35 C 1) CHANGED "REQUIRED ARRAY SIZE TOO BIG" ERROR MESSAGE.
36 C 2) INSTEAD OF TERMINATING ON THIS ERROR NOW GO BACK AND ASK FOR SIZE.
37 C ***** 5/16/89. BY R. WILSON.
38 C 1) ADDED COMPENSATION FOR NON-AIR SPACER MATERIAL IN THE
39 C COMPUTED VALUE OF THE GROUND PLANE DISTANCE.
40 C 2) TWO DISTANCES ARE NOW COMPUTED, "GDNDPLD", AND "DGNDPLA".
41 C ***** 6/21/89. BY R. WILSON.
42 C 1) CHANGED TO USING AN ARRAY, "GNDPLN", TO HOLD THE TWO GROUND PLANE
43 C DISTANCES AND ADDED THE SPACER DIELECTRIC CONSTANT AS THE THIRD
44 C VALUE STORED IN "GNDPLN".
45 C
46 C "GETGEOM" PROMPTS THE USER FOR THE DESIRED MAXIMUM SIZE OF THE ARRAY AND
47 C THE LOCATION OF THE FILTER NETWORK. FROM THIS INFORMATION AND THE BEAM
48 C DIRECTION INPUT TO "GETGEOM" IT COMPUTES THE NUMBER OF DIPOLES NEEDED IN
49 C THE ARRAY, THE ELEMENT SPACING, AN ADJUSTED ARRAY SIZE, AND THE (X,Y)
50 C LOCATIONS OF EACH DIPOLE IN THE ARRAY. THE DIPOLE WIDTHS AND LENGTHS ARE
51 C THEN DETERMINED.
52 C
53 C DESCRIPTION OF PARAMETERS
54 C
55 C "UNITS" IS A CHARACTER VARIABLE CONTAINING THE UNITS USED FOR LENGTHS
56 C AND POSITION. IT IS PROMPTED FOR BY "GETUNIT". IT IS AN INPUT TO
57 C "GETGEOM".
58 C
59 C "LAMBDA" IS THE WAVELENGTH OF THE SOURCE. THE UNITS FOR "LAMBDA" (AS FOR
60 C ALL LENGTHS IS) "UNITS". IT IS AN INPUT TO "GETGEOM".
61 C
62 C "NUMBEAM" IS THE NUMBER OF BEAMS FOR THIS DESIGN. IT IS AN INPUT TO
63 C "GETGEOM".
64 C
65 C "AZBEAM" AND "ELBEAM" ARE ARRAYS HOLDING THE AZIMUTH AND ELEVATION ANGLE
66 C FOR EACH BEAM IN DEGREES. THEY ARE INPUTS TO "GETGEOM".
67 C
68 C "PANTILT" IS THE ELEVATION ANGLE OF THE PANEL NORMAL IN DEGREES. WHEN
69 C "PANTILT" IS 0 THE PANEL IS PERPENDICULAR TO THE GROUND. IT IS AN OUTPUT
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70 C FROM "GETGEOM".
71 C
72 C "DIPTILT" IS AN ARRAY CONTAINING A UNIT DIRECTION VECTOR SPECIFYING THE
73 C DIRECTION OF THE DIPOLES IN THE APERTURE PLANE. IT SHOULD BE DIMENSIONED
74 C THREE (3) IN THE CALLING PROGRAM. SINCE THE Z COMPONENT OF "DIPTILT" WILL
75 C ALWAYS BE 0 THE ANGLE OF THE DIPOLES, IN DEGREES, WITH RESPECT TO THE
76 C APERTURE VERTICAL IS STORED IN "DIPTILT(3)". "DIPTILT" IS AN OUTPUT FROM
77 C "GETGEOM"
78 C
79 C "XSIZE" AND "YSIZE" ARE THE HORIZONTAL AND VERTICAL DIMENSIONS OF THE
80 C ARRAY. THE USER IS PROMPTED FOR THESE DIMENSIONS. "GETGEOM" THEN
81 C DETERMINES THE NUMBER AND SIZES OF THE DIPOLES, CENTERING THE ACTIVE AREA
82 C OF THE ARRAY WITHIN THE AREA DEFINED BY "XSIZE" AND "YSIZE". "XSIZE" AND
83 C "YSIZE" ARE ASSUMED TO HAVE BEEN ENTERED IN THE UNITS CONTAINED IN "UNITS".
84 C THEY ARE OUTPUTS FROM "GETGEOM".
85 C
86 C "NXEL" AND "NYEL" ARE THE NUMBER OF DIPOLE ELEMENTS IN THE HORIZONTAL AND
87 C VERTICAL DIRECTIONS RESPECTIVELY. THEY ARE DETERMINED BY "GETGEOM" SO AS
88 C TO HAVE THE ARRAY FIT WITHIN THE SPECIFIED AREA (SPECIFIED BY "XSIZE" AND
89 C "YSIZE"). THEY ARE OUTPUTS FROM "GETGEOM".
90 C
91 C "NXELMX" AND "NYELMX" ARE THE UPPER BOUNDS ON "NXEL" AND "NYEL"
92 C RESPECTIVELY. THEY ARE ALSO THE DIMENSION OF THE ARRAYS IN THE CALLING
93 C PROGRAM CORRESPONDING TO "XLOCATE" AND "YLOCATE". THEY ARE INPUTS TO
94 C "GETGEOM".
95 C
96 C "XLOCATE" AND "YLOCATE" ARE ONE DIMENSIONAL ARRAYS CONTAINING THE
97 C HORIZONTAL AND VERTICAL LOCATIONS OF EACH DIPOLE ELEMENT. FOR EXAMPLE, THE
98 C LOCATION OF THE (2,4)TH ELEMENT IN THE ARRAY IS (XLOCATE(2),YLOCATE(4)).
99 C "XLOCATE" AND "YLOCATE" ARE ASSUMED TO HAVE THE UNITS OF "UNITS". THEY ARE
100 C OUTPUTS FROM "GETGEOM".
101 C
102 C "DIPWID" IS THE WIDTH OF THE CONDUCTORS MAKING UP EACH DIPOLE IN THE ARRAY.
103 C SEE "GDWIDTH" FOR DETAILS. "DIPWID" IS AN OUTPUT FROM "GETGEOM".
104 C
105 C "DIPLNG" IS THE LENGTH IN UNITS OF "UNITS" OF EACH DIPOLE IN THE ARRAY.
106 C IT IS AN OUTPUT FROM "GETGEOM".
107 C
108 C "DX" AND "DY" ARE THE HORIZONTAL AND VERTICAL SPACING IN UNITS OF "UNITS"
109 C BETWEEN THE CENTERS OF THE DIPOLES IN THE ARRAY. THEY ARE OUTPUTS FROM
110 C "GETGEOM".
111 C
112 C "LFILNET" IS A ONE CHARACTER VARIABLE INDICATING THE DESIRED LOCATION OF
113 C THE FILTER NETWORK ON THE MYLAR. SEE "GFILNET" FOR POSSIBLE VALUES AND
114 C THEIR DESCRIPTION. "LFILNET" IS AN OUTPUT FROM "GETGEOM".
115 C
116 C "SFILNET" IS THE PERPENDICULAR DISTANCE, IN UNITS OF "UNITS", FROM THE
117 C "LFILNET" EDGE OF THE MYLAR SPECIFYING THE SIZE OF THE SPACE REQUIRED FOR
118 C THE FILTER NETWORK. "SFILNET" IS AN OUTPUT FROM "GETGEOM".
119 C
120 C "GNDPLN" IS A THREE ELEMENT REAL ARRAY HOLDING PARAMETERS FOR DESIGN OF A
121 C GROUND PLANE. IF A GROUND PLANE IS TO BE USED, "GNDPLN(1)" IS THE
122 C ELECTRICAL DISTANCE TO THE GROUND PLANE THROUGH THE DIELECTRIC OF THE
123 C SPACER MATERIAL. "GNDPLN(2)" IS THE PHYSICAL DISTANCE TO THE GROUND PLANE.
124 C UNITS FOR "GNDPLN(1)" AND "GNDPLN(2)" ARE THE SAME AS THE UNITS FOR
125 C "LAMBDA". "GNDPLN(3)" STORES THE DIELECTRIC CONSTANT OF THE SPACER
126 C MATERIAL BETWEEN THE ARRAY PANEL AND THE GROUND PLANE. IF A GROUND PLANE
127 C IS NOT DESIRED "GNDPLN(1)" AND "GNDPLN(2)" ARE SET LESS THAN ZERO,
128 C "GNDPLN(3)" WILL BE UNDEFINED. "GNDPLN(.)" ARE OUTPUTS FROM "GETGEOM".
129 C
130 C     REAL XLOCATE(NXELMX),YLOCATE(NYELMX)
131 C     REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM)
132 C     REAL DIPTILT(3),GNDPLN(3),LAMBDA
133 C     LOGICAL YESNOTF
134 C     CHARACTER UNITS*2,LFILNET*1
135 C
136 C OBTAIN THE DESIRED PANEL ELEVATION TILT.
137 C
138 C     CALL GPTILT(PANTILT)

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139 C
140 C OBTAIN THE DESIRED DIPOLE TILT ANGLES, THE "TILT OF THE LINEAR
141 C POLARIZATION".
142 C
143 C CALL GDTILT(DIPTILT)
144 C
145 C GET THE DESIRED LOCATION OF THE MATCHING NETWORK.
146 C
147 C CALL GFILNET(LAMBDA,DIPTILT(3),LFILNET,SFILNET)
148 C
149 C DETERMINE THE CONDUCTOR WIDTH, "DIPWID", TO BE USED FOR THE DIPOLES.
150 C
151 C CALL GDWIDTH(UNITS,LAMBDA,DIPWID)
152 C
153 C DETERMINE IF A GROUND PLANE IS DESIRED AND, IF SO, ITS LOCATION.
154 C
155 C CALL GGNDPLN(LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,GNDPLN)
156 C
157 C OBTAIN THE DESIRED MAXIMUM SIZE OF THE ARRAY.
158 C
159 C 1 continue
160 C CALL GSIZE(UNITS,LFILNET,SFILNET,XSIZE,XACTIVE,YSIZE,YACTIVE)
161 C
162 C COMPUTE THE NUMBER OF ELEMENTS IN THE ARRAY AND THE ELEMENT SPACING.
163 C
164 C CALL GNUMEL(LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,XACTIVE,
165 C $ YACTIVE,NXEL,NYEL,DX,DY)
166 C
167 C CHECK IF NUMBER OF ELEMENTS IS ALLOWED.
168 C
169 C IF(NXEL.GT.NXELMX .OR. NYEL.GT.NYELMX)THEN
170 C CALL BEEP
171 C WRITE(*,100)NXEL,NYEL,NXELMX,NYELMX
172 100 FORMAT(/1X,'***** ERROR - The required array is too big.'/
173 C $ 7X,'To meet your specifications the array requires ',I3,
174 C $ 1X,'elements horizontally'/7X,'and ',I3,' elements',
175 C $ 1X,'vertically. The maximum size antenna currently allowed'/
176 C $ 7X,'is ',I3,' by ',I3,'. To continue you must decrease the',
177 C $ 1X,'size of the array'/7X,'panel.'/)
178 C GO TO 1
179 C ENDIF
180 C
181 C write(*,*)
182 C write(*,*)'The actual array size is ',XSIZE,' by ',YSIZE
183 C write(*,*)'The active array size is ',xactive,' by ',yactive
184 C write(*,101)nxel,nyel
185 101 FORMAT(1X,'There are',I3,' elements HORIZONTALLY and ',I3,
186 C $ 1X,'elements VERTICALLY')
187 C write(*,*)' HORIZONTAL spacing=',dx,' VERTICAL spacing=',dy
188 C if(.not.(YesNoTF('Is this OK'))go to 1
189 C
190 C LOAD LOCATION ARRAYS "XLOCATE" AND "YLOCATE".
191 C
192 C CALL GLOCATE(NXEL,NYEL,DX,DY,XACTIVE,YACTIVE,LFILNET,
193 C $ SFILNET,XLOCATE,YLOCATE)
194 C
195 C DETERMINE THE LENGTHS OF THE DIPOLES IN THE ARRAY.
196 C
197 C CALL GDLNGTH(LAMBDA,NXEL,NYEL,DX,DY,DIPWID,DIPTILT,XACTIVE,
198 C $ YACTIVE,DIPLNG)
199 C RETURN
200 C END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GETUNIT'
4 $SUBTITLE: '    SUBROUTINE GETUNIT'
5 $PAGE
6 $NOTRUNCATE
7   SUBROUTINE GETUNIT(UNITS,FREQ2K0)
8   C
9   C   LAST MODIFIED  8/24/88.  BY R. WILSON.
10  C   *****      8/03/89.  BY R. WILSON.
11  C       1) Changed selection method from typing letters in parenthesis to
12  C         numbers alongside the choice.
13  C       2) Re-ordered the choices so that English units come first, then
14  C         metric units. The smallest units in each group come first then
15  C         the largest. This was done at the suggestion of Joe Zimmerman,
16  C         et. al. at the meeting the end of July 1989.
17  C
18  C   PARAMETER(PI=3.1415926535898,TWOPI=2.0*PI)
19  C   CHARACTER ICHOICE*1,UNITS*2
20  C
21  C   Obtain the units desired for the linear dimensions of the array,"UNITS".
22  C   Initialize the frequency to wavenumber conversion parameter, "FREQ2K0".
23  C
24  C   1 CONTINUE
25  C   WRITE(*,100)
26  C   100 FORMAT(/1X,'Please specify the units you want to use for',
27  C     $ 1X,'the array size and element'/1X,'position from one of the',
28  C     $ 1X,'following: '//20X,'0 - inches,'/20X,'1 - feet,'/
29  C     $ 20X,'2 - centimeters,'/20X,'3 - meters.'//
30  C     $ 1X,'Make your selection by entering the number corresponding',
31  C     $ 1X,'to your choice.'//1X,'I want to use: '\)
32  C   READ(*,'(A1)',END=1)ICHOICE
33  C   SELECT CASE (ICHOICE)
34  C     CASE ('0')
35  C       UNITS(1:2)='in'
36  C       FREQ2K0=TWOPI*2.54/29.97925
37  C     CASE ('1')
38  C       UNITS(1:2)='ft'
39  C       FREQ2K0=TWOPI*30.48/29.97925
40  C     CASE ('2')
41  C       UNITS(1:2)='cm'
42  C       FREQ2K0=TWOPI/29.97925
43  C     CASE ('3')
44  C       UNITS(1:2)='m'
45  C       FREQ2K0=TWOPI/0.2997925
46  C     CASE DEFAULT
47  C       CALL BEEP
48  C       WRITE(*,101)
49  C   101   FORMAT(/1X,'***** ERROR - incorrect units choice. Re-read',
50  C     $      1X,'the instructions and try again.'/)
51  C   GO TO 1
52  C   END SELECT
53  C   RETURN
54  C   END
```

```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling GFILNET'
4  $SUBTITLE: '    SUBROUTINE GFILNET'
5  $PAGE
6  $NOTRUNCATE
7      SUBROUTINE GFILNET(LAMBDA,DIPTILT,LFILNET,SFILNET)
8  C
9  C  LAST MODIFIED 11/17/88. BY R. WILSON.
10 C  ***** 4/04/89. BY R. WILSON.
11 C      1) Changed prompt for filter network location so that only "L" and
12 C         "R" are allowed for  $0 < \text{ABS}(\text{"DIPTILT"}) < 45$ , and "T" and "B" only
13 C         are allowed for  $45 < \text{ABS}(\text{"DIPTILT"}) < 90$ . "DIPTILT" can be any
14 C         angle, however, before the above criterion is applied "DIPTILT"
15 C         adjusted so that  $0 < \text{ABS}(\text{"DIPTILT"}) < 90$ . Note that "DIPTILT" is
16 C         not RETURNED changed by the routine.
17 C
18 C  "GFILNET" first prompts for the desired location of the filter network on
19 C  the array panel. It then initializes the size of the space on the array
20 C  panel to be left for the filter network. "GFILNET" stands for Get_Filter_
21 C  Network.
22 C
23 C  "LAMBDA" is the wavelength of the radiation. It is an input to "GFILNET".
24 C
25 C  "DIPTILT" is the tilt angle of the dipoles in degrees. It is used to
26 C  determine the allowed locations of the filter network. Unlike in other
27 C  routines, where "DIPTILT" is an array, here "DIPTILT" is a single number.
28 C  in fact it is equal to "DIPTILT(3)" in the other routines. "DIPTILT" is an
29 C  input to "GFILNET".
30 C
31 C  The location is returned in the character variable "LFILNET". Valid values
32 C  for "LFILNET" are: T - FOR THE TOP EDGE
33 C                     B - FOR THE BOTTOM EDGE
34 C                     L - FOR THE LEFT EDGE
35 C                     R - FOR THE RIGHT EDGE
36 C  "LFILNET" is returned upper case, however, the user can respond with either
37 C  upper or lower case. "GFILNET" does the conversion to upper case.
38 C  "LFILNET" is an output from "GFILNET".
39 C
40 C  The space for the filter network is returned in "SFILNET". Whether this
41 C  dimension will be along the X direction or the Y direction will depend on
42 C  the desired location of the filter network. "SFILNET" is an output from
43 C  "GFILNET".
44 C
45      REAL LAMBDA,SFILNET
46      CHARACTER LFILNET*1
47 C
48 C  Initialize size of the space to be left for the filter network, "SFILNET".
49 C
50      SFILNET=0.5*LAMBDA
51 C
52 C  Adjust the tilt angle, if necessary, so that  $0 < \text{DIPTLT} < 90.0$ 
53 C
54      DIPTLT=ABS(DIPTILT)
55      IF(DIPTLT .GT. 90.0)DIPTLT=180.0-DIPTLT
56 C
57 C  Get the desired location of the filter network, "LFILNET".
58 C
59      IF(DIPTLT .LT. 45.0)THEN
60          1  CONTINUE
61          WRITE(*,100)
62      100  FORMAT(/1X,'Space must be left for the filter network along',
63              $ 1X,'the'//20X,'(L)eft edge, or'//20X,'(R)ight edge'//
64              $ 1X,'of the array panel. Indicate your choice by typing the',
65              $ 1X,'corresponding letter'//1X,'shown in parenthesis.',
66              $ 1X,'I want: '\)
67          READ(*,'(A1)')LFILNET
68          CALL UPPER(LFILNET,1)
69          IF(LFILNET.NE.'L' .AND. LFILNET.NE.'R')THEN

```

```
70          CALL BEEP
71          WRITE(*,101)
72 101      FORMAT(/1X,'***** ERROR - incorrect choice. Re-read the',
73          $      1X,'instructions and try again.'/)
74          GO TO 1
75      ENDIF
76  ELSE
77  2      CONTINUE
78          WRITE(*,102)
79 102      FORMAT(/1X,'Space must be left for the filter network along',
80          $      1X,'the'//20X,'(T)op edge, or'//20X,'(B)ottom edge'//
81          $      1X,'of the array panel. Indicate your choice by typing the',
82          $      1X,'corresponding letter'//1X,'shown in parenthesis.',
83          $      1X,'I want: '\)
84          READ(*,'(A1)')LFILNET
85          CALL UPPER(LFILNET,1)
86          IF(LFILNET.NE.'T' .AND. LFILNET.NE.'B')THEN
87              CALL BEEP
88              WRITE(*,101)
89              GO TO 2
90      ENDIF
91  ENDIF
92  RETURN
93  END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GGNDPLN'
4 $SUBTITLE: ' SUBROUTINE GGNDPLN'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GGNDPLN(LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,GNDPLN)
8 C
9 C LAST MODIFIED 4/04/89. BY R. WILSON.
10 C ***** 5/16/89. BY R. WILSON.
11 C 1) Added compensation for non-air spacer material in the
12 C computed value of the ground plane distance.
13 C 2) Two distances are now computed, "DGNDPLD", and "DGNDPLA".
14 C ***** 6/12/89. BY R. WILSON.
15 C 1) Changed references to mylar in prompts to array substrate.
16 C ***** 6/21/89. BY R. WILSON.
17 C 1) Changed to using an array, "GNDPLN", to hold the two ground plane
18 C distances and added the spacer dielectric constant as the third
19 C value stored in "GNDPLN".
20 C ***** 7/20/89. BY R. WILSON.
21 C 1) Added trapping of operator data entry errors.
22 C 2) Previously a typing mistake would terminate the program with a
23 C run-time error message and a return to DOS.
24 C ***** 9/15/89. BY R. WILSON.
25 C 1) Added listing for dielectric constant of polystyrene to the prompt
26 C as suggested by Joe Zimmerman.
27 C
28 C "GGNDPLN" determines if a ground plane is desired and, if so, computes
29 C the distance to the ground plane.
30 C
31 C "LAMBDA" is the wavelength of the source. The units for "LAMBDA" are
32 C the units for "GNDPLN(1)" and "GNDPLN(2)". It is an input to "GGNDPLN".
33 C
34 C "NUMBEAM" is the number of beams for this design. It is an input to
35 C "GGNDPLN".
36 C
37 C "AZBEAM" and "ELBEAM" are arrays holding the AZIMUTH and ELEVATION angle
38 C for each beam in degrees. They are inputs to "GGNDPLN".
39 C
40 C "PANTILT" is the ELEVATION angle of the panel normal in degrees. When
41 C "PANTILT" is 0 the panel is perpendicular to the ground. It is an input
42 C to "GGNDPLN".
43 C
44 C "GNDPLN" is a three element real array holding parameters for design of a
45 C ground plane. If a ground plane is to be used, "GNDPLN(1)" is the
46 C electrical distance to the ground plane through the dielectric of the
47 C spacer material. "GNDPLN(2)" is the physical distance to the ground plane.
48 C Units for "GNDPLN(1)" and "GNDPLN(2)" are the same as the units for
49 C "LAMBDA". "GNDPLN(3)" stores the dielectric constant of the spacer
50 C material between the array panel and the ground plane. If a ground plane
51 C is not desired "GNDPLN(1)" and "GNDPLN(2)" are set less than zero,
52 C "GNDPLN(3)" will be undefined "GNDPLN(.)" are outputs from "GGNDPLN".
53 C
54 REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM),KBEAM(3),GNDPLN(3)
55 REAL LAMBDA,LAMBDA4,PANTILT
56 LOGICAL UGNDPLN,YESNOTF
57 C
58 C Determine if a ground plane is desired.
59 C
60 WRITE(*,*)
61 UGNDPLN=YESNOTF('Do you want to use a ground plane')
62 C
63 C Compute the distance to the ground plane.
64 C
65 GNDPLN(1)=-1.0
66 GNDPLN(2)=-1.0
67 IF(UGNDPLN)THEN
68 WRITE(*,100)
69 100 FORMAT(/5X,'Please enter the dielectric constant of the',
```

```
70      $      1X,'SPACER material'/5X,'between the array substrate and',
71      $      1X,'ground plane'/5X,'(typically 1.033 for polystyrene): '\)
72      READ(*,*,IOSTAT=IOSTAT)GNDPLN(3)
73      DO WHILE (IOSTAT .NE. 0)
74          CALL READERR
75          WRITE(*,100)
76          READ(*,*,IOSTAT=IOSTAT)GNDPLN(3)
77      END DO
78      GNDPLN(1)=0.0
79      GNDPLN(2)=0.0
80      LAMBDA4=LAMBDA/4.0
81      DO 1 IBEAM=1,NUMBEAM,1
82          CALL AZEL2K(AZBEAM(IBEAM),ELBEAM(IBEAM),PANTILT,KBEAM)
83          GNDPLN(1)=GNDPLN(1)+LAMBDA4/KBEAM(3)
84          GNDPLN(2)=GNDPLN(2)+LAMBDA4/SQRT(GNDPLN(3)+KBEAM(3)**2-1)
85      1      CONTINUE
86      GNDPLN(1)=GNDPLN(1)/NUMBEAM
87      GNDPLN(2)=GNDPLN(2)/NUMBEAM
88      ENDIF
89      RETURN
90      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GLOCATE'
4 $SUBTITLE: ' SUBROUTINE GLOCATE'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GLOCATE(NXEL,NYEL,DX,DY,XACTIVE,YACTIVE,LFILNET,
8 $ SFILNET,XLOCATE,YLOCATE)
9 C
10 C LAST MODIFIED 4/26/89. BY R. WILSON.
11 C
12 C "GLOCATE" LOADS THE HORIZONTAL AND VERTICAL (X AND Y) COORDINATES FOR
13 C THE CENTERS OF EACH DIPOLE ELEMENT IN A PLANAR ARRAY.
14 C
15 C "NXEL" AND "NYEL" ARE THE NUMBER OF DIPOLE ELEMENTS IN THE HORIZONTAL AND
16 C VERTICAL DIRECTIONS RESPECTIVELY. THEY ARE INPUT TO "GLOCATE".
17 C
18 C "DX" AND "DY" ARE THE HORIZONTAL AND VERTICAL SPACING BETWEEN THE CENTERS
19 C OF THE DIPOLES IN THE ARRAY. THEIR DIMENSIONS SHOULD BE CONSISTENT WITH
20 C THE DIMENSIONS OF "XACTIVE", "YACTIVE", AND "SFILNET". THEY ARE INPUTS TO
21 C "GLOCATE".
22 C
23 C "XACTIVE" AND "YACTIVE" ARE THE HORIZONTAL AND VERTICAL DIMENSIONS,
24 C RESPECTIVELY, OF THE ACTIVE AREA OF THE ARRAY PANEL. THAT IS, THE AREA OF
25 C THE PANEL WHICH ACTUALLY CONTAINS THE DIPOLES. THEIR DIMENSIONS SHOULD BE
26 C CONSISTENT WITH THE DIMENSIONS OF "DX", "DY", AND "SFILNET". THEY ARE
27 C INPUTS TO "GLOCATE".
28 C
29 C "LFILNET" IS A ONE CHARACTER VARIABLE INDICATING THE DESIRED LOCATION OF
30 C THE FILTER NETWORK ON THE MYLAR. SEE "GFILNET" FOR POSSIBLE VALUES AND
31 C THEIR DESCRIPTION. "LFILNET" IS AN INPUT TO "GLOCATE".
32 C
33 C "SFILNET" IS THE PERPENDICULAR DISTANCE FROM THE "LFILNET" EDGE OF THE
34 C MYLAR SPECIFYING THE SIZE OF THE SPACE REQUIRED FOR THE FILTER NETWORK.
35 C ITS DIMENSION SHOULD BE CONSISTENT WITH THE DIMENSIONS OF "DX", "DY",
36 C "XACTIVE", AND "YACTIVE". "SFILNET" IS AN INPUT TO "GLOCATE".
37 C
38 C "XLOCATE" AND "YLOCATE" ARE ONE DIMENSIONAL ARRAYS CONTAINING THE
39 C HORIZONTAL AND VERTICAL LOCATIONS OF EACH DIPOLE ELEMENT. FOR EXAMPLE, THE
40 C LOCATION OF THE (2,4)TH ELEMENT IN THE ARRAY IS (XLOCATE(2),YLOCATE(4)).
41 C THE CENTERS ARE CHOSEN SO AS TO CENTER THE ELEMENTS WITHIN THE AREA DEFINED
42 C BY "XACTIVE" AND "YACTIVE". THEIR DIMENSIONS ARE ASSUMED TO BE THOSE OF
43 C "DX", "DY", "XACTIVE", "YACTIVE", AND "SFILNET". "XLOCATE" AND "YLOCATE"
44 C ARE OUTPUTS FROM "GLOCATE".
45 C
46 REAL XLOCATE(NXEL),YLOCATE(NYEL)
47 CHARACTER*1 LFILNET
48 C
49 C LOAD THE LOCATION ARRAYS "XLOCATE" AND "YLOCATE".
50 C
51 XLOCATE(1)=(XACTIVE-(NXEL-1)*DX)/2.0
52 IF(LFILNET.EQ. 'L')XLOCATE(1)=XLOCATE(1)+SFILNET
53 YLOCATE(1)=(YACTIVE-(NYEL-1)*DY)/2.0
54 IF(LFILNET.EQ. 'B')YLOCATE(1)=YLOCATE(1)+SFILNET
55 DO 1 I=1,NXEL,1
56 XLOCATE(I)=(I-1)*DX+XLOCATE(1)
57 1 CONTINUE
58 DO 2 I=1,NYEL,1
59 YLOCATE(I)=(I-1)*DY+YLOCATE(1)
60 2 CONTINUE
61 RETURN
62 END
```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GNUMEL'
4 $SUBTITLE: ' SUBROUTINE GNUMEL '
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GNUMEL(LAMBDA,NUMBEAM,AZBEAM,ELBEAM,PANTILT,XACTIVE,
8 $ YACTIVE,NXEL,NYEL,DX,DY)
9 C
10 C LAST MODIFIED 4/26/89. BY R. WILSON.
11 C
12 C "GNUMEL" DETERMINES THE NUMBER OF ELEMENTS IN AN ARRAY AND THEIR SPACING
13 C SUCH THAT GRATING LOBES ARE PREVENTED.
14 C
15 C "LAMBDA" IS THE WAVELENGTH OF THE SOURCE. THE DIMENSIONS FOR "LAMBDA"
16 C DETERMINE THE DIMENSIONS ASSUMED FOR "DX" AND "DY". "LAMBDA" IS AN
17 C INPUT TO "GNUMEL".
18 C
19 C "NUMBEAM" IS THE NUMBER OF BEAMS FOR THIS DESIGN. IT IS AN INPUT TO
20 C "GNUMEL".
21 C
22 C "AZBEAM" AND "ELBEAM" ARE ARRAY HOLDING THE AZIMUTH AND ELEVATION ANGLE
23 C FOR EACH BEAM IN DEGREES. THEY ARE INPUTS TO "GNUMEL".
24 C
25 C "PANTILT" IS THE ELEVATION ANGLE OF THE PANEL NORMAL IN DEGREES. WHEN
26 C "PANTILT" IS 0 THE PANEL IS PERPENDICULAR TO THE GROUND. IT IS AN INPUT
27 C TO "GNUMEL".
28 C
29 C "XACTIVE" AND "YACTIVE" ARE THE HORIZONTAL AND VERTICAL DIMENSIONS,
30 C RESPECTIVELY, OF THE ACTIVE AREA OF THE ARRAY PANEL. THAT IS, THE AREA OF
31 C PANEL WHICH ACTUALLY CONTAINS THE DIPOLES. THEIR DIMENSIONS SHOULD BE THE
32 C SAME AS FOR "LAMBDA". "XACTIVE" AND "YACTIVE" ARE INPUTS TO "GNUMEL".
33 C
34 C "NXEL" AND "NYEL" ARE THE NUMBER OF DIPOLE ELEMENTS IN THE HORIZONTAL AND
35 C VERTICAL DIRECTIONS, RESPECTIVELY. THEY ARE CHOSEN BY "GNUMEL" TO PREVENT
36 C GRATING LOBES. THEY ARE OUTPUTS FROM "GNUMEL".
37 C
38 C "DX" AND "DY" ARE THE HORIZONTAL AND VERTICAL SPACING, RESPECTIVELY,
39 C BETWEEN THE CENTERS OF THE DIPOLES IN THE ARRAY. THEIR DIMENSIONS ARE
40 C ASSUMED TO BE THE SAME AS THE DIMENSIONS OF "LAMBDA". THEY ARE CHOSEN
41 C BY "GNUMEL" TO PREVENT GRATING LOBES. THEY ARE OUTPUTS FROM "GNUMEL".
42 C
43 REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM)
44 REAL DIPTILT(3),K(3),LAMBDA,KX,KY
45 C
46 C COMPUTE THE NUMBER OF ELEMENTS IN THE ARRAY AND THE ELEMENT SPACING.
47 C
48 CALL AZEL2K(AZBEAM(1),ELBEAM(1),PANTILT,K)
49 KX=ABS(K(1))
50 KY=ABS(K(2))
51 NXEL=INT(XACTIVE*(1.0+KX)/LAMBDA+1.0)
52 DX=(1.0-1.0/NXEL)*LAMBDA/(1.0+KX)
53 NYEL=INT(YACTIVE*(1.0+KY)/LAMBDA+1.0)
54 DY=(1.0-1.0/NYEL)*LAMBDA/(1.0+KY)
55 IF(NUMBEAM.GT. 1)THEN
56 DO 1 IBEAM=2,NUMBEAM,1
57 CALL AZEL2K(AZBEAM(IBEAM),ELBEAM(IBEAM),PANTILT,K)
58 KX=ABS(K(1))
59 KY=ABS(K(2))
60 NEL=INT(XACTIVE*(1.0+KX)/LAMBDA+1.0)
61 DEL=(1.0-1.0/NEL)*LAMBDA/(1.0+KX)
62 IF(DEL.LT. DX)THEN
63 DX=DEL
64 NXEL=NEL
65 ENDIF
66 NEL=INT(YACTIVE*(1.0+KY)/LAMBDA+1.0)
67 DEL=(1.0-1.0/NEL)*LAMBDA/(1.0+KY)
68 IF(DEL.LT. DY)THEN
69 DY=DEL
```

```
70          NYEL=NEL
71          ENDIF
72      1      CONTINUE
73          ENDIF
74          RETURN
75          END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GPTILT'
4 $SUBTITLE: ' SUBROUTINE GPTILT'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GPTILT(PANTILT)
8 C
9 C LAST MODIFIED 11/17/88. BY R. WILSON.
10 C ***** 7/20/89. BY R. WILSON.
11 C 1) Added trapping of operator data entry errors.
12 C 2) Previously a typing mistake would terminate the program with a
13 C run-time error message and a return to DOS.
14 C
15 REAL PANTILT
16 C
17 C "GPTILT" prompts for the desired panel tilt in degrees and returns it in
18 C "PANTILT". "GPTILT"= GetPanelTILT.
19 C
20 WRITE(*,100)
21 100 FORMAT(/1X,'The panel containing the array may be tilted in',
22 $ 1X,'elevation. At the prompt'/1X,'specify the desired panel',
23 $ 1X,'tilt by entering the elevation angle of the panel'/
24 $ 1X,'normal.'//5X,'Enter desired panel tilt (in degrees): '\)
25 READ(*,*,IOSTAT=IOSTAT)PANTILT
26 DO WHILE (IOSTAT.NE. 0)
27 CALL READERR
28 WRITE(*,100)
29 READ(*,*,IOSTAT=IOSTAT)PANTILT
30 END DO
31 RETURN
32 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GRAFHRD'
4 $SUBTITLE: '    SUBROUTINE GRAFHRD'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE GRAFHRD
8 C
9 C     LAST MODIFIED 3/28/89. BY R. WILSON.
10 C     ***** 7/20/89. BY R. WILSON.
11 C         1) Added trapping of operator data entry errors.
12 C         2) Previously a typing mistake would terminate the program with a
13 C             run-time error message and a return to DOS.
14 C
15 C     "GRAFHRD" prompts for the desired graphics output device and initializes
16 C     "IOPORT" and "MODEL" for use with "PLOTS".
17 C
18     CHARACTER*1 ICHOICE
19     COMMON/PLOT88C/IOPORT,MODEL,FACTR
20 C
21 C     Get the desired hardcopy device.
22 C
23     1 CONTINUE
24     WRITE(*,100)
25     100 FORMAT(/1X,'Graphics can be displayed on the following devices: '//
26 $ 20X,'0 - an EGA monochrome display, '/
27 $ 20X,'1 - an IBM CGA display, '/
28 $ 20X,'2 - an HP 7470A plotter, or'/
29 $ 20X,'3 - an HP LaserJet printer.'//1X,'Please enter the number',
30 $ 1X,'corresponding to your choice: '\)
31     READ(*,'(A1)',END=1)ICHOICE
32     SELECT CASE (ICHOICE)
33     CASE ('0')
34         IOPORT=96
35         MODEL=96
36     CASE ('1')
37         IOPORT=99
38         MODEL=99
39     CASE ('2')
40         IOPORT=9600
41         MODEL=20
42     CASE ('3')
43         IOPORT=0
44         MODEL=62
45     CASE DEFAULT
46         CALL BEEP
47         WRITE(*,101)
48     101     FORMAT(/1X,'***** ERROR - incorrect choice. Try again. '//)
49         GO TO 1
50     END SELECT
51     RETURN
52     END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling G$IZE'
4 $SUBTITLE: '    SUBROUTINE G$IZE'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE G$IZE(UNITS,LFILNET,SFILNET,XSIZE,YACTIVE,
8         $ YSIZE,YACTIVE)
9 C
10 C LAST MODIFIED 11/17/88. BY R. WILSON.
11 C ***** 11/29/88. BY R. WILSON.
12 C     1) Moved computation of "XACTIVE" and "YACTIVE" here.
13 C     2) Added protection against specifying too small a panel size.
14 C ***** 7/20/89. BY R. WILSON.
15 C     1) Added trapping of operator data entry errors.
16 C     2) Previously a typing mistake would terminate the program with a
17 C         run-time error message and a return to DOS.
18 C
19     REAL XSIZE,YSIZE
20     CHARACTER UNITS*2,LFILNET*1
21 C
22 C "G$IZE" prompts for the desired horizontal and vertical dimensions of the
23 C array panel.
24 C
25 C "UNITS" is a two character variable which contains the units currently in
26 C use for linear dimensions. See "GETUNIT" for allowed values. "UNITS" is
27 C an input to "G$IZE".
28 C
29 C "LFILNET" is a one character variable which indicates the desired location
30 C of the filter network. See "GFILNET" for allowed values. "LFILNET" is an
31 C input to "G$IZE".
32 C
33 C "SFILNET" is the space in units of "UNITS" on the array "PANEL" for the
34 C filter network. "SFILNET" is computed in "GFILNET". It is an input to
35 C "G$IZE".
36 C
37 C The horizontal dimension is returned in "XSIZE" and the vertical dimension
38 C is returned in "YSIZE". "XSIZE" and "YSIZE" include the space to be left
39 C for the filter network. They are in units of "units" and are outputs from
40 C "G$IZE".
41 C
42 C "XACTIVE" and "YACTIVE" are the horizontal and vertical dimensions,
43 C respectively, of the active area of the array panel. That is, the area of
44 C the panel which actually contains the dipoles. They are outputs from
45 C "G$IZE".
46 C
47     WRITE(*,100)
48     100 FORMAT(/1X,'At the prompt enter the desired dimensions for the',
49         $ 1X,'array panel, including the /1X,'filter network. The',
50         $ 1X,'array will be centered within this area after leaving'/
51         $ 1X,'space for the filter network.')

```

```
70      DO WHILE (IOSTAT .NE. 0)
71          CALL READERR
72          WRITE(*,102)UNITS
73          READ(*,*,IOSTAT=IOSTAT)YSIZE
74      END DO
75  ENDIF
76  IF(LFILNET.EQ.'T' .OR. LFILNET.EQ.'B')THEN
77      XACTIVE=XSIZE
78      YACTIVE=YSIZE-SFILNET
79      IF(YACTIVE .LE. 0.0)THEN
80          CALL BEEP
81          WRITE(*,103)SFILNET,UNITS
82  103      FORMAT(/1X,'***** ERROR - your specified VERTICAL',
83          $      1X,'dimension is too small. The filter'/7X,'network',
84          $      1X,'requires at least ',F8.3,1X,A2,'. Try again.'/)
85          GO TO 1
86      ENDIF
87  ELSE
88      XACTIVE=XSIZE-SFILNET
89      YACTIVE=YSIZE
90      IF(XACTIVE .LE. 0.0)THEN
91          CALL BEEP
92          WRITE(*,104)SFILNET,UNITS
93  104      FORMAT(/1X,'***** ERROR - your specified HORIZONTAL',
94          $      1X,'dimension is too small. The filter'/7X,'network',
95          $      1X,'requires at least ',F8.3,1X,A2,'. Try again.'/)
96          GO TO 1
97      ENDIF
98  ENDIF
99  RETURN
100  END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GSUBSTR'
4 $SUBTITLE: ' SUBROUTINE GSUBSTR'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GSUBSTR(UNITS,ERSUB,THSUB)
8 C
9 C LAST MODIFIED 5/08/89. BY R. WILSON.
10 C ***** 6/12/89. BY R. WILSON.
11 C 1) Changed name of subroutine from "GMYLAR" to "GSUBSTR".
12 C 2) This reflects the change in the prompts from references to mylar
13 C To references to array substrate.
14 C ***** 7/20/89. BY R. WILSON.
15 C 1) Added trapping of operator data entry errors.
16 C 2) Previously a typing mistake would terminate the program with a
17 C run-time error message and a return to DOS.
18 C ***** 9/15/89. BY R. WILSON.
19 C 1) Added display of the dielectric constant for Teflon glass and Mylar
20 C to the prompts at the suggestion of Joe Zimmerman.
21 C
22 C "GSUBSTR" prompts for the array substrate dielectric constant, "ERSUB",
23 C and thickness, "THSUB". The thickness is assumed to be in units of
24 C "UNITS".
25 C
26 CHARACTER UNITS*2
27 C
28 C Get the dielectric constant and thickness of the array substrate.
29 C
30 WRITE(*,100)
31 100 FORMAT(/1X,'In order to design the filter network the',
32 $ 1X,'dielectric constant and thickness'/1X,'of the SUBSTRATE',
33 $ 1X,'must be specified. Please enter these values at the',
34 $ 1X,'prompts.'/1X,'(Teflon glass= 2.76 Mylar=2.25)')
35 WRITE(*,101)
36 101 FORMAT(/5X,'Enter substrate DIELECTRIC CONSTANT: '\)
37 READ(*,*,IOSTAT=IOSTAT)ERSUB
38 DO WHILE (IOSTAT.NE. 0)
39 CALL READERR
40 WRITE(*,101)
41 READ(*,*,IOSTAT=IOSTAT)ERSUB
42 END DO
43 WRITE(*,102)' ',UNITS
44 102 FORMAT(A,4X,'Enter substrate THICKNESS (in ',A2,'.): '\)
45 READ(*,*,IOSTAT=IOSTAT)THSUB
46 DO WHILE (IOSTAT.NE. 0)
47 CALL READERR
48 WRITE(*,102)'0',UNITS
49 READ(*,*,IOSTAT=IOSTAT)THSUB
50 END DO
51 RETURN
52 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling KING1'
4 $SUBTITLE: ' SUBROUTINE KING1'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE KING1(D,H,RL1,RL2,ZR,ZX)
8 C
9 C Written by Mike Guler
10 C LAST MODIFIED 02-10-89
11 C
12 PARAMETER (PI=3.1415926535898,B=2.*PI)
13 REAL U(18),SI(18),CI(18)
14 HM1=H-RL1
15 HP1=H+RL1
16 HP2=H+RL2
17 HPT2=H+2.*RL2
18 HM12=H-RL1+RL2
19 HP12=H+RL1+RL2
20 HM1T2=HPT2-RL1
21 HP1T2=HPT2+RL1
22 C
23 C
24 CALL SQROOT(D,HM1,U(1),U(2))
25 CALL SQROOT(D,HP1,U(4),U(3))
26 CALL SQROOT(D,HM12,U(5),U(6))
27 CALL SQROOT(D,HP12,U(8),U(7))
28 CALL SQROOT(D,HM1T2,U(9),U(10))
29 CALL SQROOT(D,HP1T2,U(12),U(11))
30 CALL SQROOT(D,H,U(14),U(13))
31 CALL SQROOT(D,HP2,U(16),U(15))
32 CALL SQROOT(D,HPT2,U(18),U(17))
33 C
34 C
35 DO 10 I=1,18
36 CALL SIC1(U(I),SI(I),CI(I))
37 10 CONTINUE
38 C
39 C
40 COS1=COS(B*HM1)
41 SIN1=-SIN(B*HM1)
42 COS2=COS(B*HP1)
43 SIN2=SIN(B*HP1)
44 COS3=COS(B*HM1T2)
45 SIN3=-SIN(B*HM1T2)
46 COS4=COS(B*HP1T2)
47 SIN4=SIN(B*HP1T2)
48 COS5=COS(B*RL1)
49 C SIN5=SIN(B*RL1)
50 COS6=COS(B*H)
51 SIN6=SIN(B*H)
52 COS7=COS(B*HPT2)
53 SIN7=SIN(B*HPT2)
54 C
55 C
56 T1A=COS1*(CI(1)+CI(2)-CI(5)-CI(6))
57 T1B=SIN1*(-SI(1)+SI(2)+SI(5)-SI(6))
58 T2A=COS2*(CI(3)+CI(4)-CI(7)-CI(8))
59 T2B=SIN2*(-SI(3)+SI(4)+SI(7)-SI(8))
60 T3A=COS3*(-CI(5)-CI(6)+CI(9)+CI(10))
61 T3B=SIN3*(SI(5)-SI(6)-SI(9)+SI(10))
62 T4A=COS4*(-CI(7)-CI(8)+CI(11)+CI(12))
63 T4B=SIN4*(SI(7)-SI(8)-SI(11)+SI(12))
64 T5A=2.*COS5*COS6*(-CI(13)-CI(14)+CI(15)+CI(16))
65 T5B=2.*COS5*SIN6*(SI(13)-SI(14)-SI(15)+SI(16))
66 T6A=2.*COS5*COS7*(CI(15)+CI(16)-CI(17)-CI(18))
67 T6B=2.*COS5*SIN7*(-SI(15)+SI(16)+SI(17)-SI(18))
68 C
69 ZR=15*(T1A+T1B+T2A+T2B+T3A+T3B+T4A+T4B+T5A+T5B+T6A+T6B)
```



```
70 C
71 C
72 T1A=COS1*(-SI(1)-SI(2)+SI(5)+SI(6))
73 T1B=SIN1*(-CI(1)+CI(2)+CI(5)-CI(6))
74 T2A=COS2*(-SI(3)-SI(4)+SI(7)+SI(8))
75 T2B=SIN2*(-CI(3)+CI(4)+CI(7)-CI(8))
76 T3A=COS3*(SI(5)+SI(6)-SI(9)-SI(10))
77 T3B=SIN3*(CI(5)-CI(6)-CI(9)+CI(10))
78 T4A=COS4*(SI(7)+SI(8)-SI(11)-SI(12))
79 T4B=SIN4*(CI(7)-CI(8)-CI(11)+CI(12))
80 T5A=2.*COS5*COS6*(SI(13)+SI(14)-SI(15)-SI(16))
81 T5B=2.*COS5*SIN6*(CI(13)-CI(14)-CI(15)+CI(16))
82 T6A=2.*COS5*COS7*(-SI(15)-SI(16)+SI(17)+SI(18))
83 T6B=2.*COS5*SIN7*(-CI(15)+CI(16)+CI(17)-CI(18))
84 C
85 ZX=15*(T1A+T1B+T2A+T2B+T3A+T3B+T4A+T4B+T5A+T5B+T6A+T6B)
86 C
87 RETURN
88 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling KING2'
4 $SUBTITLE: '    SUBROUTINE KING2'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE KING2(H,RL1,RL2,ZR,ZX)
8 C
9 C     Written by Mike Guler
10 C     LAST MODIFIED 02-09-89
11 C
12     PARAMETER (PI=3.1415926535898,B=2.*PI)
13     REAL U(9),SI(9),CI(9)
14     HM1=H-RL1
15     HP1=H+RL1
16     HP2=H+RL2
17     HPT2=H+2.*RL2
18     HM12=H-RL1+RL2
19     HP12=H+RL1+RL2
20     HM1T2=HPT2-RL1
21     HP1T2=HPT2+RL1
22 C
23 C
24     U(1)=2.*B*HM1
25     U(2)=2.*B*HP1
26     U(3)=2.*B*HM12
27     U(4)=2.*B*HP12
28     U(5)=2.*B*HM1T2
29     U(6)=2.*B*HP1T2
30     U(7)=2.*B*H
31     U(8)=2.*B*HP2
32     U(9)=2.*B*HPT2
33 C
34 C
35     DO 10 I=1,9
36         CALL SICI(U(I),SI(I),CI(I))
37 10 CONTINUE
38 C
39 C
40     COS1=COS(B*HM1)
41     SIN1=SIN(B*HM1)
42     COS2=COS(B*HP1)
43     SIN2=SIN(B*HP1)
44     COS3=COS(B*HM1T2)
45     SIN3=SIN(B*HM1T2)
46     COS4=COS(B*HP1T2)
47     SIN4=SIN(B*HP1T2)
48     COS5=COS(B*RL1)
49 C     SIN5=SIN(B*RL1)
50     COS6=COS(B*H)
51     SIN6=SIN(B*H)
52     COS7=COS(B*HP2)
53     SIN7=SIN(B*HP2)
54 C
55 C
56     RLOG1=LOG(HM12/HM1)
57     RLOG2=LOG(HP12/HP1)
58     RLOG3=LOG(HM12/HM1T2)
59     RLOG4=LOG(HP12/HP1T2)
60     RLOG5=LOG(H/HP2)
61     RLOG6=LOG(HPT2/HP2)
62 C
63 C
64     T1=COS1*(CI(1)-CI(3)+RLOG1)+SIN1*(SI(1)-SI(3))
65     T2=COS2*(CI(2)-CI(4)+RLOG2)+SIN2*(SI(2)-SI(4))
66     T3=COS3*(CI(5)-CI(3)+RLOG3)+SIN3*(SI(5)-SI(3))
67     T4=COS4*(CI(6)-CI(4)+RLOG4)+SIN4*(SI(6)-SI(4))
68     T5=2.*(COS5*COS6*(CI(8)-CI(7)+RLOG5)+COS5*SIN6*(SI(8)-SI(7)))
69     T6=2.*(COS5*COS7*(CI(8)-CI(9)+RLOG6)+COS5*SIN7*(SI(8)-SI(9)))
```

```
70 C
71 ZR=15.*(T1+T2+T3+T4+T5+T6)
72 C
73 C
74 T1=SIN1*(CI(1)-CI(3)-RLOG1)+COS1*(SI(3)-SI(1))
75 T2=SIN2*(CI(2)-CI(4)-RLOG2)+COS2*(SI(4)-SI(2))
76 T3=SIN3*(CI(5)-CI(3)-RLOG3)+COS3*(SI(3)-SI(5))
77 T4=SIN4*(CI(6)-CI(4)-RLOG4)+COS4*(SI(4)-SI(6))
78 T5=2.*(COS5*SIN6*(CI(8)-CI(7)-RLOG5)+COS5*COS6*(SI(7)-SI(8)))
79 T6=2.*(COS5*SIN7*(CI(8)-CI(9)-RLOG6)+COS5*COS7*(SI(9)-SI(8)))
80 C
81 ZX=15.*(T1+T2+T3+T4+T5+T6)
82 C
83 RETURN
84 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling LDCURNT'
4 $SUBTITLE: ' SUBROUTINE LDCURNT'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE LDCURNT(KO,XLOCATE,YLOCATE,NXEL,NXELMX,NYEL,NUMBEAM,
8 $ AZBEAM,ELBEAM,PANTILT,DRVCURR)
9 C
10 C LAST MODIFIED 10/18/88. BY R. WILSON
11 C ***** 11/01/88. BY R. WILSON.
12 C 1) CHANGED FROM USING "THBEAM" AND "PHIBEAM" (SPHERICAL ANGLES)
13 C TO DIRECTLY USING "AZBEAM" AND "ELBEAM".
14 C ***** 11/08/88. BY R. WILSON.
15 C 1) ADDED HANDLING OF PANEL TILT.
16 C ***** 3/09/88. BY R. WILSON.
17 C 1) ADDED HANDLING OF MULTIPLE BEAMS.
18 C
19 C "LDCURNT" COMPUTES THE DRIVING POINT CURRENTS FOR A TWO DIMENSIONAL ARRAY
20 C REQUIRED TO POINT THE MAIN BEAM IN THE DIRECTION ("AZBEAM","ELBEAM").
21 C
22 C DESCRIPTION OF PARAMETERS
23 C
24 C "KO" IS THE FREE SPACE WAVENUMBER. IT IS AN INPUT TO "LDCURNT".
25 C
26 C "XLOCATE" AND "YLOCATE" ARE ONE-DIMENSIONAL ARRAYS DESCRIBING THE POSITION
27 C OF EACH OF THE DIPOLES. FOR EXAMPLE, THE X, Y LOCATION OF THE (2,4)TH
28 C ELEMENT IS (XLOCATE(2),YLOCATE(4)). THE UNITS ARE ASSUMED TO BE COMPATIBLE
29 C WITH "KO". IF "KO" IS IN RADIANS/METER THEN THE UNITS OF "XLOCATE" AND
30 C "YLOCATE" ARE METERS. (THIS IS TAKEN CARE OF AUTOMATICALLY BY "GETGEOM").
31 C "XLOCATE" AND "YLOCATE" ARE INPUTS TO "LDCURNT".
32 C
33 C "NXEL" AND "NYEL" ARE THE NUMBER OF DIPOLES ALONG X AND Y RESPECTIVELY.
34 C "NXELMX" IS THE MAXIMUM POSSIBLE NUMBER OF DIPOLES ALONG THE "X" AXIS.
35 C THIS PARAMETER IS NEEDED IN THE CALL FOR DIMENSIONING THE TWO DIMENSIONAL
36 C ARRAYS.
37 C
38 C "NUMBEAM" IS THE NUMBER OF BEAMS DESIRED. IT IS AN INPUT TO "LDCURNT".
39 C
40 C "AZBEAM" AND "ELBEAM" ARE ARRAYS CONTAINING THE AZIMUTH AND ELEVATION
41 C ANGLES, IN DEGREES OF EACH BEAM. THE "AZBEAM(1)" AND "ELBEAM(1)" ARE
42 C ASSUMED TO BE IN DEGREES. "AZBEAM" AND "ELBEAM" ARE INPUTS TO "LDCURNT".
43 C
44 C "PANTILT" IS THE ELEVATION ANGLE OF THE ARRAY PANEL NORMAL IN DEGREES.
45 C IT IS AN INPUT TO "LDCURNT".
46 C
47 C "DRVCURR" IS A COMPLEX ARRAY OF DRIVING POINT CURRENTS REQUIRED TO POINT
48 C THE MAIN BEAM IN THE DIRECTION SPECIFIED BY "AZBEAM" AND "ELBEAM".
49 C "DRVCURR" IS AN OUTPUT FROM "LDCURNT".
50 C
51 C COMPLEX DRVCURR(NXELMX,NYEL)
52 C REAL XLOCATE(NXEL),YLOCATE(NYEL),AZBEAM(NUMBEAM),ELBEAM(NUMBEAM)
53 C REAL KDIR(3),KO,KYY
54 C
55 C CHECK FOR CORRECT INPUTS.
56 C
57 C IF(NXEL.GT. NXELMX)THEN
58 C CALL BEEP
59 C WRITE(*,100)
60 100 FORMAT(/1X,'***** ERROR - program terminated in LDCURNT.'/
61 $ 7X,'NXEL(=',13,') .GT. NXELMX(=',13,')'.')
62 C STOP
63 C ENDIF
64 C
65 C COMPUTE COMPLEX DRIVING POINT CURRENTS TO ACHIEVE THIS BEAM DIRECTION.
66 C
67 C DO 5 IBEAM=1,NUMBEAM,1
68 C CALL AZEL2K(AZBEAM(IBEAM),ELBEAM(IBEAM),PANTILT,KDIR,
69 KDIR(1)=KO*KDIR(1)
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```
70      KDIR(2)=K0*KDIR(2)
71      IF(IBEAM .EQ. 1)THEN
72          DO 2 J=1,NYEL,1
73              KYY=KDIR(2)*YLOCATE(J)
74              DO 1 I=1,NXEL,1
75                  DRVCURR(I,J)=
76          $      CEXP(CMPLX(0.0,-(KDIR(1)*XLOCATE(I)+KYY)))
77      1      CONTINUE
78      2      CONTINUE
79      ELSE
80          DO 4 J=1,NYEL,1
81              KYY=KDIR(2)*YLOCATE(J)
82              DO 3 I=1,NXEL,1
83                  DRVCURR(I,J)=DRVCURR(I,J)+
84          $      CEXP(CMPLX(0.0,-(KDIR(1)*XLOCATE(I)+KYY)))
85      3      CONTINUE
86      4      CONTINUE
87      ENDIF
88      5 CONTINUE
89      RETURN
90      END
```

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1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling MOM'
4 $SUBTITLE: '    SUBROUTINE MOM'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE MOM(NWIRES,XOFFSET,YOFFSET,ZOFFSET,EL1,EL2,A,ZOUT)
8 C
9 C     Written by Mike Guler
10 C     LAST MODIFIED 03-31-89
11 C     ***** 4/11/89. BY R. WILSON.
12 C         1) ADDED PARAMETER "YOFFSET".
13 C         2) THIS ENABLES HANDLING OF IMAGE ANTENNA DUE TO A GROUND PLANE.
14 C     ***** 5/09/89. BY M. GULER.
15 C         1) CHANGED HANDLING OF SELF TERM TO ONLY CALL "KING1".
16 C
17 C     METHOD OF MOMENTS PROGRAM TO CALCULATE CURRENTS ON PARALLEL WIRES OF
18 C     ARBITRARY LENGTH. A WIRE RADIUS IS ENTERED AND USED FOR COUPLING BETWEEN
19 C     SEGMENTS ON THE SAME WIRE, BUT A THIN WIRE IS ASSUMED FOR COUPLING
20 C     BETWEEN SEGMENTS ON DIFFERENT WIRES. PIECEWISE SINUSOIDAL MODES ARE USED
21 C     FOR THE CURRENT EXPANSION FUNCTIONS AND FOR THE WEIGHTING FUNCTIONS. ALL
22 C     WIRES ARE ORIENTED PARALLEL TO THE Z-AXIS, AND EACH WIRE HAS A UNIQUE
23 C     (X,Y) LOCATION.
24 C
25 C     SELF AND MUTUAL IMPEDENCE CALCULATIONS USE EQUATIONS FROM
26 C     H.R. KING, IRE A.&P., JULY 1957, PP 306-313.
27 C
28 C     DESCRIPTION OF INPUT VARIABLES (ALL DISTANCES IN WAVELENGTHS)
29 C
30 C     NWIRES - NUMBER OF WIRES (1 OR 2)
31 C     XOFFSET - X-OFFSET OF WIRE 2
32 C     YOFFSET - Y-OFFSET OF WIRE 2
33 C     ZOFFSET - Z-OFFSET OF WIRE 2 (NOTE: SEGMENTATION IS ALONG THE Z AXIS)
34 C     EL1 - LENGTH OF ELEMENT 1
35 C     EL2 - LENGTH OF ELEMENT 2
36 C     A(1) - RADIUS OF ELEMENT 1
37 C     A(2) - RADIUS OF ELEMENT 2
38 C
39 C     VARIABLE LIST: (ALL DISTANCES MEASURED IN WAVELENGTHS)
40 C
41 C     COMPLEX:
42 C     AMPS(I)    CURRENT AT PULSE I IN AMPS
43 C     VOLTS(I)   SOURCE VOLTAGE AT PULSE I IN VOLTS
44 C     YVOLTS(I)  COPY OF SOURCE VOLTAGE FOR USE IN CSOLVE
45 C     ZM(I,J)    IMPEDANCE MATRIX (BETWEEN PULSES I & J) IN OHMS
46 C     ZMUT       MUTUAL IMPEDANCE BETWEEN LOAD & SOURCE PULSES IN OHMS
47 C
48 C     REAL:
49 C     A(I)       RADIUS OF WIRE I
50 C     FACT       FACTOR WHICH ADJUSTS SINUSOIDAL FUNCTION MAGNITUDES
51 C     H          SEGMENT OFFSET IN Z-DIRECTION (DEFINED IN KING)
52 C     PI         3.1415926535898
53 C     R          SEGMENT SEPARATION IN X-DIRECTION (DEFINED IN KING)
54 C     SEGL(I)    SEGMENT LENGTH FOR WIRE I
55 C     VMAG       MAGNITUDE OF VOLTAGE SOURCE IN VOLTS
56 C     VPHS       PHASE ANGLE OF VOLTAGE SOURCE IN DEGREES
57 C     X(I)       X-LOCATION OF WIRE I
58 C     Y(I)       Y-LOCATION OF WIRE I
59 C     Z(I,J)     Z-LOCATION OF THE J-TH PULSE OF WIRE I
60 C     ZEND(I,1)  MINIMUM Z-LOCATION OF WIRE I
61 C     ZEND(I,2)  MAXIMUM Z-LOCATION OF WIRE I
62 C     ZR         REAL PART OF MUTUAL IMPEDANCE IN OHMS (DEFINED IN KING)
63 C     ZX         IMAGINARY PART OF MUTUAL IMPEDANCE IN OHMS (DEFINED IN KING)
64 C
65 C     INTEGER:
66 C     IMUTP      PULSE NUMBER FOR MUTUAL IMPEDANCE CALCULATION
67 C     MXDIM      MAXIMUM DIMENSION OF Z-MATRIX
68 C     MXWIRE     MAXIMUM NUMBER OF WIRES ALLOWED
69 C     NOS        OFFSET COUNT USED TO FILL Z-MATRIX

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70 C      NOSI      OFFSET COUNT USED TO FILL Z-MATRIX
71 C      NOSJ      OFFSET COUNT USED TO FILL Z-MATRIX
72 C      NP        TOTAL NUMBER OF PULSES
73 C      NSEG(1)    NUMBER OF SEGMENTS IN WIRE 1
74 C      NSRCP(1)   PULSE NUMBER FOR SOURCE NUMBER 1
75 C      NWIRES     NUMBER OF WIRES
76 C      P(1)       INDEX ARRAY FOR USE IN CSOLVE
77 C
78 C      LOGICAL:
79 C      PARPIV     PARTIAL PIVOTING SWITCH FOR USE IN CSOLVE
80 C
81 C
82 C      EXTERNALS:
83 C      KING1, KING2  CALCULATE ZR AND ZX AS DEFINED IN KINGS PAPER
84 C      SICI          CALCULATES SINE & COSINE INTEGRALS DEFINED IN ABRAMOWITZ & STEGUN
85 C
86 C      CSOLVE        COMPLEX MATRIX EQUATION SOLVER WRITTEN BY RICHARD WILSON
87 C
88 C
89 C      PARAMETER (MXDIM=18,MXWIRE=2)
90 C      PARAMETER (PI=3.1415926535898)
91 C      COMPLEX ZM(MXDIM,MXDIM),VOLTS(MXDIM),YVOLTS(MXDIM)
92 C      COMPLEX AMPS(MXDIM)
93 C      COMPLEX ZOUT
94 C      REAL SEGL(MXWIRE),Z(MXWIRE,MXDIM),X(MXWIRE),Y(MXWIRE)
95 C      REAL ZEND(MXWIRE,2),A(MXWIRE)
96 C      INTEGER NSEG(MXWIRE),P(MXDIM),NSRCP(MXDIM)
97 C      LOGICAL PARPIV
98 C      PARPIV=.TRUE.
99 C      NP=0
100 C      NSEG(1)=6
101 C      NSEG(2)=6
102 C      X(1)=0.
103 C      X(2)=XOFFSET
104 C      Y(1)=0.
105 C      Y(2)=YOFFSET
106 C      ZEND(1,1)=-EL1/2.
107 C      ZEND(1,2)=EL1/2.
108 C      ZEND(2,1)=ZOFFSET-EL2/2.
109 C      ZEND(2,2)=ZOFFSET+EL2/2.
110 C      NSRCP(1)=NSEG(1)/2
111 C      VMAG=1.
112 C      VPHS=0.
113 C      IF(NWIRES.GT.2.OR.NWIRES.LE.0) THEN
114 C          CALL BEEP
115 C          WRITE(*,100)
116 100  FORMAT(/1X,'***** ERROR - program terminated in MOM.')
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117 C          WRITE(*,101)NWIRES
118 101  FORMAT(7X,'NWIRES(=,I2,') must be 1 or 2.')
```

```

119 C          STOP
120 C      ENDIF
121 C      IF(NWIRES.EQ.2) IMUTP=NSEG(1)-1+NSEG(2)/2
122 C      IF(EL1.LE.0..OR.EL2.LE.0) THEN
123 C          CALL BEEP
124 C          WRITE(*,100)
125 C          WRITE(*,102)EL1,EL2
126 102  FORMAT(7X,'EL1(=,1PE10.3,') and EL2(=,1PE10.3,') must be',
127 C          $ 1X,'.GE. 0.0.')
```

```

128 C          STOP
129 C      ENDIF
130 C      DO 10 I=1,NWIRES
131 C          IF(A(I).LE.0.) THEN
132 C              CALL BEEP
133 C              WRITE(*,100)
134 C              WRITE(*,103)I,A(I)
135 103  FORMAT(7X,'Radius of Wire ',I1,'(=,1PE10.3,') must be',
136 C          $ 1X,'.GT. 0.0.')
```

```

137 C              STOP
138 C          ENDIF

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```

139      IF(NSEG(I).LE.1) THEN
140          CALL BEEP
141          WRITE(*,100)
142          WRITE(*,104)I,NSEG(I)
104      FORMAT(7X,'No. Segments on Wire ',I1,'(= ',I3,
144      $      ' ) must be .GT. 1.'/)
145          STOP
146      ENDIF
147      DELZ=ZEND(I,2)-ZEND(I,1)
148      SEGL(I)=DELZ/NSEG(I)
149      IF(SEGL(I).GT.0.25) THEN
150          CALL BEEP
151          WRITE(*,*) '*** WARNING ***'
152          WRITE(*,*) 'WIRE NUMBER ',I
153          WRITE(*,*) 'SEGMENT LENGTH IS GREATER THAN .25 WAVELENGTHS'
154      ENDIF
155      DO 15 J=1,NSEG(I)-1
156          Z(I,J)=ZEND(I,1)+J*SEGL(I)
157      15 CONTINUE
158      NP=NP+NSEG(I)-1
159      10 CONTINUE
160      DO 20 I=1,NP
161          VOLTS(I)=CMPLX(0.,0.)
162          DO 25 J=1,NP
163              ZM(I,J)=CMPLX(0.,0.)
164      25 CONTINUE
165      20 CONTINUE
166      VOLTS(NSRCP(1))=CMPLX(VMAG*COS(VPHS),VMAG*SIN(VPHS))
167  C
168  C      FILL Z-MATRIX FOR COUPLING BETWEEN SEGMENTS ON SAME WIRE
169      NOS=0
170      DO 30 I1=1,NWIRES
171          FACT=(SIN(2.*PI*SEGL(I1)))**2
172          DO 35 I2=1,NSEG(I1)-1
173              H=(I2-2)*SEGL(I1)
174              CALL KING1(A(I1),H,SEGL(I1),SEGL(I1),ZR,ZX)
175              DO 40 I3=1,NSEG(I1)-I2
176                  IF(I2.EQ.1) THEN
177                      K1=I3+NOS
178                      ZM(K1,K1)=CMPLX(ZR,ZX)/FACT
179                  ELSE
180                      K1=I3+NOS+I2-1
181                      K2=I3+NOS
182                      ZM(K1,K2)=CMPLX(ZR,ZX)/FACT
183                      ZM(K2,K1)=ZM(K1,K2)
184                  ENDIF
185      40 CONTINUE
186      35 CONTINUE
187      NOS=NOS+NSEG(I1)-1
188      30 CONTINUE
189  C
190  C      FILL Z-MATRIX FOR COUPLING BETWEEN SEGMENTS ON DIFFERENT WIRES
191      DO 45 I1=1,NWIRES
192          NOSI=NOSSET(I1,NSEG)
193          DO 50 J1=I1+1,NWIRES
194              FACT=SIN(2.*PI*SEGL(I1))*SIN(2.*PI*SEGL(J1))
195              R=SQRT((X(I1)-X(J1))**2+(Y(I1)-Y(J1))**2)
196              NOSJ=NOSSET(J1,NSEG)
197              DO 55 J2=1,NSEG(J1)-1
198                  I2=1
199                  K2=J2
200                  H=ABS(Z(J1,J2)-Z(I1,I2))-SEGL(J1)
201                  IF(R.GT.1.E-8) THEN
202                      CALL KING1(R,H,SEGL(I1),SEGL(J1),ZR,ZX)
203                  ELSE
204                      CALL KING2(H,SEGL(I1),SEGL(J1),ZR,ZX)
205                  ENDIF
206      500      ZM(K2+NOSJ,I2+NOSI)=CMPLX(ZR,ZX)/FACT
207              ZM(I2+NOSI,K2+NOSJ)=ZM(K2+NOSJ,I2+NOSI)

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```
208      I2=I2+1
209      IF(I2.GE.NSEG(I1)) GOTO 55
210      K2=K2+1
211      IF(K2.GE.NSEG(J1)) GOTO 55
212      GOTO 500
213 55    CONTINUE
214      IF(NSEG(I1).NE.2) THEN
215        DO 60 I2=2,NSEG(I1)-1
216          J2=1
217          K2=I2
218          H=ABS(Z(J1,J2)-Z(I1,I2))-SEGL(J1)
219          IF(R.GT.1.E-8) THEN
220            CALL KING1(R,H,SEGL(I1),SEGL(J1),ZR,ZX)
221          ELSE
222            CALL KING2(H,SEGL(I1),SEGL(J1),ZR,ZX)
223          ENDIF
224 510    ZM(J2+NOSJ,K2+NOSI)=CMPLX(ZR,ZX)/FACT
225          ZM(K2+NOSI,J2+NOSJ)=ZM(J2+NOSJ,K2+NOSI)
226          J2=J2+1
227          IF(J2.GE.NSEG(J1)) GOTO 60
228          K2=K2+1
229          IF(K2.GE.NSEG(I1)) GOTO 60
230          GOTO 510
231 60    CONTINUE
232      ENDIF
233 50    CONTINUE
234 45    CONTINUE
235 C
236 C
237 C  ADJUST Z-MATRIX FOR MUTUAL CALCULATION
238      IF(NWIRES.EQ.2) THEN
239        DO 62 I=1,NP
240          ZM(I,IMUTP)=CMPLX(0.,0.)
241 62    CONTINUE
242          ZM(IMUTP,IMUTP)=CMPLX(-1.,0.)
243        ENDIF
244 C
245 C
246      DO 64 I=1,NP
247        YVOLTS(I)=VOLTS(I)
248 64    CONTINUE
249      CALL CSOLVE(ZM,MXDIM,NP,YVOLTS,PARPIV,P,AMPS)
250      IF(NWIRES.EQ.1) THEN
251        ZOUT=VOLTS(NSRCP(1))/AMPS(NSRCP(1))
252      ELSE
253        ZOUT=AMPS(IMUTP)/AMPS(NSRCP(1))
254      ENDIF
255      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling NOSSET'
4 $SUBTITLE: '    FUNCTION NOSSET'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION NOSSET(IWIRE,NSEG)
8 C
9 C     Written by Mike Guler
10 C     LAST MODIFIED 02-09-89
11 C
12     INTEGER NSEG(*)
13     NOSSET=0
14     IF(IWIRE.EQ.1) RETURN
15     DO 10 I=1,IWIRE-1
16         NOSSET=NOSSET+NSEG(I)-1
17     10 CONTINUE
18     RETURN
19     END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SHOWIN'
4 $SUBTITLE: '    SUBROUTINE SHOWIN'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SHOWIN(UNITS,FREQGHZ,NUMBEAM,AZBEAM,ELBEAM,PANTILT,
8         $ DIPTILT,LFILNET,GNDPLN,XSIZE,YSIZE,ERSUB,THSUB,INPUTOK)
9 C
10 C LAST MODIFIED 9/13/89. BY R. WILSON.
11 C
12 C "SHOWIN" displays the inputs to be used in the array design for approval
13 C by the user.
14 C
15     REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM)
16     REAL GNDPLN(3)
17     CHARACTER CNUM*80,EFILNET*6,UNITS*2,LFILNET*1
18     LOGICAL YESNOTF,INPUTOK
19 C
20 C Write a header.
21 C
22     CALL NUMCHAR(FREQGHZ,-14,0,CNUM,NCHAR)
23     WRITE(*,100)CNUM(1:NCHAR)
24 100 FORMAT(/1X,'The parameters which will be used in the design of',
25     $ 1X,'the array are as follows: '//5X,'Source Frequency',
26     $ 1X,22(' '),1X,A,' GHz')
27 C
28 C Write beam positions.
29 C
30     DO 1 I=1,NUMBEAM,1
31         CALL NUMCHAR(FLOAT(I),0,0,CNUM,NCHAR)
32         CALL NUMCHAR(AZBEAM(I),-14,NCHAR,CNUM,NCHAR1)
33         CALL NUMCHAR(ELBEAM(I),-14,NCHAR1,CNUM,NCHAR2)
34         WRITE(*,101)CNUM(1:NCHAR),CNUM(NCHAR+1:NCHAR1),
35         $ CNUM(NCHAR1+1:NCHAR2)
36 101 FORMAT(5X,'Position of Beam #',A,' (Az El)',1X,11(' '),
37     $ 1X,A,2X,A,' degrees')
38     1 CONTINUE
39 C
40 C Write panel tilt and dipole tilt.
41 C
42     CALL NUMCHAR(PANTILT,-14,0,CNUM,NCHAR1)
43     CALL NUMCHAR(DIPTILT,-14,NCHAR1,CNUM,NCHAR2)
44     WRITE(*,102)CNUM(1:NCHAR1),CNUM(NCHAR1+1:NCHAR2)
45 102 FORMAT(5X,'Panel Tilt ',28(' '),1X,A,' degrees'/
46     $ 5X,'Dipole Tilt ',27(' '),1X,A,' degrees')
47 C
48 C Write location of filter network.
49 C
50     IF(LFILNET .EQ. 'T')THEN
51         EFILNET='Top'
52     ELSEIF(LFILNET .EQ. 'B')THEN
53         EFILNET='Bottom'
54     ELSEIF(LFILNET .EQ. 'L')THEN
55         EFILNET='Left'
56     ELSEIF(LFILNET .EQ. 'R')THEN
57         EFILNET='Right'
58     ENDIF
59     WRITE(*,103)EFILNET
60 103 FORMAT(5X,'Location of the Filter Network ',8(' '),1X,A)
61 C
62 C Write Ground plane info.
63 C
64     IF(GNDPLN(1) .GT. 0.0)THEN
65         CALL NUMCHAR(GNDPLN(3),-14,0,CNUM,NCHAR)
66         WRITE(*,104)CNUM(1:NCHAR)
67 104 FORMAT(5X,'Gnd Plane Spacer Dielectric Constant ..',
68     $ 1X,A)
69     ELSE

```

```
70      WRITE(*,105)
71 105   FORMAT(5X,'Gnd Plane Spacer Dielectric Constant .. no',
72      $      1X,'ground plane')
73      ENDIF
74 C
75 C   Write panel dimensions.
76 C
77      CALL NUMCHAR(XSIZE,-14,0,CNUM,NCHAR1)
78      CALL NUMCHAR(YSIZE,-14,NCHAR1,CNUM,NCHAR2)
79      WRITE(*,106)CNUM(1:NCHAR1),UNITS,CNUM(NCHAR1+1:NCHAR2),UNITS
80 106   FORMAT(5X,'Panel horizontal dimension ',12(' '),1X,A,1X,A2,'.'/
81      $ 5X,'Panel vertical dimension ',14(' '),1X,A,1X,A2,'.')
82 C
83 C   Write substrate dielectric constant and substrate thickness.
84 C
85      CALL NUMCHAR(ERSUB,-14,0,CNUM,NCHAR1)
86      CALL NUMCHAR(THSUB,-14,NCHAR1,CNUM,NCHAR2)
87      WRITE(*,107)CNUM(1:NCHAR1),CNUM(NCHAR1+1:NCHAR2),UNITS
88 107   FORMAT(5X,'Substrate Dielectric Constant ',9(' '),1X,A/
89      $ 5X,'Substrate thickness ',19(' '),1X,A,1X,A2,'./)
90 C
91 C   Ask user if these are okay.
92 C
93      INPUTOK=YESNOTF('Are these parameters ok')
94      RETURN
95      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SICI'
4 $SUBTITLE: '    SUBROUTINE SICI'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SICI(X,SI,CI)
8 C
9 C     Written by Mike Guler
10 C     Last Modified 02-15-89
11 C
12     PARAMETER(A1=38.027264,A2=265.187033,A3=335.677320,A4=38.102495)
13     PARAMETER(B1=40.021433,B2=322.624911,B3=570.236280,B4=157.105423)
14     PARAMETER(C1=42.242855,C2=302.757865,C3=352.018498,C4=21.821899)
15     PARAMETER(D1=48.196927,D2=482.485984,D3=1114.978885,D4=449.690326)
16     PARAMETER (PI=3.1415926535898,PIOVER2=PI/2.0,EC=.57721566490153)
17     REAL X,SII,CII,SI,CI
18     IF(X .LE. 0.0) THEN
19         CALL BEEP
20         WRITE(*,100)X
21 100    FORMAT(/1X,'***** ERROR - Program terminated in SICI.'/
22 $      7X,'X(=',1PE10.3,') must be .GT. 0.'/)
23     STOP
24     ENDIF
25     IF(X.LT.1.) THEN
26         N=NINT(2.*X+2.4)
27         SI=X
28         CI=0
29         DO 10 I=1,N
30             SII=(-1)**I*X**(2*I+1)/(2*I+1)
31             CII=(-1)**I*X**(2*I)/(2*I)
32             DO 20 J1=2,2*I+1
33                 SII=SII/J1
34 20          CONTINUE
35             DO 30 J2=2,2*I
36                 CII=CII/J2
37 30          CONTINUE
38             SI=SI+SII
39             CI=CI+CII
40 10          CONTINUE
41             CI=CI+LOG(X)+EC
42     ELSE
43         X2=X*X
44         RNUM=A4+X2*(A3+X2*(A2+X2*(A1+X2)))
45         DNUM=B4+X2*(B3+X2*(B2+X2*(B1+X2)))
46         F=RNUM/DNUM/X
47         RNUM=C4+X2*(C3+X2*(C2+X2*(C1+X2)))
48         DNUM=D4+X2*(D3+X2*(D2+X2*(D1+X2)))
49         G=RNUM/DNUM/X2
50         SI=PIOVER2-F*COS(X)-G*SIN(X)
51         CI=F*SIN(X)-G*COS(X)
52     ENDIF
53     RETURN
54     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SQROOT'
4 $SUBTITLE: '    SUBROUTINE SQROOT'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SQROOT(D,H,U1,U2)
8 C
9 C     Written by Mike Guler
10 C     LAST MODIFIED 02-07-89
11 C
12     PARAMETER (PI=3.1415926535898,B=2.*PI)
13     SQR=SQRT(D*D+H*H)
14     IF(H.GT.0) THEN
15         U1=B*(SQR+H)
16         U2=B*D/(SQR+H)
17     ELSEIF(H.LT.0) THEN
18         U1=B*D/(SQR-H)
19         U2=B*(SQR-H)
20     ELSE
21         U1=B*D
22         U2=U1
23     ENDIF
24     RETURN
25     END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SUMMARY'
4 $SUBTITLE: ' SUBROUTINE SUMMARY'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE SUMMARY(DATSTMP,UNITS,FREQGHZ,LAMBDA,NUMBEAM,AZBEAM,
8 $ ELBEAM,PANTILT,XSIZE,YSIZE,NXEL,NXELMX,NYEL,DX,DY,DIPLNG,DIPWID,
9 $ DIPTILT,LFILNET,ERSUB,THSUB,GNDPLN,XLOCATE,YLOCATE,DRVCURR,
10 $ ZDRVIMP,GAIN)
11 C
12 C LAST MODIFIED 9/13/89. BY R. WILSON.
13 C
14 C "SUMMARY" writes a summary of the array design to a file.
15 C
16 COMPLEX ZDRVIMP(NXELMX,NYEL),DRVCURR(NXELMX,NYEL)
17 COMPLEX REC2POL
18 REAL XLOCATE(NXEL),YLOCATE(NYEL)
19 REAL AZBEAM(NUMBEAM),ELBEAM(NUMBEAM),GAIN(NUMBEAM),DIPTILT(3)
20 REAL GNDPLN(3),LAMBDA
21 CHARACTER DATSTMP*20,UNITS*2,LFILNET*1
22 C
23 C Write the header to the file.
24 C
25 WRITE(1,*)'DIPOLE ARRAY DESIGN',DATSTMP
26 WRITE(1,*)' *****'
27 WRITE(1,*)'The operating frequency is ',FREQGHZ,' GHz',
28 $ ' (Lambda=',LAMBDA,' ',UNITS,')'
29 IF(NUMBEAM.EQ.1)THEN
30 WRITE(1,*)'The beam is pointed at ',AZBEAM(1),' deg. AZIMUTH ',
31 $ ELBEAM(1),' deg. ELEVATION'
32 ELSE
33 WRITE(1,*)'The beams are pointed at ',AZBEAM(1),' deg. ',
34 $ 'AZIMUTH ',ELBEAM(1),' deg. ELEVATION'
35 DO 1 IBEAM=2,NUMBEAM,1
36 WRITE(1,*) ' ',AZBEAM(IBEAM),
37 $ ' deg. AZIMUTH ',ELBEAM(IBEAM),' deg. ELEVATION'
38 1 CONTINUE
39 ENDIF
40 WRITE(1,*)' *****'
41 WRITE(1,*)'The array panel is tilted ',PANTILT,' degrees in ',
42 $ 'ELEVATION'
43 WRITE(1,*)'The array is ',XSIZE,' ',UNITS,'. by ',
44 $ YSIZE,' ',UNITS,'.
45 WRITE(1,*)'There are ',NXEL,' elements in the HORIZONTAL',
46 $ ' direction'
47 WRITE(1,*) ' ',NYEL,' elements in the VERTICAL direction'
48 WRITE(1,*)'The dipole elements are spaced ',DX,' ',UNITS,
49 $ ' apart HORIZONTALLY'
50 WRITE(1,*) ' ',DY,' ',UNITS,
51 $ ' apart VERTICALLY'
52 WRITE(1,*)'Each dipole is ',DIPLNG,' ',UNITS,'. long and ',DIPWID,
53 $ ' ',UNITS,'. wide'
54 WRITE(1,*)'Each dipole is tilted ',DIPTILT(3),' degrees from',
55 $ ' VERTICAL'
56 WRITE(1,*)' *****'
57 IF(LFILNET.EQ.'B')THEN
58 WRITE(1,*)'The filter network is located along the ',
59 $ 'BOTTOM edge of the substrate'
60 ELSEIF(LFILNET.EQ.'T')THEN
61 WRITE(1,*)'The filter network is located along the ',
62 $ 'TOP edge of the substrate'
63 ELSEIF(LFILNET.EQ.'R')THEN
64 WRITE(1,*)'The filter network is located along the ',
65 $ 'RIGHT edge of the substrate'
66 ELSEIF(LFILNET.EQ.'L')THEN
67 WRITE(1,*)'The filter network is located along the ',
68 $ 'LEFT edge of the substrate'
69 ENDIF

```

```

70      WRITE(1,*)'The substrate dielectric constant is ',ERSUB
71      WRITE(1,*)'The substrate is ',THSUB,' ',UNITS,'. thick'
72      IF(GNDPLN(2) .GT. 0.0)THEN
73          WRITE(1,*)'          *****'
74          WRITE(1,*)'A ground plane is to be used ',GNDPLN(2),' ',UNITS,
75          $      ' from the array panel'
76          WRITE(1,*)'The dielectric constant of the spacer material',
77          $      ' is ',GNDPLN(3)
78      ENDIF
79      WRITE(1,*)'          *****'
80  C
81  C      Write the dipole locations, driving point voltages, currents and
82  C      impedances to the file.
83  C
84      WRITE(1,101)
85      101  FORMAT(/7X,'Array',5X,'|',8X,'Location',7X,'|',
86      $      16X,'Driving Point',3X,'Column',3X,'Row',2X,'|', 'Horizontal',
87      $      3X,'Vertical',2X,'|',7X,'Current',16X,'Impedance')
88      DO 3 J=1,NYEL,1
89          Y=YLOCATE(J)
90          DO 2 I=1,NXEL,1
91              WRITE(1,102)I,J,XLOCATE(I),Y,
92              $      REC2POL(DRVCURR(I,J),.FALSE.),
93              $      REC2POL(ZDRVIMP(I,J),.FALSE.)
94          102  FORMAT(4X,15,'|',15,2('|',G10.3),
95          $      2(1X,'|',G10.3,'/_',G10.3))
96          2  CONTINUE
97          3  CONTINUE
98          WRITE(1,*)'          *****'
99  C
100 C      Write the gain values at the main beam locations to the file.
101 C
102      WRITE(1,103)
103      103  FORMAT(1X,'Azimuth',2X,'Elevation',2X,'Gain dBi')
104      DO 4 I=1,NUMBEAM,1
105          WRITE(1,104)AZBEAM(I),ELBEAM(I),GAIN(I)
106      104  FORMAT(1X,F8.3,2X,F8.3,2X,F8.3)
107      4  CONTINUE
108      WRITE(1,*)'          *****'
109  C
110      RETURN
111      END

```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling UNIT2IN'
4 $SUBTITLE: '    FUNCTION UNIT2IN'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION UNIT2IN(X,UNITS)
8 C
9 C  LAST MODIFIED 5/08/89.
10 C
11     CHARACTER UNITS*2
12 C
13 C  "UNIT2IN" CONVERTS "X" IN UNITS OF "UNITS" TO X IN UNITS OF INCHES.
14 C
15     IF(UNITS .EQ. 'ft')THEN
16         UNIT2IN=X*12.0
17     ELSEIF(UNITS .EQ. 'in')THEN
18         UNIT2IN=X
19     ELSEIF(UNITS .EQ. 'm')THEN
20         UNIT2IN=X/0.0254
21     ELSEIF(UNITS .EQ. 'cm')THEN
22         UNIT2IN=X/2.54
23     ENDIF
24     RETURN
25     END
```

```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling AXISXY'
4  $SUBTITLE: '    SUBROUTINE AXISXY'
5  $PAGE
6  $NOTRUNCATE
7      SUBROUTINE AXISXY(NOPT,XSIZE,YSIZE,BOXDIR,XMAX,XMIN,YMAX,YMIN,
8          $ DELTAX,DELTAY,AXISLBL,XSCALE,YSCALE)
9  C
10 C  LAST MODIFIED 9/21/87. BY R. WILSON.
11 C      1) DETERMINE FONT USED FOR AXIS NUMBERS WITH CALL TO "SYMESC"
12 C  ***** 4/20/88. BY R. WILSON.
13 C      1) NOW DRAW BOX BY CALL TO "DRWBOX".
14 C  ***** 12/05/88. BY R. WILSON.
15 C      1) REMOVED CALL TO "DRWBOX" AND DRAW THE AXES WITHIN "LINAXIS" AND
16 C          "LOGAXIS".
17 C      2) REMOVED "CHARTYP" AS ARGUMENT TO "LINAXIS" AND "LOGAXIS".
18 C  ***** 1/10/89. BY R. WILSON.
19 C      1) MOVED ADJUSTMENT FOR "YMAX"="YMIN" HERE.
20 C  ***** 5/05/89. BY R. WILSON.
21 C      1) ADDED CAPABILITY OF ROTATING THE GRAPH "BOX".
22 C      2) THE ROTATION IS INDICATED BY THE ARRAY "BOXDIR" WHICH CONTAINS THE
23 C          DIRECTION COSINES OF THE BOX X-AXIS WITH THE PLOTTER AXES.
24 C
25      REAL XORIGIN(2),BOXDIR(3)
26      CHARACTER AXISLBL(2)*(*),IAXIS*8
27      COMMON/LINAXC/MAXDIG
28  C
29 C  "NOPT" INDICATES HOW THE AXES ARE TO BE LABELED AS FOLLOWS
30 C          X-LOW  X-UP  Y-LEFT  Y-RIGHT
31 C      NOPT=0      PARL    NO      PERP    NO
32 C      NOPT=1      PARL    TICS   PERP    TICS
33 C      NOPT=2      PARL    PARL   PERP    PERP
34 C      NOPT=3      PARL    NO     PARL    NO
35 C      NOPT=4      PARL    TICS   PARL    TICS
36 C      NOPT=5      PARL    PARL   PARL    PARL
37 C
38 C  WHERE X-LOW REFERS TO THE LOWER X-AXIS, X-UP REFERS TO THE UPPER X-AXIS,
39 C  Y-LEFT REFERS TO THE LEFT Y-AXIS AND Y-RIGHT REFERS TO THE RIGHT Y-AXIS.
40 C  "NO" INDICATES NO LABELING ON THAT AXIS, "TICS" INDICATES ONLY TIC MARKS
41 C  ON THAT AXIS, "PARL" INDICATES TICS MARKS WITH NUMBERS PARALLEL TO THE
42 C  AXIS AND "PERP" INDICATES TIC MARKS WITH NUMBERS PERPENDICULAR TO THE
43 C  AXIS.
44 C
45 C  FOR DEFINITIONS OF THE OTHER PARAMETERS SEE GRAPH.
46 C
47 C  CALCULATE PARAMETERS FOR SYMBOL.
48 C
49      TICSIZE=0.02*SQRT(XSIZE*XSIZE+YSIZE*YSIZE)
50      HEIGHT=TICSIZE
51      EHT=0.8*HEIGHT
52  C
53 C  CHECK FOR "YMAX"="YMIN" AND ADJUST IF NECESSARY.
54 C
55      IF(YMAX .EQ. YMIN)THEN
56          DELTAY=1.0/(10.0**(NUMDECR(YMAX,MAXDIG-1)+1))
57          YMAX=YMAX+DELTAY
58          YMIN=YMIN-DELTAY
59      ENDIF
60 C
61 C  ANNOTATE LEFT Y-AXIS.
62 C
63      XORIGIN(1)=-YSIZE*BOXDIR(2)
64      XORIGIN(2)=YSIZE*BOXDIR(1)
65      ANGLE=BOXDIR(3)-90.0
66      IF(NOPT.GE.0 .AND. NOPT.LE.2)THEN
67          IAXIS='PERP-1-1'
68      ELSEIF(NOPT.GE.3 .AND. NOPT.LE.5)THEN
69          IAXIS='PARL-1-1'

```

```
70      ENDIF
71      IF(DELTA .GE. 0.0)THEN
72          CALL LINAXIS(YMIN,YMAX,DELTA,HEIGHT,TICSIZE,ANGLE,YSIZE,
73      $      XORIGIN,IAXIS,YSCALE,YLPRIME)
74      ELSEIF(DELTA .LT. 0.0)THEN
75          CALL LOGAXIS(YMIN,YMAX,EHT,HEIGHT,TICSIZE,ANGLE,YSIZE,
76      $      XORIGIN,IAXIS,YSCALE,YLPRIME)
77      ENDIF
78      CALL TITLE(AXISLBL(2),ANGLE,-1,YLPRIME,HEIGHT,YSIZE,XORIGIN)
79  C
80  C  ANNOTATE LOWER X-AXIS.
81  C
82      XORIGIN(1)=0.0
83      XORIGIN(2)=0.0
84      ANGLE=BOXDIR(3)
85      IF(DELTA .GE. 0.0)THEN
86          CALL LINAXIS(XMAX,XMIN,DELTA,HEIGHT,TICSIZE,ANGLE,XSIZE,
87      $      XORIGIN,'PARL+1-1',XSCALE,YLPRIME)
88      ELSEIF(DELTA .LT. 0.0)THEN
89          CALL LOGAXIS(XMAX,XMIN,EHT,HEIGHT,TICSIZE,ANGLE,XSIZE,
90      $      XORIGIN,'PARL+1-1',XSCALE,YLPRIME)
91      ENDIF
92      CALL TITLE(AXISLBL(1),ANGLE,1,YLPRIME,HEIGHT,XSIZE,XORIGIN)
93      IF(NOPT.NE.0 .AND. NOPT.NE.3)THEN
94  C
95  C  ADD RIGHT Y-AXIS.
96  C
97          XORIGIN(1)=XSIZE*BOXDIR(1)
98          XORIGIN(2)=XSIZE*BOXDIR(2)
99          ANGLE=BOXDIR(3)+90.0
100         IF(NOPT.EQ.1 .OR. NOPT.EQ.4)THEN
101             IAXIS='NOLABEL'
102         ELSEIF(NOPT .EQ. 2)THEN
103             IAXIS='PERP+1-1'
104         ELSEIF(NOPT .EQ. 5)THEN
105             IAXIS='PARL-1-1'
106         ENDIF
107         IF(DELTA .GE. 0.0)THEN
108             CALL LINAXIS(YMAX,YMIN,DELTA,HEIGHT,TICSIZE,ANGLE,YSIZE,
109     $      XORIGIN,IAXIS,YSCALE,YLPRIME)
110         ELSEIF(DELTA .LT. 0.0)THEN
111             CALL LOGAXIS(YMAX,YMIN,EHT,HEIGHT,TICSIZE,ANGLE,YSIZE,
112     $      XORIGIN,IAXIS,YSCALE,YLPRIME)
113         ENDIF
114  C
115  C  ADD UPPER X-AXIS.
116  C
117          XORIGIN(1)=XSIZE*BOXDIR(1)-YSIZE*BOXDIR(2)
118          XORIGIN(2)=XSIZE*BOXDIR(2)+YSIZE*BOXDIR(1)
119          ANGLE=BOXDIR(3)+180.0
120          IF(NOPT.EQ.1 .OR. NOPT.EQ.4)THEN
121              IAXIS='NOLABEL'
122          ELSE
123              IAXIS='PARL-1-1'
124          ENDIF
125          IF(DELTA .GE. 0.0)THEN
126              CALL LINAXIS(XMIN,XMAX,DELTA,HEIGHT,TICSIZE,ANGLE,XSIZE,
127     $      XORIGIN,IAXIS,XSCALE,YLPRIME)
128          ELSEIF(DELTA .LT. 0.0)THEN
129              CALL LOGAXIS(XMIN,XMAX,EHT,HEIGHT,TICSIZE,ANGLE,XSIZE,
130     $      XORIGIN,IAXIS,XSCALE,YLPRIME)
131          ENDIF
132      ENDIF
133      RETURN
134      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling BEEP'
4 $SUBTITLE: '    SUBROUTINE BEEP'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE BEEP
8 C
9 C   LAST MODIFIED 12/07/88.  BY R. WILSON.
10 C
11 C   "BEEP" BEEPS THE SPEAKER BY SENDING A CONTROL G TO THE SCREEN.
12 C
13     WRITE(*,'(1X,A1)')CHAR(7)
14     RETURN
15     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling CLOSPLT'
4 $SUBTITLE: ' SUBROUTINE CLOSPLT'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE CLOSPLT
8 C
9 C LAST MODIFIED 5/17/89. BY R. WILSON.
10 C ***** 9/10/89. BY R. WILSON.
11 C 1) Added FACTR to the PLOT88C common block. This allows NEWPAGE
12 C to reset the user specified scale factor for each page of plots.
13 C 2) Added special handling for the case of graphics output to the
14 C console (for 93 <= MODEL <=97 and MODEL=99). This allows
15 C displaying a message for the final page of plots. The message
16 C for the other pages is handled by NEWPAGE.
17 C 3) Changed the criterion for output to the laser printer to include
18 C all the laser printer model numbers.
19 C ***** 9/11/89. BY R. WILSON.
20 C 1) XPAGEORG and YPAGEORG are passed in a common block from NEWPAGE
21 C for use by CLOSPLT in displaying a message if the console is the
22 C output device.
23 C 2) Changed from IF..THEN to SELECT CASE structure to test for MODEL
24 C number.
25 C
26 COMMON/PLOT88C/IOPORT,MODEL,FACTR
27 COMMON/NEWPAGC/XPAGEORG,YPAGEORG
28 C
29 C "CLOSPLT" writes a message to the screen if plot is to go to the
30 C laser printer or the plotter then closes the PLOT88 file which causes
31 C the hardcopy to be displayed.
32 C
33 SELECT CASE (MODEL)
34 CASE (60:65)
35 WRITE(*,100)CHAR(7)
36 100 FORMAT('+',A,'Please wait - sending the plots to the Laser',
37 $ 1X,'Printer...',20(' '))
38 CALL PLOT(0.0,0.0,999)
39 WRITE(*,102)CHAR(7)
40 CASE (20)
41 WRITE(*,101)CHAR(7)
42 101 FORMAT('+',A,'Ready to send plots to HP 7470A. LOAD',
43 $ 1X,'paper, STRIKE any key when ready...')
44 CALL WAITKY(IASCI1,ISCANCD)
45 WRITE(*,102)' '
46 CALL PLOT(0.0,0.0,999)
47 CASE(93:97,99)
48 IF(MODEL .EQ. 96)CALL COLOR(4,IERR)
49 CALL FACTOR(1.0)
50 CALL SYMBOL(2.5-XPAGEORG,5.0-YPAGEORG,0.12,
51 $ 'Strike Any Key To Continue',0.0,26)
52 WRITE(*,102)CHAR(7)
53 CALL PLOT(0.0,0.0,999)
54 CASE DEFAULT
55 WRITE(*,102)CHAR(7)
56 CALL PLOT(0.0,0.0,999)
57 END SELECT
58 102 FORMAT('+',A,77(' '))
59 C
60 RETURN
61 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling COSD'
4 $SUBTITLE: '    FUNCTION COSD'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION COSD(ANGLE)
8 C
9 C   LAST MODIFIED 12/01/88.  BY. R. WILSON.
10 C
11 C   "COSD" COMPUTES THE COSINE OF THE ANGLE "ANGLE" WHERE "ANGLE" IS IN
12 C   DEGREES.
13 C
14     PARAMETER(PI=3.1415926535898,DEG2RAD=PI/180.0)
15     COSD=COS(ANGLE*DEG2RAD)
16     RETURN
17     END
```

```
1 $MESSAGE:'Compiling DATE'
2 $SUBTITLE: '  Function DATE'
3 $PAGE
4 $NOTRUNCATE
5     FUNCTION DATE()
6 C
7 C   LAST MODIFIED 8/28/88.  BY R. WILSON
8 C
9 C   "DATE" RETURNS THE CURRENT DATE (AS REPORTED BY THE SYSTEM CLOCK).  MS
10 C   FORTRAN HAS A LIBRARY ROUTINE CALLED "GETDAT" WHICH IS CALLED BY "DATE".
11 C   THE RETURNED INTEGER*2 VALUES ARE PACKED INTO A CHARACTER VARIABLE "DATE".
12 C
13     INTEGER*2 IYR,IMON,IDAY
14     CHARACTER DATE*10
15 C
16 C   GET THE CURRENT DATE FROM SYSTEM CLOCK.
17 C
18     CALL GETDAT(IYR,IMON,IDAY)
19 C
20 C   PACK DATE INTO CHARACTER VARIABLE "DATE".
21 C
22     WRITE(DATE,100)IMON,IDAY,IYR
23 100 FORMAT(12,'/',12,'/',14)
24     IF(DATE(4:4) .EQ. ' ')THEN
25         DATE(4:4)='0'
26     ENDIF
27     RETURN
28     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling DBAMP'
4 $SUBTITLE: ' SUBROUTINE DBAMP'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE DBAMP(AMP,NX,NY,NXMAX,AMAX,AMINDB,LOGTODB)
8 C
9 C LAST MODIFIED 3/18/86. BY R. WILSON.
10 C ***** 6/17/88. BY R. WILSON.
11 C 1) ADDED CHECK FOR CORRECT "NX" SIZE COMPARED TO "NXMAX".
12 C ***** 6/29/89. BY R. WILSON.
13 C 1) ADDED CODE TO HANDLE "AMAX" BEING SMALL (PARTICULARLY "AMAX"=0.0).
14 C 2) A NEW VARIABLE, "ANORM" IS SET TO "AMAX" UNLESS "AMAX" IS .LT.
15 C "ZERO" IN WHICH CASE "ANORM" IS SET TO "ZERO". "ZERO" IS DEFINED IN
16 C A PARAMETER STATEMENT BELOW.
17 C 3) UPDATED THE ERROR MESSAGE FORMAT TO BE CONSISTENT WITH THOSE IN
18 C OTHER LIBRARY ROUTINES.
19 C
20 C "DBAMP" CONVERTS THE REAL ARRAY "AMP" TO DB. THE VALUES IN "AMP" ARE
21 C NORMALIZED TO "AMAX" BEFORE CONVERSION. IF THE RESULTING DB VALUE WILL BE
22 C LESS THAN "AMINDB" DB THEN IT IS SET EQUAL TO "AMINDB". "LOGTODB" IS
23 C USUALLY SET TO EITHER 10.0 OR 20.0. THIS ALLOWS THE CONVERSION OF EITHER
24 C POWER RATIOS OR VOLTAGE (FIELD) RATIOS, RESPECTIVELY, TO DB.
25 C
26 C THE ARRAY "AMP" IN THE CALLING PROGRAM MAY BE EITHER 1 OR 2 DIMENSIONAL.
27 C "NX" BY "NY" VALUES IN THE ARRAY ARE CONVERTED. IF "AMP" IS 1 DIMENSIONAL
28 C THEN "NY" SHOULD BE PASSED AS A 1 (ONE). "NXMAX" IS USED BY "DBAMP" AS
29 C THE ROW DIMENSION OF "AMP". IT SHOULD BE SET TO THE VALUE OF THE ROW
30 C DIMENSION OF THE CORRESPONDING ARRAY IN THE CALLING PROGRAM, ESPECIALLY IF
31 C "AMP" IS TO BE 2 DIMENSIONAL. A CHECK IS MADE TO INSURE THAT "NX" .LE.
32 C "NXMAX" BY "DBAMP" AND THE PROGRAM IS TERMINATED WITH AN ERROR MESSAGE IF
33 C THIS IS NOT THE CASE.
34 C
35 C PARAMETER (ZERO=1.0E-12)
36 C REAL AMP(NXMAX,*),LOGTODB
37 C
38 C CHECK FOR PROPER INPUTS.
39 C
40 C IF(NX .GT. NXMAX)THEN
41 C WRITE(*,100)NX,NXMAX
42 100 FORMAT(1X,'***** ERROR- Program terminated in DBAMP. '/
43 $ 7X,'NX(= ',I5,' ) .GT. NXMAX(= ',I5,' ).')
44 C STOP
45 C ENDIF
46 C
47 C CONVERT AMP TO DB.
48 C
49 C AMIN10=10.0**(AMINDB/LOGTODB)
50 C ANORM=AMAX
51 C IF(ANORM .LT. ZERO)ANORM=ZERO
52 C DO 1 J=1,NY,1
53 C DO 1 I=1,NX,1
54 C AIJ=ABS(AMP(I,J)/ANORM)
55 C IF(AIJ .LE. AMIN10)THEN
56 C AMP(I,J)=AMINDB
57 C ELSE
58 C AMP(I,J)=LOGTODB*ALOG10(AIJ)
59 C ENDIF
60 C 1 CONTINUE
61 C RETURN
62 C END
```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling DOSNAME'
4 $SUBTITLE: '    FUNCTION DOSNAME'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION DosName(FNAME)
8 C
9 C  "DosName" returns .TRUE. if the character string "FNAME" is one of the
10 C  DOS reserved names (or special MS Fortran device names), see code below.
11 C  Otherwise, it returns .FALSE.. The name is checked without any included
12 C  path or extension first. If it is found to be a DOS reserved name then
13 C  the path and extension are removed from "FNAME" to help INQUIRE and OPEN
14 C  recognize the special names. If the base name is not one of the DOS
15 C  reserved names then it is checked against the additional MS Fortran reserved
16 C  names. If the base name matches one of the Fortran reserved name and there
17 C  is no extension or path "DosName" will be returned .TRUE..
18 C
19 C  NOTE: "FNAME" may be modified by "DosName" so the function call should NOT
20 C  be made with a constant for "FNAME".
21 C
22     INTEGER LSTCHAR,FSTCHAR
23     LOGICAL DosName,SimpleName
24     CHARACTER FNAME*(*),FNAMEUP*11
25 C
26 C  Get the Name without the path specifaction.
27 C
28     LSTCHAR=NONBLNK(FNAME,LEN(FNAME),1)
29     FSTCHAR=SCAN(FNAME,'\\,.',TRUE.)
30     IDOT=INDEX(FNAME, '.')
31     IF(IDOT.GT. 0)LSTCHAR=IDOT-1
32     IF(FSTCHAR.EQ. 0)THEN
33         IF(IDOT.EQ. 0)SimpleName=.TRUE.
34         FSTCHAR=1
35     ELSE
36         SimpleName=.FALSE.
37         FSTCHAR=FSTCHAR+1
38     ENDIF
39 C
40 C  Check for match with DOS reserved names with path and extension removed.
41 C
42     FNAMEUP=FNAME(FSTCHAR:LSTCHAR)
43     CALL UPPER(FNAMEUP,0)
44     DosName=(FNAMEUP.EQ. 'AUX' .OR. FNAMEUP.EQ. 'COM1' .OR.
45 $           FNAMEUP.EQ. 'COM2' .OR. FNAMEUP.EQ. 'CON' .OR.
46 $           FNAMEUP.EQ. 'PRN' .OR. FNAMEUP.EQ. 'LPT1' .OR.
47 $           FNAMEUP.EQ. 'LPT2' .OR. FNAMEUP.EQ. 'LPT3' .OR.
48 $           FNAMEUP.EQ. 'NUL')
49 C
50 C  If reserved name was found change FNAME to help INQUIRE and OPEN recognize
51 C  that fact. If not, check the name with three names reserved by MS FORTRAN,
52 C  returning true in this case only if no path or extension is present.
53 C
54     IF(DosName)THEN
55         FNAME(1:)=FNAME(FSTCHAR:LSTCHAR)
56     ELSE
57         Dosname=(FNAMEUP.EQ. 'ERR' .OR. FNAMEUP.EQ. 'LINE' .OR.
58 $           FNAMEUP.EQ. 'USER') .AND. SimpleName
59     ENDIF
60     RETURN
61     END
```

```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling DRWCURV'
4  $SUBTITLE: '    SUBROUTINE DRWCURV'
5  $PAGE
6  $NOTRUNCATE
7      SUBROUTINE DRWCURV(X,Y,NX,XSIZE,YSIZE,BOXDIR,XMIN,YMIN,
8          $ XSCALE,YSCALE,JGRAPH)
9  C
10 C  LAST MODIFIED  2/20/89.  BY R. WILSON.
11 C  *****      5/05/89.  BY R. WILSON.
12 C      1) Added capability of rotating the graph "BOX".
13 C      2) The rotation is indicated by the array "BOXDIR" which contains the
14 C          direction cosines of the box X-axis with the plotter X-axis.
15 C
16 C  "DRWCURV" connects the points whose XY coordinates are contained in the
17 C  arrays "X" and "Y". The curve is drawn within a box. Any part of the curve
18 C  falling outside the box is not drawn.
19 C
20 C  "X" and "Y" are real arrays containing the coordinates, in user units, of
21 C  the points to be connected by a straight line segments. They are
22 C  dimensioned "NX". They are inputs to "DRWCURV".
23 C
24 C  "NX" is the size of the coordinate arrays "X" and "Y". "NX" is an input to
25 C  "DRWCURV".
26 C
27 C  "XSIZE" and "YSIZE" are the X and Y dimensions, respectively, of the box
28 C  which is to contain the curve. They are assumed to be in inches. "XSIZE"
29 C  and "YSIZE" are inputs to "DRWCURV".
30 C
31 C  "BOXDIR" is a real array which contains the direction cosines of the X-axis
32 C  of the box with the physical plotter axes. "BOXDIR(1)" holds the direction
33 C  cosine w.r.t. the plotter X-axis. "BOXDIR(2)" holds the direction cosine
34 C  w.r.t. the plotter Y-axis. "BOXDIR" is used to rotate the box to any
35 C  angle. The angle of the box, in degrees, is stored in "BOXDIR(3)" since
36 C  the plotter does not have a Z-axis.
37 C
38 C  "XMIN" and "YMIN" are the X and Y values, in user coordinates, which are
39 C  desired at the origin of the box containing the curve. They are inputs to
40 C  "DRWCURV".
41 C
42 C  "XSCALE" and "YSCALE" are the X and Y scale factors, respectively, used in
43 C  converting the user coordinates to inches on the plot. They are inputs to
44 C  "DRWCURV".
45 C
46 C  "JGRAPH" is an integer indicating the number of the current curve being
47 C  plotted in the box. If "JGRAPH" is negative then the "JGRAPH"-TH centered
48 C  symbol will be plotted approximately every inch in arc length along the
49 C  current curve. "JGRAPH" is an input to "DRWCURV".
50 C
51     REAL X(NX),Y(NX),BOXDIR(3)
52     LOGICAL OUTSIDE
53 C
54 C  The following statement functions are used in windowing the plot data if
55 C  "XMAX, XMIN, YMAX, YMIN" do not include all of the plot data.
56 C
57     XINTSCT(RX,RY,RXL,RYL,RXMAX)=((RX-RXL)/(RY-RYL))*
58     $ (RYMAX-RYL)+RXL
59     YINTSCT(RX,RY,RXL,RYL,RXMAX)=((RY-RYL)/(RX-RXL))*
60     $ (RXMAX-RXL)+RYL
61 C
62 C  Scale data in "X" and "Y" and plot.
63 C
64     OUTSIDE=.TRUE.
65     DO 1 I=1,NX,1
66         XP=(X(I)-XMIN)*XSCALE
67         YP=(Y(I)-YMIN)*YSCALE
68         IF(XP.GT.XSIZE .OR. XP.LT.0.0 .OR.
69     $     YP.GT.YSIZE .OR. YP.LT.0.0 .OR. I.EQ.1)THEN

```

```

70 C
71 C      The current point is outside the box.
72 C
73 C      IF(.NOT.(OUTSIDE))THEN
74 C
75 C      The previous point was inside the box. Linearly interpolate to
76 C      find the intersection of the curve leaving the box with the box
77 C      boundary.
78 C
79 C      XPNEW=XP
80 C      YPNEW=YP
81 C      IF(XPNEW .GT. XSIZE)THEN
82 C          YPNEW=YINTSCT(XPNEW,YPNEW,XPLAST,YPLAST,XSIZE)
83 C          XPNEW=XSIZE
84 C      ELSEIF(XPNEW .LT. 0.0)THEN
85 C          YPNEW=YINTSCT(XPNEW,YPNEW,XPLAST,YPLAST,0.0)
86 C          XPNEW=0.0
87 C      ENDIF
88 C      IF(YPNEW .GT. YSIZE)THEN
89 C          XPNEW=XINTSCT(XPNEW,YPNEW,XPLAST,YPLAST,YSIZE)
90 C          YPNEW=YSIZE
91 C      ELSEIF(YPNEW .LT. 0.0)THEN
92 C          XPNEW=XINTSCT(XPNEW,YPNEW,XPLAST,YPLAST,0.0)
93 C          YPNEW=0.0
94 C      ENDIF
95 C      XPAGE=XPNEW*BOXDIR(1)-YPNEW*BOXDIR(2)
96 C      YPAGE=XPNEW*BOXDIR(2)+YPNEW*BOXDIR(1)
97 C      CALL PLTT(XPAGE,YPAGE,2)
98 C      ENDIF
99 C      IPEN=3
100 C      OUTSIDE=.TRUE.
101 C      SLENGTH=0.0
102 C      ELSE
103 C
104 C      The current point is inside the box.
105 C
106 C      IF(OUTSIDE)THEN
107 C
108 C      The previous point was outside the box. Linearly interpolate to
109 C      find the intersection of the curve entering the box with the box
110 C      boundary.
111 C
112 C      IF(XPLAST .GT. XSIZE)THEN
113 C          YPLAST=YINTSCT(XP,YP,XPLAST,YPLAST,XSIZE)
114 C          XPLAST=XSIZE
115 C      ELSEIF(XPLAST .LT. 0.0)THEN
116 C          YPLAST=YINTSCT(XP,YP,XPLAST,YPLAST,0.0)
117 C          XPLAST=0.0
118 C      ENDIF
119 C      IF(YPLAST .GT. YSIZE)THEN
120 C          XPLAST=XINTSCT(XP,YP,XPLAST,YPLAST,YSIZE)
121 C          YPLAST=YSIZE
122 C      ELSEIF(YPLAST .LT. 0.0)THEN
123 C          XPLAST=XINTSCT(XP,YP,XPLAST,YPLAST,0.0)
124 C          YPLAST=0.0
125 C      ENDIF
126 C      XPAGE=XPLAST*BOXDIR(1)-YPLAST*BOXDIR(2)
127 C      YPAGE=XPLAST*BOXDIR(2)+YPLAST*BOXDIR(1)
128 C      CALL PLTT(XPAGE,YPAGE,3)
129 C      ENDIF
130 C      IPEN=2
131 C      OUTSIDE=.FALSE.
132 C      SLENGTH=SLENGTH+CABS(CMLPX((XP-XPLAST),(YP-YPLAST)))
133 C      ENDIF
134 C      XPAGE=XP*BOXDIR(1)-YP*BOXDIR(2)
135 C      YPAGE=XP*BOXDIR(2)+YP*BOXDIR(1)
136 C      CALL PLTT(XPAGE,YPAGE,IPEN)
137 C      XPLAST=XP
138 C      YPLAST=YP

```

```
139 C
140 C      If "JGRAPH" .LT. 0 plot a centered symbol every 1 inch in arc length.
141 C
142      IF(JGRAPH.LT.0 .AND. SLENGTH.GE.1.0)THEN
143          CALL SYMBOL(XPage,YPage,0.1,ABS(JGRAPH),0.0,-1)
144          SLENGTH=0.0
145      ENDIF
146 1 CONTINUE
147      RETURN
148      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling ENG'
4 $SUBTITLE: '    SUBROUTINE ENG'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE ENG(X,Y,DIV,IEXP)
8 C
9 C     LAST MODIFIED 3/03/85.  BY E. B. JOY
10 C
11 C     "ENG" CALCULATES "Y", "DIV" AND "IEXP" SUCH THAT "X"="Y"*"DIV" AND
12 C     DIV=10**IEXP, WHERE "IEXP" IS SOME MULTIPLE OF 3 AND 1.0 <= ABS("Y")
13 C     < 1000. (ACTUALLY 0.001 <= ABS("Y") < 1000. CHANGE .LT. TO .LE. IN
14 C     "IF(IX.LT.0) IEXP=IEXP-3" TO MAKE THE FIRST INEQUALITY VALID).
15 C
16     IF(X .NE. 0.0)THEN
17         IX=INT(ALOG10(ABS(X)))
18         IEXP=(IX/3)*3
19         IF(IX .LT. 0) IEXP=IEXP-3
20         DIV=10.0**IEXP
21         Y=X/DIV
22     ELSE
23         Y=0.0
24         IEXP=0
25         DIV=1.0
26     ENDIF
27     RETURN
28     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling GRAPH'
4 $SUBTITLE: ' SUBROUTINE GRAPH'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE GRAPH(X,Y,NX,NXMAX,NOPT,XSIZE,YSIZE,BOXDIR,XMAX,XMIN,
8 $ YMAX,YMIN,DELTAX,DELTAY,AXISLBL,NGRAPH,NSPLINE)
9 C
10 C LAST MODIFIED 9/21/87. BY R. WILSON.
11 C ***** 1/09/89. BY R. WILSON.
12 C 1) MOVED PROTECTION FROM FINDING "YMAX"="YMIN" IN THE DATA TO
13 C "AXISXY".
14 C ***** 2/21/89. BY R. WILSON.
15 C 1) NOW USE CALL TO "DRWCURV" TO DRAW EACH CURVE.
16 C ***** 5/05/89. BY R. WILSON.
17 C 1) ADDED CAPABILITY OF ROTATING THE GRAPH "BOX".
18 C 2) THE ROTATION IS INDICATED BY THE ARRAY "BOXDIR" WHICH CONTAINS THE
19 C DIRECTION COSINES OF THE BOX X-AXIS WITH THE PLOTTER AXES.
20 C
21 C THIS IS A GENERAL PURPOSE X-Y PLOT ROUTINE. IT IS CAPABLE OF PLOTTING
22 C LINEAR-LINEAR, SEMILOG(X LINEAR OR Y LINEAR), OR LOG-LOG.
23 C
24 C DESCRIPTION OF PARAMETERS
25 C
26 C "X" AND "Y" ARE ARRAYS CONTAINING THE ABSCISSA AND ORDINATE OF THE CURVE TO
27 C BE PLOTTED. "X" AND "Y" SHOULD BE DIMENSIONED X(NX), Y(NX).
28 C
29 C "NX" IS THE NUMBER OF POINTS IN X AND Y.
30 C
31 C "NOPT" INDICATES HOW THE AXES ARE TO BE LABELED. SEE "AXISXY" FOR DETAILS.
32 C
33 C "XSIZE" AND "YSIZE" ARE THE MAXIMUM X AND Y DIMENSION OF THE PLOT IN
34 C INCHES.
35 C
36 C "BOXDIR" IS A REAL ARRAY WHICH CONTAINS THE DIRECTION COSINES OF THE X-AXIS
37 C OF THE BOX WITH THE PHYSICAL PLOTTER AXES. "BOXDIR(1) HOLDS THE DIRECTION
38 C COSINE W.R.T. THE PLOTTER X-AXIS. "BOXDIR(2) HOLDS THE DIRECTION COSINE
39 C W.R.T. THE PLOTTER Y-AXIS. "BOXDIR" IS USED TO ROTATE THE BOX TO ANY
40 C ANGLE. THE ANGLE OF THE BOX, IN DEGREES, IS STORED IN "BOXDIR(3)" SINCE
41 C THE PLOTTER DOES NOT HAVE A Z-AXIS. "GRAPH" ASSUMES THAT THE BOX ORIGIN
42 C HAS BEEN SET FROM THE CALLING ROUTINE AND THAT NONE OF THE BOX FALLS
43 C OUTSIDE THE PLOTTER MINIMUM LIMITS. NO CHECK IS DONE FOR THIS. IF THE
44 C ORIGIN HAS NOT BEEN SET CORRECTLY AND PART OF THE BOX DOES FALL OUTSIDE THE
45 C PLOTTER MINIMUM LIMITS PROBABLY PARTS OF THE CONTAINED GRAPH WILL NOT BE
46 C PLOTTED CORRECTLY SINCE THE CALCOMP ROUTINES TEND TO LOSE THEIR FIX ON THE
47 C ORIGIN WHEN THIS HAPPENS.
48 C
49 C "XMAX", "XMIN", "YMAX", "YMIN" ARE THE MAXIMUMS AND MINIMUMS TO BE PLOTTED
50 C ON THE RESPECTIVE AXES. THE MINIMUMS ARE PLOTTED AT THE ORIGIN AND THE
51 C MAXIMUMS ARE PLOTTED "XSIZE" AND "YSIZE" INCHES FROM THE RESPECTIVE
52 C ORIGINS. THE MAXIMUMS AND/OR MINIMUMS NEED NOT BE THE ACTUAL MAXIMUMS OR
53 C MINIMUMS OF THE DATA. ALSO "XMAX" DOESN'T NEED TO BE .GT. "XMIN" AND
54 C "YMAX" DOESN'T NEED TO BE .GT. "YMIN". IN ADDITION IF THE AXIS MAXIMUM
55 C AND MINIMUM ARE EQUAL TO EACH OTHER WHEN "GRAPH" IS CALLED THEN "GRAPH"
56 C SCANS THE ARRAY OF VALUES FOR THAT AXIS AND FINDS THE MAXIMUM AND MINIMUM
57 C OF THE DATA. THE DELTA VALUE FOR THAT AXIS IS THEN SET TO ZERO SO THAT
58 C WHEN "TPlot" IS CALLED THE PROGRAM WILL DETERMINE THE TYPE OF SCALING
59 C NECESSARY FOR THAT AXIS.
60 C
61 C "DELTAX" AND "DELTAY" ARE USED IN DETERMINING THE TYPE OF AXIS SCALING
62 C DESIRED. IF A DELTA VALUE IS GREATER THAN ZERO THAT AXIS WILL BE SCALED
63 C LINEARLY AND THE DELTA VALUE WILL BE USED AS THE TIC MARK INTERVAL. IF A
64 C DELTA VALUE IS LESS THAN ZERO, THEN AFTER A CHECK BY "TPlot" TO MAKE SURE
65 C ZERO DOESN'T OCCUR ON THE AXIS ANYWHERE, THE AXIS IS SCALED LOGARITHMICAL-
66 C LY. IF A DELTA VALUE IS ZERO THEN "TPlot" WILL DETERMINE THE TYPE OF
67 C SCALING FOR THAT AXIS BASED ON THE RATIO OF MAX TO MIN ON THAT AXIS (SEE
68 C "TPlot" FOR DETAILS). IF "TPlot" DETERMINES A LINEAR AXIS IS 'POSSIBLE'
69 C THEN THE DELTA VALUE REMAINS ZERO SO THAT THE CALL TO "LINAXIS" WILL
```

```

70 C PRODUCE LINEAR AUTO-SCALING. IF "TPLOT" DETERMINES THAT A LOG AXIS IS
71 C NECESSARY THE DELTA VALUE IS RETURNED AS -1 FROM "TPLOT" SO THAT A LOG AXIS
72 C WILL BE PRODUCED.
73 C
74 C "AXISLBL" IS A ONE DIMENSIONAL CHARACTER ARRAY CONTAINING THE USER SUPPLIED
75 C LABEL FOR THE X AND Y AXES. "AXISLBL(1)" IS USED FOR THE X- AXIS AND
76 C "AXISLBL(2)" IS USED FOR THE Y-AXIS.
77 C
78 C "NGRAPH" IS THE NUMBER OF PLOTS WITHIN THIS BOX. IF ABS(NGRAPH) IS GREATER
79 C THAN 1 MORE THAN ONE GRAPH WILL BE PLOTTED ON THE SAME SET OF AXES. IF
80 C NGRAPH .LT. 0 THEN THE INDIVIDUAL GRAPHS WILL BE LABELED WITH CENTERED
81 C SYMBOLS EVERY 1 INCH IN ARC-LENGTH ALONG THE GRAPH.
82 C
83 C NOTES: THE MAIN PROGRAM SHOULD CONTAIN STATEMENTS WHICH
84 C INITIALIZE THE PLOT SOFTWARE, MOVE THE ORIGIN
85 C UP AND TO THE RIGHT THEN TERMINATE THE PLOT SOFTWARE
86 C WHEN ALL DESIRED PLOTS ARE FINISHED. E.G.,
87 C
88 C CALL PLOTS(IBUF,512,NTAPE,PENCODE)
89 C CALL PLOT(2.0,2.0,-3)
90 C
91 C PROGRAM
92 C
93 C CALL PLOT(0.0,0.0,999)
94 C
95 C PARAMETER (NSPMAX=1024)
96 C REAL X(NXMAX),Y(NXMAX),XSPLINE(NSPMAX),YSPLINE(NSPMAX),BOXDIR(3)
97 C CHARACTER AXISLBL(2)*(*)
98 C
99 C IF "XMAX" .EQ. "XMIN" FIND MAX/MIN OF DATA IN "X(I)" AND USE AS "XMAX" AND
100 C "XMIN". SET "DELTAX" TO 0.0 TO FORCE THE PROGRAM TO DETERMINE THE TYPE OF
101 C SCALING ON THE X-AXIS.
102 C
103 C IF(XMAX .EQ. XMIN)THEN
104 C CALL MAXMIN(X,NX,1,NX,XMAX,XMIN,NX,1,1,1)
105 C DELTAX=0.0
106 C ENDIF
107 C CALL TPLOT(XMAX,XMIN,100.0,DELTAX)
108 C
109 C IF "YMAX" .EQ. "YMIN" FIND MAX/MIN OF DATA IN Y(I) AND USE AS "YMAX" AND
110 C "YMIN". IF MORE THAN 1 PLOT IS TO BE MADE IN THIS BOX USE ALL OF THE
111 C Y-DATA FOR THIS BOX IN FINDING THE MAX/MIN OF THE DATA; STORE THESE Y
112 C VALUES IN A SCRATCH FILE AND READ THE Y DATA FROM FROM THIS SCRATCH FILE
113 C WHEN PLOTTING. SET "DELTAY"=0.0 TO FORCE THE PROGRAM TO DETERMINE THE TYPE
114 C OF SCALING.
115 C
116 C IYUNIT=5
117 C IF(YMAX .EQ. YMIN)THEN
118 C CALL MAXMIN(Y,NX,1,NX,YMAX,YMIN,NX,1,1,1)
119 C DELTAY=0.0
120 C IF(ABS(NGRAPH) .GT. 1)THEN
121 C OPEN(UNIT=2,STATUS='SCRATCH')
122 C WRITE(2,*)NX
123 C WRITE(2,*)(X(I),I=1,NX,1)
124 C WRITE(2,*)(Y(I),I=1,NX,1)
125 C IYUNIT=2
126 C DO 1 JGRAPH=2,ABS(NGRAPH),1
127 C READ(5,*)NX
128 C READ(5,*)(X(I),I=1,NX,1)
129 C READ(5,*)(Y(I),I=1,NX,1)
130 C WRITE(2,*)NX
131 C WRITE(2,*)(X(I),I=1,NX,1)
132 C WRITE(2,*)(Y(I),I=1,NX,1)
133 C CALL MAXMIN(Y,NX,1,NX,YMAXP,YMINP,NX,1,1,1)
134 C YMAX=AMAX1(YMAX,YMAXP)
135 C YMIN=AMIN1(YMIN,YMINP)
136 C 1 CONTINUE
137 C REWIND(2)
138 C READ(2,*)NX

```

```
139 C   READ(2,*)(X(I),I=1,NX,1)
140       READ(2,*)(Y(I),I=1,NX,1)
141       ENDIF
142       ENDIF
143       CALL TPLLOT(YMAX,YMIN,100.0,DELTAY)
144 C
145 C   DRAW BOX, ANNOTATE AXES, INSURE XSCALE AND YSCALE HAVE CORRECT SIGN, AND
146 C   CONVERT AXIS MAX/MIN TO LOGARITHMS IF NECESSARY
147 C
148       CALL AXISXY(NOPT,XSIZE,YSIZE,BOXDIR,XMAX,XMIN,YMAX,YMIN,
149 $   DELTAX,DELTAY,AXISLBL,XSCALE,YSCALE)
150       XSCALE=SIGN(XSCALE,(XMAX-XMIN))
151       YSCALE=SIGN(YSCALE,(YMAX-YMIN))
152       IF(DELTAX .LT. 0.0)THEN
153         XMAX=ALOG10(ABS(XMAX))
154         XMIN=ALOG10(ABS(XMIN))
155         CALL LOGCON(X,NX)
156       ENDIF
157       IF(DELTAY .LT. 0.0)THEN
158         YMAX=ALOG10(ABS(YMAX))
159         YMIN=ALOG10(ABS(YMIN))
160       ENDIF
161 C
162 C   PLOT THE CURVES IN THIS BOX.
163 C
164       DO 3 JGRAPH=1,ABS(NGRAPH),1
165         IF(JGRAPH .GT. 1)READ(IYUNIT,*)(Y(I),I=1,NX,1)
166 C       IF(JGRAPH .GT. 1)THEN
167 C         READ(IYUNIT,*)NX
168 C         READ(IYUNIT,*)(X(I),I=1,NX,1)
169 C         READ(IYUNIT,*)(Y(I),I=1,NX,1)
170 C       ENDIF
171         IF(DELTAY .LT. 0.0)CALL LOGCON(Y,NX)
172         CALL SPLINE(X,Y,NX,XSPLINE,YSPLINE,NSP,NSP,NSPLINE,JGRAPH)
173         CALL DRWCURV(XSPLINE,YSPLINE,NSP,XSIZE,YSIZE,BOXDIR,XMIN,YMIN,
174 $   XSCALE,YSCALE,SIGN(JGRAPH,NGRAPH))
175 3 CONTINUE
176       IF(IYUNIT .NE. 5)CLOSE(IYUNIT)
177       RETURN
178       END
```



```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling INTRPL'
4 $SUBTITLE: ' SUBROUTINE INTRPL'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE INTRPL(X,Y,NX,XSPLINE,YSPLINE,NXSPLIN)
8 C
9 C LAST MODIFIED 7/05/87. BY R. WILSON.
10 C ***** 12/01/88. BY R. WILSON.
11 C 1) MOVED ERROR MESSAGES INTO FORMAT STATEMENTS
12 C 2) ADDED LOGICAL VARIABLE "PRGSTOP" SO THAT ALL ERROR CONDITIONS
13 C WOULD BE REPORTED AT ONCE.
14 C ***** 6/29/89. BY R. WILSON.
15 C 1) UPDATED THE ERROR MESSAGE FORMAT TO BE CONSISTENT WITH THOSE IN
16 C OTHER LIBRARY ROUTINES.
17 C
18 C "INTRPL" INTERPOLATES FROM VALUES OF THE FUNCTION GIVEN AS ORDINATES OF
19 C INPUT DATA POINTS IN AN X-Y PLANE AND FOR A GIVEN SET OF X VALUES
20 C (ABSCISSAS), THE VALUES OF A SINGLE-VALUED FUNCTION Y=Y(X). NOTE: THIS
21 C IS A MODIFIED VERSION OF THE ROUTINE DESCRIBED BY H. AKIMA IMPLEMENTING
22 C ALGORITHM 433 FROM THE COMM. OF THE ACM. IMSL REFERENCES THIS WHEN
23 C DISCUSSING IT'S ROUTINE "IQHSCU" AND CALLS THIS PROCEDURE QUASI-CUBIC
24 C HERMITE INTERPOLATION. "INTRPL" IS A LITTLE MORE GENERAL THAN THE IMSL
25 C ROUTINE AND IT ALSO COMPUTES THE VALUES OF THE 'SPLINE'. THE IMSL ROUTINE
26 C REQUIRES A CALL TO ANOTHER SUBPROGRAM TO DO THIS.
27 C
28 C DEFINITION OF PARAMETERS
29 C
30 C "X AND "Y ARE THE INPUT ARRAYS CONTAINING THE INPUT DATA POINTS. "X"
31 C CONTAINS THE ABSCISSAS AND "Y" CONTAINS THE ORDINATES. THE "X(1)" MUST BE
32 C IN ASCENDING ORDER. A CHECK IS MADE FOR THIS AND THE PROGRAM TERMINATES
33 C IF NOT TRUE.
34 C
35 C "NX" IS THE NUMBER OF INPUT DATA POINTS AND THE DIMENSION OF THE "X" AND
36 C "Y" ARRAYS.
37 C
38 C "XSPLINE" IS THE INPUT ARRAY CONTAINING THE ABSCISSA VALUES AT WHICH THE
39 C INTERPOLATED ORDINATE VALUES ARE DESIRED. THEY NEED NOT BE ORDERED BUT
40 C THE INTERPOLATION RUNS FASTER IF THEY ARE.
41 C
42 C "YSPLINE" IS THE OUTPUT ARRAY CONTAINING THE INTERPOLATED ORDINATE VALUES
43 C CORRESPONDING THE ABSCISSA VALUES IN "XSPLINE".
44 C
45 C "NXSPLIN" IS THE NUMBER OF DESIRED INTERPOLATED POINTS AND THE DIMENSION
46 C OF "XSPLINE" AND "YSPLINE". NXSPIN MUST BE .GE. 1. A CHECK IS MADE FOR
47 C THIS AND THE PROGRAM TERMINATES IF NOT TRUE.
48 C
49 REAL X(NX),Y(NX),XSPLINE(NXSPLIN),YSPLINE(NXSPLIN)
50 REAL M1,M2,M3,M4,M5
51 LOGICAL PRGSTOP
52 EQUIVALENCE (P0,X3),(Q0,Y3),(Q1,T3)
53 C
54 C IT APPEARS THAT THE FOLLOWING EQUIVALENCE STATEMENTS ARE USED JUST TO SAVE
55 C MEMORY SPACE. (commented out here to prevent problems with using
56 C $STORAGE:2 on Microsoft compiler command)
57 C EQUIVALENCE (XSPLINK,DX),(IMIN,X2,A1,M1),(IMAX,X5,A5,M5)
58 C EQUIVALENCE (J,SW,SA),(Y2,W2,W4,Q2),(Y5,W3,Q3)
59 C using these EQUIVALENCE statements instead.
60 EQUIVALENCE (XSPLINK,DX),(X2,A1),(X5,A5),(IMAX,M5)
61 EQUIVALENCE (SW,SA),(Y2,W2,W4,Q2),(Y5,W3,Q3)
62 C
63 C CHECK FOR CORRECT INPUTS.
64 C
65 NXM1=NX-1
66 NXP1=NX+1
67 PRGSTOP=.FALSE.
68 IF(NX .LT. 2)THEN
69 WRITE(*,100)NX

```

```

70 100  FORMAT(1X,'***** ERROR- program terminated in INTRPL.'/
71      $      5X,'NX(= ',15,') NOT .GE. 2.')
```

72 PRGSTOP=.TRUE.

73 ENDIF

74 IF(NXSPLIN .LE. 0)THEN

75 WRITE(\*,101)NXSPLIN

76 101 FORMAT(1X,'\*\*\*\*\* ERROR- program terminated in INTRPL.'/

77 \$ 7X,'NXSPLIN(= ',15,') .LE. 0.')

78 PRGSTOP=.TRUE.

79 ENDIF

80 IF(PRGSTOP)STOP

81 C

82 C CHECK THAT ABSCISSA VALUES ARE IN ASCENDING ORDER.

83 C

84 DO 11 I=2,NX,1

85 IF(X(I-1) .GE. X(I))THEN

86 WRITE(\*,102)I-1,X(I-1),I,X(I)

87 102 FORMAT(1X,'\*\*\*\*\* ERROR - program terminated in INTRPL.'/

88 \$ 7X,2('X(',15,')= ',1PG14.7,:,' .LE. '))

89 STOP

90 ENDIF

91 11 CONTINUE

92 C

93 C PERFORM SPLINE INTERPOLATION.

94 C

95 IPV=0

96 DO 80 K=1,NXSPLIN,1

97 XSPLINK=XSPLINE(K)

98 C

99 C LOCATE THE DESIRED POINT.

100 C

101 IF(NX .EQ. 2)THEN

102 I=2

103 ELSEIF(XSPLINK .GE. X(NX))THEN

104 I=NXP1

105 ELSEIF(XSPLINK .LT. X(1))THEN

106 I=1

107 ELSE

108 IMIN=2

109 IMAX=NX

110 21 I=(IMIN+IMAX)/2

111 IF(XSPLINK .LT. X(I))THEN

112 IMAX=I

113 ELSE

114 IMIN=I+1

115 ENDIF

116 IF(IMAX .GT. IMIN) GO TO 21

117 I=IMAX

118 ENDIF

119 C

120 C CHECK IF I=IPV.

121 C

122 IF(I .NE. IPV)THEN

123 IPV=I

124 C

125 C PICK UP NECESSARY X AND Y VALUES AND ESTIMATE THEM IF NECESSARY.

126 C

127 J=I

128 IF(J .EQ. 1)J=2

129 IF(J .EQ. NXP1)J=NX

130 X3=X(J-1)

131 Y3=Y(J-1)

132 X4=X(J)

133 Y4=Y(J)

134 A3=X4-X3

135 M3=(Y4-Y3)/A3

136 IF(NX .NE. 2)THEN

137 IF(J .NE. 2)THEN

138 X2=X(J-2)

```

139          Y2=Y(J-2)
140          A2=X3-X2
141          M2=(Y3-Y2)/A2
142      ENDIF
143      IF(J .NE. NX)THEN
144          X5=X(J+1)
145          Y5=Y(J+1)
146          A4=X5-X4
147          M4=(Y5-Y4)/A4
148          IF(J .EQ. 2)M2=M3+M3-M4
149      ELSE
150          M4=M3+M3-M2
151      ENDIF
152  ELSE
153      M2=M3
154      M4=M3
155  ENDIF
156  IF(J .GT. 3)THEN
157      A1=X2-X(J-3)
158      M1=(Y2-Y(J-3))/A1
159  ELSE
160      M1=M2+M2-M3
161  ENDIF
162  IF(J .LT. NXM1)THEN
163      A5=X(J+2)-X5
164      M5=(Y(J+2)-Y5)/A5
165  ELSE
166      M5=M4+M4-M3
167  ENDIF
168  C
169  C      NUMERICAL DIFFERENTIATION.
170  C
171      IF(I .NE. NXP1)THEN
172          W2=ABS(M4-M3)
173          W3=ABS(M2-M1)
174          SW=W2+W3
175          IF(SW .EQ. 0.0)THEN
176              W2=0.5
177              W3=0.5
178              SW=1.0
179          ENDIF
180          T3=(W2*M2+W3*M3)/SW
181      ENDIF
182      IF(I .NE. 1)THEN
183          W3=ABS(M5-M4)
184          W4=ABS(M3-M2)
185          SW=W3+W4
186          IF(SW .EQ. 0.0)THEN
187              W3=0.5
188              W4=0.5
189              SW=1.0
190          ENDIF
191          T4=(W3*M3+W4*M4)/SW
192      ENDIF
193      IF(I .EQ. NXP1)THEN
194          T3=T4
195          SA=A2+A3
196          T4=0.5*(M4+M5-A2*(A2-A3)*(M2-M3)/(SA*SA))
197          X3=X4
198          Y3=Y4
199          A3=A2
200          M3=M4
201      ENDIF
202      IF(I .EQ. 1)THEN
203          T4=T3
204          SA=A3+A4
205          T3=0.5*(M1+M2-A4*(A3-A4)*(M3-M4)/(SA*SA))
206          X3=X3-A4
207          Y3=Y3-M2*A4

```

```
208          A3=A4
209          M3=M2
210          ENDIF
211 C
212 C          DETERMINE THE COEFFICIENTS.
213 C
214 60          Q2=(2.0*(M3-T3)+M3-T4)/A3
215           Q3=(-M3-M3+T3+T4)/(A3*A3)
216          ENDIF
217 C
218 C          COMPUTE THE POLYNOMIAL.
219 C
220          DX=XSPLINK-P0
221          YSPLINE(K)=Q0+DX*(Q1+DX*(Q2+DX*Q3))
222 80 CONTINUE
223          RETURN
224          END
```

```

1  $PAGESIZE:80
2  $LINESIZE:132
3  $MESSAGE:'Compiling LINAXIS'
4  $SUBTITLE: '    SUBROUTINE LINAXIS'
5  $PAGE
6  $NOTRUNCATE
7      SUBROUTINE LINAXIS(XMAX,XMIN,DELTAX,HEIGHT,TICSIZE,
8          $  ANGLE,XSIZE,XORIGIN,IAXIS,XSCALE,YLPRIME)
9  C
10 C  LAST MODIFIED  3/26/87.  BY R. WILSON.
11 C  ***** 12/05/88.  BY R. WILSON.
12 C      1) REMOVED "CHARTYP" FROM ARGUMENT LIST
13 C      2) "LINAXIS" NOW DRAWS THE AXIS LINE
14 C  ***** 1/10/89.  BY R. WILSON.
15 C      1) NO LONGER SAVE SIGN OF "DELTAX" SINCE "DELTAX" IS NON-NEGATIVE
16 C          (POSITIVE OR ZERO) UPON ENTRY AND WANT IT POSITIVE UPON EXIT.
17 C
18 C  "LINAXIS" ANNOTATES THE AXIS WITH A LINEAR SCALE.
19 C
20      REAL XORIGIN(2)
21      INTEGER NUMDECR
22      CHARACTER CENGX*80,IAXIS*8
23      LOGICAL LBLAXIS,LBLTIC
24      COMMON/LINAXC/MAXDIG
25 C
26 C  "INTRND(X,DEL)" IS A STATEMENT FUNCTION INSURING THAT THE INT FUNCTION
27 C  IS PERFORMED ON "X" ROUNDED TO APPROXIMATELY ALOG10(DEL).
28 C
29      INTRND(X,DEL)=INT(X+SIGN(DEL,X))
30 C
31 C  IF "DELTAX"= 0.0 FIND A VALUE FOR "DELTAX" AND NEW VALUES FOR "XMAX" AND
32 C  "XMIN".  MAKE SURE "DELTAX" HAS THE SAME SIGN AS ("XMAX"-XMIN).  "DELTAX"
33 C  WILL BE MADE POSITIVE BEFORE RETURNING.  COMPUTE SCALE FACTOR FOR THIS AXIS
34 C  (THIS WILL BE MADE POSITIVE BEFORE RETURNING).  COMPUTE SINE AND COSINE OF
35 C  "ANGLE" FOR ROTATION COMPUTATION.
36 C
37      IF(DELTAX .EQ. 0.0)THEN
38          CALL SCALE1(XMAX,XMIN,.TRUE.,5,XMAXP,XMINP,DELTAX)
39          XMAX=XMAXP
40          XMIN=XMINP
41      ENDIF
42      DELTAX=SIGN(DELTAX,(XMAX-XMIN))
43      XSCALE=XSIZE/(XMAX-XMIN)
44      COSANGL=COSD(ANGLE)
45      SINANGL=SIND(ANGLE)
46 C
47 C  DETERMINE IF TICMARKS SHOULD BE PLOTTED.  DETERMINE IF NUMBERS SHOULD
48 C  BE PLOTTED; IF SO INITIALIZE REQ'D VARIABLES, AND COMPUTE FACTORS FOR
49 C  ENGINEERING NOTATION.
50 C
51      LBLTIC=.TRUE.
52      IF(ABS(TICSIZE) .LE. 0.005)LBLTIC=.FALSE.
53      IF(IAXIS .EQ. 'NOLABEL')THEN
54          LBLAXIS=.FALSE.
55      ELSE
56          LBLAXIS=.TRUE.
57          READ(IAXIS(5:6),'(I2)')NSIGN
58          READ(IAXIS(7:8),'(I2)')NSIDE
59          YSPACE=NSIDE*(0.8*HEIGHT)
60          IF(IAXIS(1:4) .EQ. 'PARL')THEN
61              ANGNUM=ANGLE+((1-NSIGN)/2.0)*180.0
62              IF(NSIDE .NE. NSIGN)THEN
63                  YPRIME=YSPACE+NSIDE*HEIGHT
64                  YLPRIME=YPRIME
65              ELSE
66                  YPRIME=YSPACE
67                  YLPRIME=YSPACE+NSIDE*HEIGHT
68              ENDIF
69          ELSEIF(IAXIS(1:4) .EQ. 'PERP')THEN

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70      ANGNUM=ANGLE-NSIGN*90.0
71      YLPRIME=0.0
72      ENDIF
73 C
74 C      DETERMINE THE FACTOR, DIVX, BY WHICH ALL NUMBERS APPEARING ON THE
75 C      AXIS MUST BE MULTIPLIED TO OBTAIN THEIR TRUE VALUE
76 C
77      IF(XMAX.EQ.0.0)THEN
78          CALL ENG(XMIN,ENGXM,DIVX,IEXPX)
79      ELSEIF(XMIN.EQ.0.0)THEN
80          CALL ENG(XMAX,ENGMX,DIVX,IEXPX)
81      ELSE
82          CALL ENG(XMAX,ENGMX,DIVMX,IEXPXM)
83          CALL ENG(XMIN,ENGXM,DIVXM,IEXPXM)
84          DIVX=AMAX1(DIVMX,DIVXM)
85      ENDIF
86      ENGDX=DELTA/DIVX
87      ENGMX=XMAX/DIVX
88      ENGXM=XMIN/DIVX
89 C
90 C      DETERMINE NUMBER OF DIGITS TO RIGHT OF DECIMAL IN THE ENGINEERING
91 C      FORM OF THE NUMBERS TO PLOTTED ON THE AXIS.
92 C
93      NDEC=MIN(MAX(NUMDECR(ENGDX,MAXDIG),NUMDECR(ENGMX,MAXDIG),
94 $      NUMDECR(ENGXM,MAXDIG)),MAXDIG)
95      ENDIF
96 C
97 C      ANNOTATE AXIS.
98 C
99      NTX=INTRND((XMAX-XMIN)/DELTA,2.0E-5)
100     NTX1=NTX+1
101     IF(XMAX .GT. XMIN)THEN
102         XTMIN=XMIN
103     ELSE
104         XTMIN=XMAX-NTX*DELTA
105     ENDIF
106 C
107 C      DRAW AXIS LINE.
108 C
109     CALL PLOT(XORIGIN(1),XORIGIN(2),3)
110     XPAGE=XSIZE*COSANGL+XORIGIN(1)
111     YPAGE=XSIZE*SINANGL+XORIGIN(2)
112     CALL PLOT(XPAGE,YPAGE,2)
113 C
114 C      ANNOTATE THE AXIS LINE.
115 C
116     DO 7 I=1,NTX1,1
117         XT=XTMIN+(I-1)*DELTA
118         XT1=(XT-XMIN)*XSCALE
119         IF(LBLAXIS)THEN
120 C
121 C             PLOT NUMBER BY TIC MARK.
122 C
123             ENGX=XT/DIVX
124             CALL NUMCHAR(ENGX,NDEC,0,CENGX,NCHAR)
125             CALL SLENRW(XLEN,HEIGHT,CENGX,NCHAR)
126             IF(IAXIS(1:4) .EQ. 'PARL')THEN
127                 XPRIME=XT1-NSIGN*XLEN/2.0
128             ELSEIF(IAXIS(1:4) .EQ. 'PERP')THEN
129                 XPRIME=XT1-NSIGN*HEIGHT/2.0
130             IF(NSIGN .NE. NSIDE)THEN
131                 YPRIME=YSPACE
132                 IF(ENGX.GE.0.0 .AND. (XMAX.LT.0.0 .OR. XMIN.LT.0.0))
133 $                     YPRIME=YPRIME+NSIDE*HEIGHT
134                 YLPRIME=NSIDE*AMAX1(ABS(YLPRIME),
135 $                     ABS(YPRIME+NSIDE*XLEN))
136             ELSE
137                 YPRIME=YSPACE+NSIDE*XLEN
138                 YLPRIME=NSIDE*AMAX1(ABS(YLPRIME),

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```
139      $      ABS(YPRIME))
140      ENDIF
141      ENDIF
142      XPAGE=XPRIME*COSANGL-YPRIME*SINANGL+
143      $      XORIGIN(1)
144      YPAGE=XPRIME*SINANGL+YPRIME*COSANGL+
145      $      XORIGIN(2)
146      CALL SYMBOL(XPAGE,YPAGE,HEIGHT,CENGX,ANGNUM,NCHAR)
147      ENDIF
148      IF(XTI.GT. 0.005 .AND. XTI.LT.(XSIZE-0.005) .AND. LBLTIC)THEN
149 C
150 C      PLOT TIC MARK.
151 C
152      XPAGE=XTI*COSANGL+XORIGIN(1)
153      YPAGE=XTI*SINANGL+XORIGIN(2)
154      CALL PLOT(XPAGE,YPAGE,3)
155      XPAGE=XPAGE-TICSIZE*SINANGL
156      YPAGE=YPAGE+TICSIZE*COSANGL
157      CALL PLOT(XPAGE,YPAGE,2)
158      ENDIF
159      7 CONTINUE
160 C
161 C      COMPUTE Y-COORDINATE (BEFORE ROTATION) OF BOTTOM EDGE OF AXIS
162 C      LETTERING ASSUMING LETTERING IS DESIRED ON SAME SIDE OF AXIS
163 C      AS THE NUMBERS.
164 C
165      YLPRIME=YLPRIME+YSPACE+((NSIDE-1)/2)*HEIGHT
166 C
167 C      MAKE SURE "XSCALE" AND "DELTAX" ARE POSITIVE.
168 C
169      XSCALE=ABS(XSCALE)
170      DELTAX=ABS(DELTAX)
171      RETURN
172      END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling LOGAXIS'
4 $SUBTITLE: ' SUBROUTINE LOGAXIS'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE LOGAXIS(XMAX,XMIN,EHT,HEIGHT,TICSIZE,ANGLE,
8 $ XSIZE,XORIGIN,IAXIS,XSCALE,YLPRIME)
9 C
10 C LAST MODIFIED 7/05/87. BY R. WILSON.
11 C ***** 12/05/88. BY R. WILSON.
12 C 1) Removed "chartyp" from argument list.
13 C 2) "LOGAXIS" now draws the axis line.
14 C ***** 6/29/89. BY R. WILSON.
15 C 1) Updated the error message format to be consistent with those in
16 C other library routines.
17 C
18 C "LOGAXIS" annotates the axis with a log scale and returns an "XSCALE" for
19 C this axis for use when plotting the data. "XMAX" and "XMIN" may be
20 C modified as described below (but not converted to logarithms).
21 C
22 REAL XORIGIN(2),LOGTEN(10)
23 CHARACTER CEXP*80,CHARX*21,IAXIS*8,CSYM*3
24 EQUIVALENCE (CHARX,CEXP(1:21))
25 LOGICAL LBLAXIS,LBLTIC
26 DATA LOGTEN/0.0,0.301029995664,0.4771212547197,0.602059991328,
27 $ 0.698970004336,0.7781512503836,0.8450980400143,0.9030899869919,
28 $ 0.9542425094393,1.0/
29 C
30 C Initialize "CSYM", the character string representation of 10 or -10.
31 C
32 IF(XMAX.GT.0.0 .AND. XMIN.GT.0.0)THEN
33 CSYM(1:2)='10'
34 NSYM=2
35 ELSEIF(XMAX.LT.0.0 .AND. XMIN.LT.0.0)THEN
36 CSYM(1:3)='-10'
37 NSYM=3
38 XMAX=-XMAX
39 XMIN=-XMIN
40 ELSE
41 WRITE(*,100)
42 100 FORMAT(1X,'***** ERROR - program termination in LOGAXIS.'/
43 $ 7X,'MAX and MIN do not have the SAME sign.')
44 STOP
45 ENDIF
46 C
47 C Determine a modified "XMIN"="K"*10**"NDECMIN" such that the new "XMIN" is
48 C a greatest lower bound of the old "xmin". Also determine a modified
49 C "XMAX"="KMAX"*10**"NDECMAX" such that the new "XMAX" is a least upper
50 C bound of the old "XMAX". "K" and "KMAX" are integers between 1 and 9.
51 C "NDECMIN" and "NDECMAX" are integers.
52 C
53 WRITE(CHARX,'(1PE21.14)')XMIN
54 READ(CHARX(19:21),'(I3)')NDECMIN
55 READ(CHARX(1:2),'(I2)')KMIN
56 WRITE(CHARX,'(1PE21.14)')XMAX
57 READ(CHARX(19:21),'(I3)')NDECMAX
58 READ(CHARX(1:2),'(I2)')KMAX
59 C
60 C If "XMAX" .GT. "XMIN" increase "KMAX" if necessary and make sure "KMAX"
61 C and "KMIN" are between 1 and 9 inclusive. If "XMAX" .LT. "XMIN" increase
62 C "KMIN" if necessary and make sure "KMAX" and "KMIN" are between 2 and 10
63 C inclusive.
64 C
65 IF(XMAX .GT. XMIN)THEN
66 IF(MOD((XMAX/10.0**NDECMAX),1.0) .GT. 1.0E-14)THEN
67 KMAX=KMAX+1
68 IF(KMAX .EQ. 10)THEN
69 KMAX=1

```



```

70         NDECMAX=NDECMAX+1
71     ENDIF
72 ENDIF
73 NDECDL=1
74 KSTOP=9
75 ELSE
76     IF(MOD((XMIN/10.0*NDECMIN),1.0) .GT. 2.0E-5)KMIN=KMIN+1
77     IF(KMIN .EQ. 1)THEN
78         KMIN=10
79         NDECMIN=NDECMIN-1
80     ENDIF
81     IF(KMAX .EQ. 1)THEN
82         KMAX=10
83         NDECMAX=NDECMAX-1
84     ENDIF
85     NDECDL=-1
86     KSTOP=2
87 ENDIF
88 C
89 C   Compute new "XMAX" and "XMIN" and convert to logarithms (anti-log's will
90 C   be taken and signs will be restored before returning). Compute scale
91 C   factor for this axis (this will be made positive before returning),
92 C   compute cosine and sine of "angle" for rotation computation.
93 C
94     XMAX=LOGTEN(KMAX)+NDECMAX
95     XMIN=LOGTEN(KMIN)+NDECMIN
96     XSCALE=XSIZE/(XMAX-XMIN)
97     COSANGL=COSD(ANGLE)
98     SINANGL=SIND(ANGLE)
99 C
100 C   Determine if ticmarks should be plotted. Determine if numbers should be
101 C   plotted; if so initialize req'd variables.
102 C
103     LBLTIC=.TRUE.
104     IF(ABS(TICSIZE) .LE. 0.005)LBLTIC=.FALSE.
105     IF(IAXIS .EQ. 'NOLABEL')THEN
106         LBLAXIS=.FALSE.
107     ELSE
108         LBLAXIS=.TRUE.
109         READ(IAXIS(5:6),'(I2)')NSIGN
110         READ(IAXIS(7:8),'(I2)')NSIDE
111         YSPACE=NSIDE*(0.8*HEIGHT)
112         IF(IAXIS(1:4) .EQ. 'PARL')THEN
113             ANGNUM=ANGLE+((1-NSIGN)/2)*180.0
114             IF(NSIDE .NE. NSIGN)THEN
115                 YPRIME=YSACE+NSIDE*(HEIGHT+EHT/2.0)
116                 YLPRIME=YPRIME
117             ELSE
118                 YPRIME=YSACE
119                 YLPRIME=YSACE+NSIDE*(HEIGHT+EHT/2.0)
120             ENDIF
121             YPRIMEE=YPRIME+NSIGN*(HEIGHT-EHT/2.0)
122         ELSEIF(IAXIS(1:4) .EQ. 'PERP')THEN
123             ANGNUM=ANGLE-NSIGN*90.0
124             YLPRIME=0.0
125         ENDIF
126     ENDIF
127 C
128 C   Draw axis line.
129 C
130     CALL PLOT(XORIGIN(1),XORIGIN(2),3)
131     XPAGE=XSIZE*COSANGL+XORIGIN(1)
132     YPAGE=XSIZE*SINANGL+XORIGIN(2)
133     CALL PLOT(XPAGE,YPAGE,2)
134 C
135 C   Annotate axis line.
136 C
137     CALL SLENRW(XLEN10,HEIGHT,CSYM,NSYM)
138     CALL SLENRW(XLMINUS,EHT,'-',1)

```

```

139      KSTART=KMIN
140      DO 8 NDEC=NDECMIN,NDECMAX,NDECDEL
141          IF((KSTART.EQ.1 .OR. KSTART.EQ.10) .AND. LBLAXIS)THEN
142      C
143      C          Plot power of ten below major tick mark.
144      C
145          IF(NDECDEL .EQ. 1)THEN
146              XT=NDEC
147          ELSE
148              XT=NDEC+1
149          ENDIF
150          XT1=(XT-XMIN)*XSCALE
151          CALL NUMCHAR(XT,0,0,CEXP,NCHARLG)
152          CALL SLENRW(XLEN,EHT,CEXP,NCHARLG)
153          XLEN=XLEN+XLEN10
154          IF(IAXIS(1:4) .EQ. 'PARL')THEN
155              XPRIME=XT1-NSIGN*XLEN/2.0
156              XPRIMEE=XPRIME+NSIGN*(XLEN10+0.01)
157          ELSEIF(IAXIS(1:4) .EQ. 'PERP')THEN
158              XPRIME=XT1-NSIGN*HEIGHT/2.0
159              XPRIMEE=XPRIME+NSIGN*(HEIGHT-EHT/2.0)
160              IF(NSIGN .NE. NSIDE)THEN
161                  YPRIME=YSPACE
162                  YLPRIME=NSIDE*AMAX1(ABS(YLPRIME),
163      $                      ABS(YPRIME+NSIDE*XLEN))
164              ELSE
165                  YPRIME=YSPACE+NSIDE*XLEN
166                  IF(XT.GE.0.0 .AND. MIN(NDECMAX,NDECMIN).LT.0)
167      $                      YPRIME=YPRIME+NSIDE*XLMINUS
168                  YLPRIME=NSIDE*AMAX1(ABS(YLPRIME),
169      $                      ABS(YPRIME))
170              ENDIF
171              YPRIMEE=YPRIME-NSIGN*(XLEN10+0.01)
172          ENDIF
173          XPAGE=XPRIME*COSANGL-YPRIME*SINANGL+
174      $          XORIGIN(1)
175          YPAGE=XPRIME*SINANGL+YPRIME*COSANGL+
176      $          XORIGIN(2)
177          CALL SYMBOL(XPAGE,YPAGE,HEIGHT,CSYM,ANGNUM,NSYM)
178          XPRIMEE=XPRIMEE*COSANGL-YPRIMEE*SINANGL+
179      $          XORIGIN(1)
180          YPAGE=XPRIMEE*SINANGL+YPRIMEE*COSANGL+
181      $          XORIGIN(2)
182          CALL SYMBOL(XPAGE,YPAGE,EHT,CEXP,ANGNUM,NCHARLG)
183      ENDIF
184      IF(NDEC .EQ. NDECMIN)KSTART=KMIN+NDECDEL
185      IF(NDEC .EQ. NDECMAX)KSTOP=KMAX-NDECDEL
186      IF((NDECDEL*(KSTOP-KSTART)).GE.0 .AND. LBLTIC)THEN
187      C
188      C          Plot tick marks.
189      C
190      DO 7 J= KSTART,KSTOP,NDECDEL
191          XT=LOGTEN(J)+NDEC
192          XT1=(XT-XMIN)*XSCALE
193          IF(J.EQ.1 .OR. J.EQ.10)THEN
194              TICMARK=TICSIZE
195          ELSE
196              TICMARK=TICSIZE/2.0
197          ENDIF
198          XPAGE=XT1*COSANGL+XORIGIN(1)
199          YPAGE=XT1*SINANGL+XORIGIN(2)
200          CALL PLOT(XPAGE,YPAGE,3)
201          XPAGE=XPAGE-TICMARK*SINANGL
202          YPAGE=YPAGE+TICMARK*COSANGL
203          CALL PLOT(XPAGE,YPAGE,2)
204      7      CONTINUE
205      ENDIF
206      IF(NDECDEL .EQ. 1)THEN
207          KSTART=1

```

```
208      ELSEIF(NDECDEL .EQ. -1)THEN
209          KSTART=10
210      ENDIF
211      & CONTINUE
212  C
213  C   Compute y-coordinate (before rotation) of bottom edge of axis lettering
214  C   assuming lettering is desired on same side of axis as the numbers.
215  C
216      YLPRIME=YLPRIME+YSPACE+((NSIDE-1)/2)*HEIGHT
217  C
218  C   Make sure "XSCALE" is positive. Set "XMAX" and "XMIN" To modified values
219  C   and restore old sign.
220  C
221      XSCALE=ABS(XSCALE)
222      IF(CSYM(1:1) .EQ. '-')THEN
223          CHARX(1:1)='- '
224      ELSE
225          CHARX(1:1)= ' '
226      ENDIF
227      CHARX(3:18)='.000000000000000E'
228      IF(KMAX .EQ. 10)THEN
229          CHARX(2:2)='1'
230          WRITE(CHARX(19:21),'(13)')NDECMAX+1
231      ELSE
232          WRITE(CHARX(2:2),'(11)')KMAX
233          WRITE(CHARX(19:21),'(13)')NDECMAX
234      ENDIF
235      READ(CHARX,'(1PE21.14)')XMAX
236      IF(KMIN .EQ. 10)THEN
237          CHARX(2:2)='1'
238          WRITE(CHARX(19:21),'(13)')NDECMIN+1
239      ELSE
240          WRITE(CHARX(2:2),'(11)')KMIN
241          WRITE(CHARX(19:21),'(13)')NDECMIN
242      ENDIF
243      READ(CHARX,'(1PE21.14)')XMIN
244      RETURN
245      END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling LOGCON'
4 $SUBTITLE: ' SUBROUTINE LOGCON'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE LOGCON(X,NX)
8 C
9 C LAST MODIFIED 10/07/85. BY R. WILSON.
10 C
11 PARAMETER (ZERO=1.0E-12)
12 REAL X(NX)
13 DO 1 I=1,NX,1
14 AX=ABS(X(I))
15 IF(AX .GT. ZERO)THEN
16 X(I)=ALOG10(AX)
17 ELSE
18 X(I)=-12.0
19 ENDIF
20 1 CONTINUE
21 RETURN
22 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling MAXMIN'
4 $SUBTITLE: '    SUBROUTINE MAXMIN'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE MAXMIN(ARRAY,NX,NY,NXMAX,AMAX,AMIN,IMAX,IMIN,JMAX,JMIN)
8 C
9 C     LAST MODIFIED 8/15/86. BY R. WILSON.
10 C
11     REAL ARRAY(NXMAX,*),AMAX,AMIN
12 C
13 C     "MAXMIN" FINDS THE MAXIMUM AND MINIMUM OF THE DATA IN THE REAL ARRAY
14 C     "ARRAY" FOR THE ARRAY INDICES (I,J) WHERE
15 C
16 C         "IMIN" .LE. I .LE. "IMAX"
17 C         "JMIN" .LE. J .LE. "JMAX"
18 C
19 C     MAKE SURE "IMIN", "IMAX", "JMIN", AND "JMAX" ARE WITHIN THE PROPER RANGE.
20 C
21     IMINARA=MIN(IMIN,IMAX)
22     IMAXARA=MAX(IMIN,IMAX)
23     JMINARA=MIN(JMIN,JMAX)
24     JMAXARA=MAX(JMIN,JMAX)
25     IMINARA=MIN(MAX(1,IMINARA),NX)
26     IMAXARA=MIN(MAX(1,IMAXARA),NX)
27     JMINARA=MIN(MAX(1,JMINARA),NY)
28     JMAXARA=MIN(MAX(1,JMAXARA),NY)
29 C
30 C     FIND MAX AND MIN WITHIN INDICATED REGION OF I AND J.
31 C
32     AMAX=ARRAY(IMINARA,JMINARA)
33     AMIN=ARRAY(IMINARA,JMINARA)
34     DO 1 J=JMINARA,JMAXARA,1
35         DO 1 I=IMINARA,IMAXARA,1
36             IF(ARRAY(I,J) .GT. AMAX)AMAX=ARRAY(I,J)
37             IF(ARRAY(I,J) .LT. AMIN)AMIN=ARRAY(I,J)
38 1 CONTINUE
39     RETURN
40     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling NONBLNK'
4 $SUBTITLE: '    FUNCTION NONBLNK'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION NONBLNK(CSTRING,ISTART,ISTOP)
8 C
9 C     LAST MODIFIED 11/18/87. BY R. WILSON.
10 C
11     INTEGER DELTA,NONBLNK
12     CHARACTER CSTRING*(*)
13 C
14 C     "NONBLNK" determines the first non-blank character in the character string
15 C     "CSTRING" if "ISTART" is .LT. "ISTOP". It determines the last non-blank
16 C     character in the string if "ISTART" is .GT. "ISTOP". If no non-blank
17 C     characters are found "NONBLNK" is set to 0.
18 C
19     DELTA=SIGN(1,(ISTOP-ISTART))
20     DO 1 I=ISTART,ISTOP,DELTA
21         NONBLNK=I
22         IF(CSTRING(I:I) .NE. ' ')RETURN
23     1 CONTINUE
24     NONBLNK=0
25     RETURN
26     END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling NUMCHAR'
4 $SUBTITLE: '    SUBROUTINE NUMCHAR'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE NUMCHAR(XNUM,NDECR,OFFSET,CNUM,NCHAR)
8 C
9 C LAST MODIFIED 10/08/87. BY R. WILSON.
10 C ***** 3/15/88. BY R. WILSON.
11 C     1) Changed second argument name from "NRIGHT" to "NDECR". This
12 C        corrected an error which would occur when "NUMCHAR" is called
13 C        with a 'CONSTANT' second argument which is negative.
14 C ***** 12/05/88. BY R. WILSON.
15 C     1) Removed "CHARTYP" from argument list.
16 C ***** 2/05/90. BY R. WILSON.
17 C     1) Use ABS("OFFSET") to trap the possibility that the user may
18 C        inadvertently use an "OFFSET" < 0. Note: in MS Fortran 5.0
19 C        this does not cause a runtime error, however, the results are
20 C        incorrect. Also, a runtime error is generated on CYBER.
21 C
22 C "NUMCHAR" converts the real number "XNUM" to a character string stored
23 C in "CNUM".
24 C
25 C ABS("NDECR") denotes the desired number of digits to the right of the
26 C decimal point in the character version of the real number "XNUM". For
27 C "NDECR" .GE. 0 "CNUM" will be the character version of "XNUM" with "XNUM"
28 C having been rounded to "NDECR" digits to the right of the decimal place.
29 C Usually "NDECR" is .GE. 0. However, if "NDECR" is .LT. 0 then "NUMDECR"
30 C is called to determine the number of non-zero digits to be included right
31 C of the decimal point in "CNUM". The absolute value of this negative
32 C "NDECR" is used in the call to "NUMDECR" as the maximum allowed number of
33 C digits. Note: as indicated below calling "NUMCHAR" with a constant negative
34 C value (the argument in the call is a number or parameter not a variable)
35 C for NDECR" will not cause problems. "NDECR" is an input to "NUMCHAR".
36 C
37 C "OFFSET" is the starting character position in "CNUM" to be used for the
38 C string representing the real number "XNUM". Usually "OFFSET"=0 but in some
39 C cases "OFFSET" > 0; in which case the characters "CNUM(1:OFFSET)" are not
40 C destroyed. "OFFSET" is an input to "NUMCHAR".
41 C
42 C "NCHAR" is the number of characters stored in "CNUM" upon return from
43 C "NUMCHAR". This value includes the "OFFSET" value input to "NUMCHAR". That
44 C is, "NCHAR" is the length of the string in "CNUM". NCHAR" is an output
45 C from "NUMCHAR".
46 C
47 C CHARACTER CNUM*(*),INTCHAR*18,CFORMAT*80
48 C INTEGER FSTCHAR,OFFSET,LCNUM
49 C
50 C "INTRND(X,XDEL)" is a statement function insuring that the INT function is
51 C performed on X rounded to account for any round off error.
52 C
53 C     INTRND(X,XDEL)=INT(X+SIGN(XDEL,X))
54 C
55 C Find length of "CNUM". Make sure "OFFSET" is non-negative.
56 C
57 C     LCNUM=LEN(CNUM)
58 C     IOFFSET=ABS(OFFSET)
59 C
60 C Find the number of character in "XNUM". Note: "NRIGHT" is set equal to
61 C the dummy argument "NDECR". Then "NRIGHT" is used in the remainder of
62 C "NUMCHAR" to avoid the problem of changing the input "NDECR" when "NUMCHAR"
63 C is called with a constant value for "NDECR" which is negative.
64 C
65 C     NRIGHT=NDECR
66 C     IF(ABS(XNUM) .GT. 1.0)THEN
67 C         NCHAR=INTRND(ALOG10(ABS(XNUM)),2.0E-5)+1
68 C     ELSE
69 C         NCHAR=1

```

```
70      ENDIF
71      IF(XNUM .LT. 0.0)NCHAR=NCHAR+1
72      IF(NRIGHT .LT. 0)NRIGHT=NUMDECR(XNUM,ABS(NRIGHT))
73      NCHAR=NCHAR+NRIGHT+1
74 C
75 C   Initialize "CFORMAT".
76 C
77      CFORMAT='(F'
78 C
79 C   Convert "NLEFT" and "NRIGHT" to character, load into "CFORMAT"
80 C
81      WRITE(INTCHAR,FMT='(I18)')NCHAR
82      FSTCHAR=NONBLNK(INTCHAR,1,18)
83      LENGTH=18-FSTCHAR
84      CFORMAT(3:LENGTH+3)=INTCHAR(FSTCHAR:18)
85      IDOT=LENGTH+4
86      CFORMAT(IDOT:IDOT)='.'
87      WRITE(INTCHAR,FMT='(I18)')NRIGHT
88      FSTCHAR=NONBLNK(INTCHAR,1,18)
89      LENGTH=18-FSTCHAR
90      CFORMAT(IDOT+1:IDOT+LENGTH+1)=INTCHAR(FSTCHAR:18)
91      CFORMAT(IDOT+LENGTH+2:)=')'
92 C
93 C   Using format string in "CFORMAT" write "XNUM" to "CNUM("OFFSET"+2:)".
94 C
95      WRITE(CNUM(IOFFSET+1:),CFORMAT(1:IDOT+LENGTH+2))XNUM
96 C
97 C   Adjust the string so that a leading "0" is included for "XNUM" < 1.0.
98 C
99      IDOT=INDEX(CNUM(IOFFSET+1:),'.')+IOFFSET
100     IF(CNUM(IDOT-2:IDOT) .EQ. ' -.')THEN
101         CNUM(IDOT-2:IDOT-1)='-0'
102     ELSEIF(CNUM(IDOT-1:IDOT) .EQ. ' .')THEN
103         CNUM(IDOT-1:IDOT-1)='0'
104     ENDIF
105     CALL REMOVE(CNUM(IOFFSET+1:),NCHAR)
106     NCHAR=NCHAR+IOFFSET
107 C
108 C   If "NRIGHT" is 0 ("XNUM" is a whole number) don't include the decimal
109 C   point in the string.
110 C
111     IF(NRIGHT .EQ. 0)THEN
112         IDOT=INDEX(CNUM(IOFFSET+1:),'.')+IOFFSET
113         CNUM(IDOT:)= ' '
114         NCHAR=IDOT-1
115     ENDIF
116     RETURN
117     END
```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling NUMDECR'
4 $SUBTITLE: '    FUNCTION NUMDECR'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION NUMDECR(X,MAXDECR)
8 C
9 C     LAST MODIFIED 3/26/87. BY R. WILSON.
10 C     ***** 2/05/90. BY R. WILSON.
11 C         1) Return if fractional part of "X" is zero instead of returning if
12 C            "X" is zero.
13 C         2) If the fractional part of "X" is zero, return with "NUMDECR"=0.
14 C
15     INTEGER NUMDECR,MAXDECR
16     CHARACTER CHARX*21,FORMAT*8
17 C
18 C     "NUMDECR" determines the number of digits, including leading zeroes,
19 C     to the right of the decimal point in the number "X". This is performed
20 C     on "X" rounded to "MAXDECR" significant digits to the right of the
21 C     decimal point.
22 C
23     NUMDECR=0
24     XFRACT=X-INT(X)
25     IF(XFRACT .NE. 0.0)THEN
26 C
27 C         If the fractional part of "X" is non-zero write this fractional part
28 C         into a character variable. When the "XFRACT" is written into "CHARX"
29 C         the result will contain "MAXDECR" significant figures. If the
30 C         fractional part were not used below (i.e. replace XFRACT with X) then
31 C         for "X" .gt. 1.0 only (MAXDECR-NLEFT) digits would be reported as
32 C         existing. For use with plot routines this would generally not be a
33 C         problem, but the definition of "MAXDECR" would not be implemented.
34 C
35         NSIGFIG=MIN(MAXDECR,14)
36         FORMAT='(E21.)'
37         WRITE(FORMAT(6:),'(I2,')')NSIGFIG
38         WRITE(CHARX,FORMAT)XFRACT
39         READ(CHARX(19:21),'(I3)')NUMDECR
40         ICHAR1=18-NSIGFIG
41 C
42 C         Since only the fractional part is being used the exponent "NUMDECR" is
43 C         usually .LE. 0. However, the INT function may cause rounding (for
44 C         example if X=.999999999999) so the next "IF" statement is used to insure
45 C         that the character variable is "SCANNED" correctly.
46 C
47         IF(NUMDECR .GE. 0)ICAR1=ICAR1+NUMDECR
48         NUMDECR=NSIGFIG-NUMDECR
49         DO 1 I=17,ICAR1,-1
50             IF(CHARX(I:I) .NE. '0')GO TO 2
51             NUMDECR=NUMDECR-1
52     1 CONTINUE
53     2 CONTINUE
54     ENDIF
55     RETURN
56     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling OPNFILE'
4 $SUBTITLE: '    SUBROUTINE OPNFILE'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE OPNFILE(IUNIT,IOTYPE,FNAME,NAMLGTH,PROMPT,WHICHARG)
8 C
9 C     LAST MODIFIED 5/26/89. BY R. WILSON.
10 C     ***** 7/26/89. BY R. WILSON.
11 C         1) Modified to use new MS Fortran 5.0 routines NARGS, and GETARG
12 C            which return command line argument.
13 C         2) Added "WHICHARG" to the argument list.
14 C     ***** 9/06/89. BY R. WILSON.
15 C         1) Renamed parameter "MODE" to "IOTYPE".
16 C         2) Acceptable parameters for "IOTYPE" are now INPUT, OUTPUT, and
17 C            APPEND.
18 C         3) If IOTYPE is APPEND the file is opened in APPEND mode, i.e. at
19 C            the end of information ready for writing.
20 C     ***** 11/15/89. BY R. WILSON.
21 C         1) Re-worded the messages produced by format statements 101 and 102.
22 C
23 C     "OPNFILE" Opens a file for INPUT, OUTPUT, or APPEND.
24 C
25 C     "IUNIT" is the unit number to open the file on. It is an INPUT to
26 C     "OPNFILE".
27 C
28 C     "IOTYPE" is a character variable containing the mode to open the file in.
29 C     It can have the values 'INPUT', 'OUTPUT', or 'APPEND'. A check is made for
30 C     the existence of the file. If the file is to be opened for INPUT and it
31 C     does not exist an informative message is displayed and the user is asked
32 C     for a new file name. If the file is to be opened for OUTPUT and it does
33 C     exist the user is asked if it is okay to overwrite. If the file is opened
34 C     for APPEND and it does not exist an informative message is displayed and
35 C     the user is asked for a new file name. If "IOTYPE" is not 'INPUT',
36 C     'OUTPUT', or 'APPEND', no checks are made for existence of the file and the
37 C     old file contents, if any, will be destroyed by any write operation.
38 C
39 C     "FNAME" is the name of the file to be and which is eventually opened.
40 C     If "FNAME" is blank then, if "WHICHARG" is .GT. 0, the "WHICHARG" argument
41 C     on the command line is checked for a file. If a file name is not found
42 C     there then the user is prompted for a file name. "FNAME" is an INPUT to
43 C     and an OUTPUT from "OPNFILE".
44 C
45 C     "NAMLGTH" is the number of characters in "FNAME". it is an OUTPUT from
46 C     "OPNFILE".
47 C
48 C     "PROMPT" is a character string to be used in the prompt for the file name
49 C     when "FNAME" is blank, no file is specified in the command tail, or "FNAME"
50 C     (obtained from the keyboard or the command tail) already exists. "PROMPT"
51 C     is an INPUT to "OPNFILE".
52 C
53 C     "WHICHARG" is the number of the command line argument to check for a file
54 C     name if "FNAME" is blank. If "WHICHARG" is .LE. 0 or there are fewer than
55 C     "WHICHARG" arguments on the command line (in addition to the executable
56 C     file name which is argument number 0) the user is prompted for a file name.
57 C     "WHICHARG" is an INPUT to "OPNFILE".
58 C
59 C
60 C     CHARACTER FNAME*(*),PROMPT*(*),IOTYPE*6,IOTYPE1*6
61 C     INTEGER IUNIT,NAMLGTH,MXNLGTH,NUMARGS,PLGTH,WHICHARG
62 C     INTEGER*4 NARGS
63 C     LOGICAL FEXIST,ISDOS,YESNOTF,DOSNAME
64 C     EXTERNAL YESNOTF,DOSNAME
65 C
66 C     Check for a blank file name. Get length of "PROMPT".
67 C
68 C     MXNLGTH=LEN(FNAME)
69 C     NAMLGTH=NONBLNK(FNAME,MXNLGTH,1)
```

```

70      PLGTH=NONBLNK(PROMPT,LEN(PROMPT),1)
71 C
72 C   If the name is blank look in the command tail for the name.
73 C
74      IF(NAMLGTH .EQ. 0)THEN
75          NUMARGS=INT2(NARGS())-1
76          IF(WHICHARG .GT. 0 .AND. WHICHARG .LE. NUMARGS)THEN
77              CALL GETARG(WHICHARG,FNAME,NAMLGTH)
78          ELSE
79              WRITE(*,100)PROMPT(1:PLGTH)
80 100      FORMAT(/1X,A,' \')
81          READ(*,'(A)')FNAME
82          NAMLGTH=NONBLNK(FNAME,MXNLGTH,1)
83      ENDIF
84  ENDIF
85 C
86 C   Check for existence of the file if "IOTYPE" is 'INPUT', 'OUTPUT' or
87 C   'APPEND'.
88 C
89      IOTYPE1=IOTYPE
90      CALL UPPER(IOTYPE1,6)
91 1 CONTINUE
92      ISDOS=DosName(FNAME)
93      CALL UPPER(FNAME,NAMLGTH)
94      INQUIRE(FILE=FNAME,EXIST=FEXIST)
95      IF(IOTYPE1(1:6) .EQ. 'OUTPUT')THEN
96 C
97 C   Check if the file name is a DOS reserved name, and check for file
98 C   existence.
99 C
100      FEXIST=FEXIST .AND. .NOT.(ISDOS)
101 C
102 C   Want to only write to file. If it already exists ask if okay to
103 C   overwrite.
104 C
105      IF(FEXIST)THEN
106          CALL BEEP
107          WRITE(*,101)FNAME(1:NAMLGTH)
108 101      FORMAT(/1X,'***** WARNING - You requested output to be',
109 $          1X,'WRITTEN to the file: '//7X,A//
110 $          1X,'which already exists.'/)
111          IF( .NOT. (YESNOTF('Is it okay to overwrite'))))THEN
112              WRITE(*,100)PROMPT(1:PLGTH)
113              READ(*,'(A)')FNAME
114              NAMLGTH=NONBLNK(FNAME,MXNLGTH,1)
115              GO TO 1
116          ENDIF
117      ENDIF
118
119      ELSEIF(IOTYPE1(1:5) .EQ. 'INPUT')THEN
120 C
121 C   Want to only read from file. If it does not exist ask for name again.
122 C
123      FEXIST=FEXIST .OR. ISDOS
124      IF(.NOT. (FEXIST))THEN
125          CALL BEEP
126          WRITE(*,102)FNAME(1:NAMLGTH)
127 102      FORMAT(/1X,'***** ERROR - You requested input to be',
128 $          1X,'READ from the file: '//7X,A//
129 $          1X,'which does not exist. Try again.')
130          WRITE(*,100)PROMPT(1:PLGTH)
131          READ(*,'(A)')FNAME
132          NAMLGTH=NONBLNK(FNAME,MXNLGTH,1)
133          GO TO 1
134      ENDIF
135  ENDIF
136 C
137 C   OPEN THE FILE.
138 C

```

```
139      IF(IOTYPE1(1:6) .EQ. 'APPEND')THEN
140          OPEN(IUNIT,FILE=FNAME,ACCESS='APPEND')
141      ELSE
142          OPEN(IUNIT,FILE=FNAME)
143      ENDIF
144  C
145      RETURN
146  END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling PLTT'
4 $SUBTITLE: '    SUBROUTINE PLTT'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE PLTT(X,Y,IPEN)
8 C
9 C     LAST MODIFIED 6/13/85.
10 C
11 C     PLTT ELIMINATES MOVING PEN FOR HIDDEN LINES.
12 C
13     XLAST=XN
14     YLAST=YN
15     ILAST=IN
16     XN=X
17     YN=Y
18     IN=IPEN
19     IF(IPEN .EQ. 2)THEN
20         IF(ILAST .EQ. 2)THEN
21             CALL PLOT(X,Y,IPEN)
22         ELSEIF(ILAST .EQ. 3)THEN
23             CALL PLOT(XLAST,YLAST,ILAST)
24             CALL PLOT(X,Y,IPEN)
25         ENDIF
26     ELSEIF(IPEN .LT. 0)THEN
27         CALL PLOT(X,Y,IPEN)
28     ENDIF
29     RETURN
30     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling READERR'
4 $SUBTITLE: '    SUBROUTINE READERR'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE READERR
8 C
9 C   LAST MODIFIED 8/3/89.  BY R. WILSON.
10 C
11 C   "READERR" writes an message to the screen indicating IMPROPER input and
12 C   instructing the user to try again.
13 C
14     CALL BEEP
15     WRITE(*,100)
16 100 FORMAT(1X,'***** ERROR - Improper input.  Try again!'/)
17     RETURN
18     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling REC2POL'
4 $SUBTITLE: '    FUNCTION REC2POL'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION REC2POL(CRECT,DB)
8 C
9 C  LAST MODIFIED 11/13/87. BY R. WILSON
10 C  ***** 6/21/88. BY R. WILSON
11 C      1) Changed to a function and added to "PLTLIB"
12 C
13     PARAMETER(PI=3.1415926535898,RAD2DEG=180.0/PI,ZERO=1.0E-12)
14     COMPLEX CRECT,REC2POL
15     LOGICAL DB
16 C
17 C  "REC2POL" computes the magnitude and phase of the complex number "CRECT"
18 C  and stores the magnitude in the real part of "REC2POL" and the phase in
19 C  the imaginary part of "REC2POL". If "DB" is TRUE then the dB amplitude
20 C  will be stored. The pahse will be in degrees.
21 C
22     AMP=CABS(CRECT)
23     IF(AMP .LE. ZERO)THEN
24         PHASE=0.0
25     ELSE
26         PHASE=ATAN2(AIMAG(CRECT),REAL(CRECT))*RAD2DEG
27     ENDIF
28     IF(DB)THEN
29         AMP=20.0*ALOG10(MAX(AMP,ZERO))
30     ENDIF
31     REC2POL=CMPLX(AMP,PHASE)
32     RETURN
33     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling REMOVE'
4 $SUBTITLE: '    SUBROUTINE REMOVE'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE REMOVE(CSTRING,NCHAR)
8 C
9 C     LAST MODIFIED  9/19/85.  BY R. WILSON.
10 C     ***** 6/28/88.  BY R. WILSON.
11 C         1) Corrected error which occurs when attempt is made to add
12 C            colon on end of "CSTRING" when colon position would be passed
13 C            end of "CSTRING".
14 C     ***** 12/05/88.  BY R. WILSON.
15 C         1) Modified to run using PLOT88 which doesn't stop plotting when
16 C            a colon is encountered in the string.  So don't want to add the
17 C            the colon.
18 C     ***** 7/18/89.  BY R. WILSON.
19 C         1) Corrected error in logic which left the tail of "CSTRING" in the
20 C            new, "leading-blank-removed" "CSTRING".
21 C         2) This only shows up if you call "REMOVE" again with the same
22 C            "CSTRING" multiple times (as is now done in "AXIS3D").
23 C         3) This error may not show up with some compilers.  I don't recall
24 C            seeing this error up with the Microsoft compiler for example.
25 C
26 C     "REMOVE" removes leading blanks from the character string "CSTRING".  The
27 C     number of characters in the string "CSTRING" is returned as "NCHAR".
28 C
29 C     INTEGER FSTCHAR,LSTCHAR,LSTRING
30 C     CHARACTER*(*) CSTRING
31 C
32 C     FIND LENGTH OF "CSTRING".
33 C
34 C     LSTRING=LEN(CSTRING)
35 C
36 C     REMOVE LEADING BLANK SPACES.
37 C
38 C     NCHAR=0
39 C     FSTCHAR=NONBLNK(CSTRING,1,LSTRING)
40 C     IF(FSTCHAR.NE. 0)THEN
41 C         LSTCHAR=NONBLNK(CSTRING,LSTRING,FSTCHAR)
42 C         NCHAR=LSTCHAR-FSTCHAR+1
43 C         IF(FSTCHAR.NE. 1)THEN
44 C             CSTRING(1:)=CSTRING(FSTCHAR:LSTCHAR)
45 C         ENDIF
46 C     ENDIF
47 C     RETURN
48 C     END
```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SCALE1'
4 $SUBTITLE: '    SUBROUTINE SCALE1'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SCALE1(XMAX,XMIN,CONTAIN,NTICSM1,XMAXP,XMINP,DELTAX)
8 C
9 C     LAST MODIFIED 3/27/86. BY R. WILSON
10 C
11 C     GIVEN "XMAX", "XMIN"(.NE. "XMAX"), AND "NTICSM1" SCALE1 FINDS A NEW RANGE
12 C     RANGE ("XMAXP", "XMINP") DIVISIBLE INTO APPROXIMATELY "NTICSM1" LINEAR
13 C     INTERVALS OF SIZE DELTAX. IF "CONTAIN" IS TRUE THEN THE INTERVAL
14 C     ("XMIN","XMAX") WILL BE CONTAINED IN ("XMINP","XMAXP"). THIS IS
15 C     THE SITUATION NORMALLY USED IN LINEARLY SCALING AN AXIS FOR PLOTTING
16 C     (LMAXIS). IF "CONTAIN" IS FALSE THEN ("XMINP","XMAXP") WILL BE
17 C     CONTAINED IN ("XMIN","XMAX"). THIS WOULD BE THE SITUATION NORMALLY
18 C     USED IN SCALING THE CONTOUR VALUES IN CONTOUR PLOTS (CONTR).
19 C
20 C     IF "DELTAX"=0 ON INPUT THEN AN ADJUSTED "DELTAX" IS FOUND AND USED IN
21 C     FINDING "XMAXP" AND "XMINP". OTHERWISE THE "DELTAX" VALUE PASSED ON INPUT
22 C     IS USED IN FINDING "XMAXP" AND "XMINP".
23 C
24 C     "VINT" IS AN ARRAY OF ACCEPTABLE VALUES FOR "DELTAX" (TIMES AN INTEGER
25 C     POWER OF 10.0).
26 C
27 C     "SQR" IS AN ARRAY OF GEOMETRIC MEANS OF ADJACENT VALUES OF "VINT", USED AS
28 C     BREAK POINTS TO DETERMINE WHICH "VINT" VALUE TO ASSIGN TO "DELTAX."
29 C
30     REAL VINT(4),SQR(3)
31     LOGICAL CONTAIN,ORDERED
32     DATA VINT/1.,2.,5.,10./
33     DATA SQR/1.414214,3.162278,7.071068/
34 C
35 C     "DEL" ACCOUNTS FOR COMPUTER ROUND-OFF. IT SHOULD BE GREATER THAN THE
36 C     ROUND-OFF EXPECTED FROM A DIVISION AND FLOAT OPERATION. IT SHOULD BE
37 C     LESS THAN THE MINIMUM INCREMENT OF THE PLOTTING DEVICE USED BY THE MAIN
38 C     PROGRAM IN INCHES DIVIDED BY THE PLOT SIZE IN INCHES TIMES THE NUMBER
39 C     OF INTERVALS.
40 C
41     DEL=0.00002
42 C
43 C     IF "DELTAX" PASSED TO "SCALE1" IS 0.0 FIND A NEW ADJUSTED VALUE FOR
44 C     "DELTAX", OTHERWISE USE THE "DELTAX" VALUE PASSED TO "SCALE1" IN
45 C     DETERMINING THE ADJUSTED "XMAX" AND "XMIN".
46 C
47     IF(DELTAX .EQ. 0)THEN
48 C
49 C         FIND APPROXIMATE INTERVAL SIZE.
50 C
51         DELTAX=ABS(XMAX-XMIN)/NTICSM1
52         NDIGL=INT(ALOG10(DELTAX))
53         IF(DELTAX .LT. 1.)NDIGL=NDIGL-1
54 C
55 C         SCALE "DELTAX" INTO A NUMBER BETWEEN 1 AND 10.
56 C
57         SDELTAX=DELTAX/10.0**NDIGL
58 C
59 C         USE "SDELTAX" TO FIND CLOSEST "VINT" VALUE.
60 C
61         DO 1 I=1,3,1
62             IF(SDELTAX .LT. SQR(I))GO TO 2
63     1      CONTINUE
64         I=4
65 C
66 C         COMPUTE ACTUAL "DELTAX".
67 C
68     2      CONTINUE
69         DELTAX=VINT(I)*10.0**NDIGL
```

```
70      ENDIF
71 C
72 C   FIND NEW" XMAX" AND "XMIN".
73 C
74      ORDERED=(XMAX .GT. XMIN)
75      IF(CONTAIN .EQV. ORDERED)THEN
76          FM1=XMIN/DELTAX
77          FM2=XMAX/DELTAX
78      ELSE
79          FM1=XMAX/DELTAX
80          FM2=XMIN/DELTAX
81      ENDIF
82      M1=INT(FM1)
83      IF(FM1 .LT. 0.0)M1=M1-1
84      IF(ABS(FLOAT(M1)+1.0-FM1) .LT. DEL)M1=M1+1
85      M2=INT(FM2+1.)
86      IF(FM2 .LT. -1.)M2=M2-1
87      IF(ABS(FM2+1.0-FLOAT(M2)) .LT. DEL)M2=M2-1
88      IF(CONTAIN .EQV. ORDERED)THEN
89          XMINP=DELTAX*FLOAT(M1)
90          XMAXP=DELTAX*FLOAT(M2)
91      ELSE
92          XMINP=DELTAX*FLOAT(M2)
93          XMAXP=DELTAX*FLOAT(M1)
94      ENDIF
95      IF(CONTAIN)THEN
96 C
97 C   ADJUST LIMITS IF NECESSARY TO ACCOUNT FOR ROUNDOFF.
98 C
99      IF(ORDERED)THEN
100         IF((XMINP-XMIN) .GT. DEL)XMINP=XMIN
101         IF((XMAX-XMAXP) .GT. DEL)XMAXP=XMAX
102     ELSE
103         IF((XMIN-XMINP) .GT. DEL)XMINP=XMIN
104         IF((XMAXP-XMAX) .GT. DEL)XMAXP=XMAX
105     ENDIF
106 ENDIF
107 RETURN
108 END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SIND'
4 $SUBTITLE: '    FUNCTION SIND'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION SIND(ANGLE)
8 C
9 C  LAST MODIFIED 12/01/88.  BY. R. WILSON.
10 C
11 C  "SIND" COMPUTES THE SINE OF THE ANGLE "ANGLE" WHERE "ANGLE" IS IN
12 C  DEGREES.
13 C
14     PARAMETER(PI=3.1415926535898,DEG2RAD=PI/180.0)
15     SIND=SIN(ANGLE*DEG2RAD)
16     RETURN
17     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SLENRW'
4 $SUBTITLE: '    SUBROUTINE SLENRW'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SLENRW(WIDTH,HEIGHT,TEXT,N)
8 C
9 C     LAST MODIFIED 5/13/85. BY R. WILSON.
10 C     ***** 12/01/88. BY R. WILSON.
11 C         1) Modified to work with the PLOT88 library
12 C         2) To this end changed from calling SLEN to GETWID
13 C         3) In the future might want to remove "SLENRW" and change
14 C           any calls to it in the plot library to calls to "GETWID"
15 C
16     CHARACTER*(*)TEXT
17 C
18 C     "WIDTH" is the returned length of the text in the character string
19 C     "TEXT". "HEIGHT" is the desired height of the text and "N" is the
20 C     number of characters in "TEXT" to be considered.
21 C
22     CALL GETWID(HEIGHT,TEXT,N,WIDTH)
23     RETURN
24     END
```

```

1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling SPLINE'
4 $SUBTITLE: '    SUBROUTINE SPLINE'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE SPLINE(X,Y,NX,XSPLINE,YSPLINE,NXSPMAX,NXSP,
8         $ NSPLINE,JGRAPH)
9 C
10 C  LAST MODIFIED  7/05/87.  BY R. WILSON.
11 C  *****      2/02/87.  BY R. WILSON.
12 C      1) MODIFIED ERROR MESSAGE SO IT PROVIDES MORE INFORMATION.
13 C  *****      6/29/89.  BY R. WILSON.
14 C      1) UPDATED THE ERROR MESSAGE FORMAT TO BE CONSISTENT WITH THOSE IN
15 C      OTHER LIBRARY ROUTINES.
16 C
17 C  "SPLINE" TAKES THE DATA IN THE ARRAYS "X" AND "Y" AND LOADS IT INTO
18 C  THE CORRESPONDING ARRAYS "XSPLINE" AND "YSPLINE".  IF "NSPLINE"=1 THEN
19 C  'LOCAL' SPLINE SMOOTHING IS PERFORMED.
20 C
21 C  DEFINITION OF PARAMETERS.
22 C
23 C  FOR THE DEFINITIONS OF "X", "Y", "NX", "XSPLINE", AND "YSPLINE" SEE THE
24 C  LISTING FOR "INTRPL".
25 C
26 C  "NXSPMAX" IS THE MAXIMUM NUMBER OF POINTS AT WHICH SMOOTHING IS DESIRED.
27 C  IT IS ALSO THE DIMENSION OF THE ARRAYS "XSPLINE" AND "YSPLINE".
28 C
29 C  "NXSP" IS SET EQUAL TO "NXSPMAX" IF SMOOTHING IS DESIRED. IT IS SET EQUAL
30 C  TO "NX" IF SMOOTHING IS NOT DESIRED.
31 C
32 C  "NSPLINE" CONTROLS THE TYPE OF SMOOTHING PERFORMED AS FOLLOWS:
33 C      NSPLINE=0    NO SMOOTHING IS PERFORMED
34 C      =1    'LOCAL' SPLINE SMOOTHING IS PERFORMED
35 C
36 C  "JGRAPH" DETERMINES WHETHER THE ABSCISSA VALUES STORED IN "XSPLINE" ARE
37 C  RESET.  IF "JGRAPH" .EQ. 1 THEN THEY ARE RESET, IF NOT THEN SMOOTHING IS
38 C  PERFORMED AT THE OLD ABSCISSA VALUES.
39 C
40     REAL X(NX),Y(NX),XSPLINE(NXSPMAX),YSPLINE(NXSPMAX)
41     IF(NX .GT. NXSPMAX)THEN
42         WRITE(*,100)NX,NXSPMAX
43 100    FORMAT(1X,'***** ERROR- program terminated in SPLINE.'/
44         $      7X,'Dimension of arrays X and Y (NX=',15,') exceeds',
45         $      1X,'dimension of arrays',7X,'XSPLINE and YSPLINE',
46         $      1X,'(NXSPMAX=',15,').')
47     STOP
48     ENDIF
49     IF(NSPLINE .GT. 0)THEN
50         IF(JGRAPH .EQ. 1)THEN
51 C
52 C      CALCULATE ABSCISSA VALUES AT WHICH SPLINE APPROXIMATIONS
53 C      ARE DESIRED AND STORE IN XSPLINE.
54 C
55         NXSP=NXSPMAX
56         UFAC=(X(NX)-X(1))/(NXSPMAX-1.0)
57         DO 2 I=1,NXSP,1
58             XSPLINE(I)=(I-1)*UFAC+X(1)
59     2    CONTINUE
60     ENDIF
61 C
62 C      CALCULATE VALUES OF 'LOCAL' SPLINE APPROXIMATION AT THE XSPLINE(I).
63 C      STORE IN YSPLINE.
64 C
65     CALL INTRPL(X,Y,NX,XSPLINE,YSPLINE,NXSPMAX)
66     ELSE
67 C
68 C      NO SPLINE APPROXIMATION DESIRED.
69 C

```

```
70      NXSP=NX
71      DO 3 I=1,NXSP,1
72          XSPLINE(I)=X(I)
73          YSPLINE(I)=Y(I)
74      3    CONTINUE
75      ENDIF
76      RETURN
77      END
```

```
1 $MESSAGE:'Compiling TIME'
2 $SUBTITLE: '  Function TIME'
3 $PAGE
4 $NOTRUNCATE
5     FUNCTION TIME()
6 C
7 C   LAST MODIFIED  8/28/88.  BY R. WILSON.
8 C   *****      5/25/89.  BY R. WILSON.
9 C       1) ADDED CODE TO FORMAT THE SECONDS PART OF THE TIME STRING AS
10 C         '01', '02', ETC., FOR SECONDS .LE. 9.
11 C
12 C   "TIME" RETURNS THE CURRENT TIME (AS REPORTED BY THE SYSTEM CLOCK).  MS
13 C   FORTRAN HAS A LIBRARY ROUTINE CALLED "GETTIM" WHICH IS CALLED BY "TIME".
14 C   THE RETURNED INTEGER*2 VALUES ARE PACKED INTO A CHARACTER VARIABLE IN CDC
15 C   CYBER NOS/VE FORMAT AND RETURNED AS "TIME".
16 C
17 C       INTEGER*2 IHR,IMIN,ISEC,I100TH
18 C       CHARACTER TIME*8
19 C
20 C   GET THE CURRENT TIME FROM THE SYSTEM CLOCK.
21 C
22 C       CALL GETTIM(IHR,IMIN,ISEC,I100TH)
23 C
24 C   PACK TIME INTO CHARACTER VARIABLE "TIME" IN CDC NOS FORMAT.
25 C
26 C       WRITE(TIME,100)IHR,IMIN,ISEC
27 100 FORMAT(12,':',12,':',12)
28 C       IF(TIME(4:4) .EQ. ' ')THEN
29 C           TIME(4:4)='0'
30 C       ENDIF
31 C       IF(TIME(7:7) .EQ. ' ')THEN
32 C           TIME(7:7)='0'
33 C       ENDIF
34 C       RETURN
35 C       END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling TITLE'
4 $SUBTITLE: '    SUBROUTINE TITLE'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE TITLE(CTITLE,ANGLE,NSIGN,YLETTER,HEIGHT,XSIZE,XORIGIN)
8 C
9 C     LAST MODIFIED 6/01/86. BY R. WILSON.
10 C
11 C     "TITLE" PLOTS THE CHARACTER STRING "CTITLE" PARALLEL TO AN AXIS WHICH
12 C     STARTS AT "XORIGIN", IS OF LENGTH "XSIZE" AND IS AT AN ANGLE "ANGLE"
13 C     TO THE HORIZONTAL. THE CHARACTERS IN THE TITLE WILL BE PLOTTED WITH
14 C     HEIGHT "HEIGHT", AND THEIR BOTTOM EDGE WILL BE AT "YLETTER" BEFORE
15 C     ROTATION (TO THE ANGLE "ANGLE"). THE CHARACTERS WILL BE CENTERED
16 C     ALONG THE AXIS. ANY LEADING BLANKS IN THE STRING "CTITLE" WILL BE
17 C     REMOVED BEFORE CENTERING. IF "NSIGN"= +1 THE CHARACTERS WILL BE
18 C     PLOTTED PARALLEL TO THE AXIS. IF "NSIGN"= -1 THE CHARACTERS WILL BE
19 C     PLOTTED ANTI-PARALLEL TO THE AXIS.
20 C
21     REAL XORIGIN(2)
22     CHARACTER CTITLE*(*)
23 C
24 C     REMOVE LEADING BLANKS AND CENTER TITLE ALONG AXIS.
25 C
26     CALL REMOVE(CTITLE,NCHAR)
27     IF(NCHAR .GT. 0)THEN
28         CALL SLENRW(XTITLE,HEIGHT,CTITLE,NCHAR)
29         XLETTER=(XSIZE-NSIGN*XTITLE)/2.0
30         XPAGE=XLETTER*COSD(ANGLE)-YLETTER*SIND(ANGLE)+
31         $     XORIGIN(1)
32         YPAGE=XLETTER*SIND(ANGLE)+YLETTER*COSD(ANGLE)+
33         $     XORIGIN(2)
34         ANGTITL=ANGLE+((1-NSIGN)/2.0)*180.0
35         CALL SYMBOL(XPAGE,YPAGE,HEIGHT,CTITLE,ANGTITL,NCHAR)
36     ENDIF
37     RETURN
38     END
```



```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling TPLOT'
4 $SUBTITLE: '    SUBROUTINE TPLOT'
5 $PAGE
6 $NOTRUNCATE
7     SUBROUTINE TPLOT(XMAX,XMIN,TMAX,DELTAX)
8 C
9 C     LAST MODIFIED 10/13/85.  BY R. WILSON.
10 C
11 C     DETERMINE TYPE OF AXIS SCALING TO BE USED IN PLOTTING AXIS, LINEAR OR
12 C     LOGARITHMIC.
13 C
14 C     "DELTAX" IS AN INPUT-OUTPUT VARIABLE.  FOR "DELTAX" .LT. 0.0 THE USER IS
15 C     REQUESTING A LOGARITHMIC AXIS.  "TPLOT" CHECKS TO MAKE SURE THIS IS POSSIBLE
16 C     (I.E. THAT 0 WILL NOT APPEAR SOMEWHERE ON THE AXIS BETWEEN "XMAX" AND
17 C     "XMIN") AND IF A LOG AXIS IS POSSIBLE A NEGATIVE "DELTAX" VALUE WILL BE
18 C     RETURNED.  IF A LOGARITHMIC AXIS IS NOT POSSIBLE "DELTAX"=0.0 WILL BE
19 C     RETURNED SO THAT "AXISXY" WILL PLOT AN AUTO-SCALED LINEAR AXIS.  FOR
20 C     "DELTAX"=0.0 THE USER IS ASKING "TPLOT" TO DETERMINE THE TYPE OF AXIS
21 C     SCALING TO USE.  IF THE RATIO, "TLOG" (DISCUSSED BELOW) IS .LE. "TMAX" THEN
22 C     A "DELTAX"=0.0 IS RETURNED AND AN AUTO-SCALED LINEAR AXIS IS OBTAINED.  IF
23 C     "TLOG" IS .GT. "TMAX" A NEGATIVE "DELTAX" IS RETURNED AND A LOGARITHMIC
24 C     AXIS IS OBTAINED.  FOR "DELTAX" .GT. 0.0 THE USER IS ASKING FOR A LINEAR
25 C     PLOT AND "TPLOT" RETURNS THE POSITIVE "DELTAX" VALUE TO GIVE IT TO HIM.
26 C     IN THIS CASE "LINAXIS" WILL NOT AUTO-SCALE.
27 C
28 C     "TLOG" IS DEFINED THE WAY IT IS IN ORDER TO ALLOW THE POSSIBILITY (HOWEVER
29 C     REMOTE) THAT THE USER WANTS THE MAXIMUM VALUE ON THE AXIS LEFT OF (BELOW)
30 C     THE MINIMUM VALUE ON THE AXIS.
31 C
32     IF(DELTAX .LT. 0.0)THEN
33         IF((XMAX*XMIN) .LE. 0.0)DELTAX=0.0
34     ELSEIF(DELTAX .EQ. 0.0)THEN
35         ACTMIN=MIN(XMAX,XMIN)
36         IF(ACTMIN .EQ. 0.0)RETURN
37         ACTMAX=MAX(XMAX,XMIN)
38         TLOG=ACTMAX/ACTMIN
39         IF(TLOG.LE.0.0)RETURN
40         IF(TLOG.LE.TMAX)RETURN
41         DELTAX=-1.0
42     ENDIF
43     RETURN
44     END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling UPPER'
4 $SUBTITLE: ' SUBROUTINE UPPER'
5 $PAGE
6 $NOTRUNCATE
7 SUBROUTINE UPPER(CSTRING,NUM2UP)
8 C
9 C LAST MODIFIED 8/02/88. BY R. WILSON.
10 C ***** 1/13/89. BY R. WILSON.
11 C 1) CONVERSION FROM THE FIRST CHARACTER TO THE LAST NON-BLANK
12 C CHARACTER IN "CSTRING" IS NOW PERFORMED BOTH FOR "NUM2UP" <= 0 AND
13 C "NUM2UP" > "LSTCHAR".
14 C
15 C "UPPER" CONVERTS THE FIRST "NUM2UP" CHARACTERS IN THE STRING "CSTRING" TO
16 C UPPER CASE. IF "NUM2UP" <= 0 OR > "LSTCHAR" THEN THE ROUTINE WILL SCAN
17 C THROUGH THE STRING FROM THE FIRST CHARACTER TO THE LAST NON-BLANK
18 C CHARACTER CONVERTING TO UPPER CASE IF NECESSARY.
19 C
20 C INTEGER LSTCHAR,MXNCHAR
21 C CHARACTER*(*) CSTRING
22 C
23 C DETERMINE LENGTH OF "CSTRING".
24 C
25 C MXNCHAR=LEN(CSTRING)
26 C LSTCHAR=NONBLNK(CSTRING,MXNCHAR,1)
27 C
28 C IF "CSTRING" IS NOT ALL BLANKS SCAN THROUGH "CSTRING" REPLACING LOWER
29 C CASE CHARACTERS WITH THEIR UPPER CASE EQUIVALENTS. IF "CSTRING" IS JUST
30 C BLANK MAKE IT A SINGLE BLANK CHARACTER.
31 C
32 C IF(LSTCHAR.GT. 0)THEN
33 C IF(NUM2UP.LE.0 .OR. NUM2UP.GT.LSTCHAR)THEN
34 C NCHAR=LSTCHAR
35 C ELSE
36 C NCHAR=NUM2UP
37 C ENDIF
38 C DO 1 I=1,NCHAR,1
39 C ICOLSEQ=ICHAR(CSTRING(I:1))
40 C IF(ICOLSEQ.GE.97 .AND. ICOLSEQ.LE. 122)THEN
41 C CSTRING(I:1)=CHAR(ICOLSEQ-32)
42 C ENDIF
43 C 1 CONTINUE
44 C ELSE
45 C CSTRING=' '
46 C ENDIF
47 C RETURN
48 C END
```

```
1 $PAGESIZE:80
2 $LINESIZE:132
3 $MESSAGE:'Compiling YesNoTF'
4 $SUBTITLE: '    FUNCTION YesNoTF'
5 $PAGE
6 $NOTRUNCATE
7     FUNCTION YesNoTF(PROMPT)
8 C
9 C   LAST MODIFIED  3/20/89. BY R. WILSON.
10 C
11     CHARACTER PROMPT*(*),YESNO*1
12     LOGICAL YesNoTF
13 C
14 C   PROMPTS FOR A "Y"es OR "N"o ANSWER TO THE STANDARD OUTPUT DEVICE USING
15 C   THE PROMPT STRING "PROMPT" AND CONVERTS A "Y"es ANSWER TO .TRUE. AND
16 C   A "N"o ANSWER TO .FALSE..
17 C
18     1 CONTINUE
19     WRITE(*,100)PROMPT
20 100  FORMAT(1X,A,' (y or n)? '\)
21     READ(*,'(A1)')YESNO
22     CALL UPPER(YESNO,1)
23     IF(YESNO .EQ. 'N')THEN
24         YesNoTF=.FALSE.
25     ELSEIF(YESNO .EQ. 'Y')THEN
26         YesNoTF=.TRUE.
27     ELSE
28         GO TO 1
29     ENDIF
30     RETURN
31     END
```

```

1 C *****
2 C          ANTENNA LAYOUT PROGRAM
3 C *****
4 C MAIN PROGRAM AND LAYOUT-RELATED SUBROUTINES.
5 C NETWORK DESIGN AND INDUCTANCE/CAPACITANCE CALCULATIONS IN
6 C MODULE NETS.
7 C *****
8 C
9     REAL LANT,LAMBDA
10    DIMENSION XO(20,20),YO(20,20),EL1(20,20)
11    DIMENSION EL2(20,20),EL3(20,20),MTYPE(20,20)
12    DIMENSION XP(30),YP(30),XX(20,20),YY(20,20)
13    DIMENSION XH(400),YH(400),ZH(400),MH(400)
14    CHARACTER*1 FEEDLOC
15    LOGICAL RFLAG
16 C
17    COMMON /WINSIZ/WX1,WY1,WX2,WY2,FACT
18 C
19    DATA XMAX/10.5/,YMAX/7.3/
20    DATA WNORM/0.15/
21    DATA YCLR/-3E10/
22    DATA LTOP/1/,LBOT/2/,LBRD/3/
23    DATA PI/3.141596/
24    DATA FTHICK/0.0014/
25 C
26 C
27    OPEN(UNIT=11,FORM='FORMATTED',FILE=' ',STATUS='OLD')
28 C READ FREQUENCY IN GHz
29    READ(11,*)GFREQ
30    LAMBDA=3E10/(1E9*GFREQ*2.54)
31 C READ XSIZE AND YSIZE OF THE ANTENNA LAYOUT.
32    READ(11,*)XDIM,YDIM
33 C
34 C READ DIELECTRIC CONSTANT AND THICKNESS
35    READ(11,*)EPSR,THICK
36    THICK=THICK*1E3
37 C READ THE TIP-TO-TIP ANTENNA LENGTH, ANTENNA WIDTH AND ANTENNA TILT.
38    READ(11,*)LANT,WANT,TILT
39    IF(TILT.GE.0.)THEN
40        ANGLE=PI/2.-TILT*PI/180.
41    ELSE
42        ANGLE=-PI/2.-TILT*PI/180.
43    ENDIF
44 C WRITE(0,*)'TILT, ANGLE: ',TILT,ANGLE
45
46    IF(ABS(ANGLE).GE.1E-6)THEN
47        IROT=1
48    ELSE
49        IROT=0
50    ENDIF
51 C
52 C READ FEED NETWORK LOCATION.
53    READ(11,100)FEEDLOC
54    IF(FEEDLOC.EQ.'B')THEN
55        ITOP=0
56        ISWAP=0
57        ILOC=1
58    ELSE IF(FEEDLOC.EQ.'T')THEN
59        ITOP=1
60        ISWAP=0
61        ILOC=2
62    ELSE IF(FEEDLOC.EQ.'L')THEN
63        ITOP=0
64        ISWAP=1
65        ILOC=1
66    ELSE IF(FEEDLOC.EQ.'R')THEN
67        ITOP=1
68        ISWAP=1
69        ILOC=2

```

```
70      ELSE
71          ITOP=0
72          ISWAP=0
73          ILOC=1
74      ENDIF
75  C
76  C
77  100 FORMAT(A1)
78  C READ THE NUMBER OF COLUMNS AND ROWS IN THE ARRAY.
79      READ(11,*)NCOL,NROW
80  C
81      IF(NCOL.GT.20.OR.NROW.GT.20)THEN
82          WRITE(0,*)'Storage limits antenna to 20 rows or columns.'
83          STOP
84      ENDIF
85  C
86  C READ DATA IN ONE ROW AT A TIME
87  C
88      DO 1 M=1,NROW
89      DO 1 N=1,NCOL
90          READ(11,*)XO(M,N),YO(M,N),CURR,PHASE,ZMAG,ZANGL
91      1 CONTINUE
92  C
93  C READ THE MATCHING NETWORK DATA
94  C
95      DO 2 M=1,NROW
96      DO 2 N=1,NCOL
97          READ(11,*)NC,NR,MTYPE(M,N),EL1(M,N),EL2(M,N),EL3(M,N)
98      2 CONTINUE
99  C
100     JJ=0
101     DO 10 N=1,NCOL
102     DO 10 M=1,NROW
103         JJ=JJ+1
104         MH(JJ)=MTYPE(M,N)
105         XH(JJ)=XO(M,N)
106         10 YH(JJ)=YO(M,N)
107     C 10 WRITE(0,*)XH(JJ),YH(JJ)
108     C
109         IF(ISWAP.EQ.1)THEN
110     C
111         NZZZ=NROW
112         NROW=NCOL
113         NCOL=NZZZ
114     C
115         JJ=0
116         DO 11 M=1,NROW
117         DO 11 N=1,NCOL
118             JJ=JJ+1
119             MTYPE(M,N)=MH(JJ)
120             XO(M,N)=YH(JJ)
121         11 YO(M,N)=XH(JJ)
122     C
123         NZZZ=NROW
124         NROW=NCOL
125         NCOL=NZZZ
126         JJ=0
127         DO 12 N=1,NCOL
128         DO 12 M=1,NROW
129             JJ=JJ+1
130             XH(JJ)=EL1(M,N)
131             YH(JJ)=EL2(M,N)
132         12 ZH(JJ)=EL3(M,N)
133     C 12 WRITE(0,*)XH(JJ),YH(JJ),ZH(JJ)
134     C
135         NZZZ=NROW
136         NROW=NCOL
137         NCOL=NZZZ
138         JJ=0
```

```
139      DO 13 M=1,NROW
140      DO 13 N=1,NCOL
141          JJ=JJ+1
142          EL1(M,N)=YH(JJ)
143          EL2(M,N)=XH(JJ)
144          EL3(M,N)=ZH(JJ)
145      13 WRITE(0,*)EL1(M,N),EL2(M,N),EL3(M,N)
146      C
147          XTEMP=XDIM
148          XDIM=YDIM
149          YDIM=XTEMP
150          ANGLE=-TILT*PI/180.
151      C
152      ENDIF
153      C
154      C READ THE DATA FOR THE ARRAY MATCHING NETWORK.
155      C READ(11,*)MT,ET1,ET2,ET3
156      C
157      IF(GFREQ.GE.1.0)THEN
158          WFEED=.0625
159      ELSE
160          WFEED=.125
161      ENDIF
162      C
163      LANT=LANT/2.
164      777 WRITE(0,500)
165      500 FORMAT(//1H,'Antenna Layout Program: Version 1/11/90'//1H ,
166      & 'Select Desired Procedure'/1H ,
167      & 5X,'1-Automatically Scale Plot to EGA Screen'/1H ,
168      & 5X,'2-Automatically Scale Plot to HP-7570 Plotter on COM1'/1H ,
169      & 5X,'3-Automatically Scale Plot to HP-7585 Plotter on COM2'/1H ,
170      & 5X,'4-Automatically Scale Plot to HP-LJet Plotter on LPT1'/1H ,
171      & 5X,'5-Plot With Scale = 1 to HP-7585 Plotter on COM2'/1H ,
172      & 5X,'6-Specify Plotter Port, Type, Scale, and Plot Window'//)
173      C
174      WRITE(0,501)
175      501 FORMAT(1H,'Enter Number to Indicate Choice: '\)
176      READ(0,*)ICHOICE
177      IF(ICHOICE.GT.6.OR.ICHOICE.LT.1)GO TO 777
178      C
179      IF(ICHOICE.EQ.1)THEN
180          IOPORT=97
181          MODEL=97
182          WX1=0.
183          WY1=0.
184          WX2=XDIM
185          WY2=YDIM
186          FACT=1.
187      ENDIF
188      C
189      IF(ICHOICE.EQ.2)THEN
190          IOPORT=9600
191          MODEL=20
192          WX1=0.
193          WY1=0.
194          WX2=XDIM
195          WY2=YDIM
196          FACT=AMIN1(XMAX/XDIM,YMAX/YDIM)
197      ENDIF
198      C
199      IF(ICHOICE.EQ.3)THEN
200          IOPORT=9650
201          MODEL=85
202          WX1=0.
203          WY1=0.
204          WX2=XDIM
205          WY2=YDIM
206          FACT=AMIN1(64./XDIM,34./YDIM)
207          IF(FACT.GT.1.)FACT=1.
```

```
208      ENDIF
209 C
210      IF(ICHOICE.EQ.4)THEN
211          IOPORT=0
212          MODEL=62
213          WX1=0.
214          WY1=0.
215          WX2=XDIM
216          WY2=YDIM
217          FACT=AMIN1(9.9/XDIM,7.9/YDIM)
218      ENDIF
219 C
220      IF(ICHOICE.EQ.5)THEN
221          IOPORT=9650
222          MODEL=85
223          WX1=0.
224          WY1=0.
225          WX2=XDIM
226          WY2=YDIM
227          FACT=1.
228      ENDIF
229 C
230      IF(ICHOICE.EQ.6)THEN
231          WRITE(0,222)
232          222 FORMAT(1H,'Enter IOPORT, MODEL, SCALE FACTOR: '\)
233          READ(0,*)IOPORT,MODEL,FACT
234          WRITE(0,223)
235          223 FORMAT(1H,'Enter WINDOW Values: '\)
236          READ(0,*)WX1,WY1,WX2,WY2
237      ENDIF
238 C
239 C
240 C IF ONLY ONE ROW PRESENT, SET DISTANCE FROM THE FEED POINT TO
241 C BE ONE-HALF WAVELENGTH.
242 C
243      IF(NROW.GT.1)THEN
244          YDIST=YO(2,1)-YO(1,1)
245      ELSE
246          YDIST=LAMBDA/2.
247      ENDIF
248 C
249 C SET UP THE PLOTTING
250      CALL PLOTS(0,IOPORT,MODEL)
251 C      WRITE(0,*)'WX1,WY1,WX2,WY2: ',WX1,WY1,WX2,WY2
252 C
253      BX1=WX1
254      BX2=WX2
255      BY1=WY1
256      BY2=WY2
257 C
258      CALL WINDOW(BX1,BY1,BX2,BY2)
259 C
260 C
261 C      WRITE(0,*)'Scale Factor: ',FACT
262      CALL FACTOR(FACT)
263 C
264 C      WRITE(0,*)'WX1,WY1,WX2,WY2: ',WX1,WY1,WX2,WY2
265 C
266      CALL PLOT(WX1,WY1,3)
267      CALL PLOT(WX1,WY2,2)
268      CALL PLOT(WX2,WY2,2)
269      CALL PLOT(WX2,WY1,2)
270      CALL PLOT(WX1,WY1,2)
271 C
272 C DRAW THE ANTENNAS AND FEED MATCHING NETWORKS
273 C SEND A MESSAGE TO THE OPERATOR
274      WRITE(0,300)
275      300 FORMAT(/1H,'Constructing Antennas and Feed Structure ....'//)
276 C
```

```

277      CALL FEEDPNT(NROW,NCOL,XO,YO,MTYPE,EL1,EL2,EL3,
278      &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
279      &  YCLR,LAMBDA,ILOC,M)
280  C
281  C      WRITE(0,*)'EXIT FEEDPNT; YCLR: ',YCLR
282  C
283  C  DRAW THE FEED LINE EXTENSIONS
284      CALL FEEDLIN(NROW,NCOL,XO,YO,WFEED,IROT,ANGLE,YCLR,
285      &  ITOP,YDIST)
286  C
287  C  IF MORE THAN ONE ROW, CONSTRUCT MEANDERED TRANSMISSION LINES BETWEEN
288  C  ANTENNAS.
289  C
290      IF(NROW.GT.1)THEN
291          CALL MEANDER(XP,YP,XP1,YP1,NPOINT,YCLR,YDIST,ANGLE,
292          &  WNORM,LAMBDA,EPSR,.FALSE.)
293  C
294          CALL PATH(XO,YO,NROW,NCOL,XP,YP,XP1,YP1,NPOINT,WFEED,LTOP)
295          CALL PATH(XO,YO,NROW,NCOL,XP,YP,XP1,YP1,NPOINT,WFEED,LBOT)
296      ELSE
297          XP1=-YCLR*SIN(ANGLE)
298          YP1=YCLR*COS(ANGLE)
299      ENDIF
300  C
301  C  CONSTRUCT MEANDERED TRANSMISSION LINES FROM THE FEED POINTS.
302  C  THIS MEANDER LINE IS ALWAYS VERTICAL AND MAY BE A DIFFERENT
303  C  LENGTH FROM THAT CONNECTING THE ANTENNAS.  SUBROUTINE
304  C  MEANDER MUST BE CALLED.
305  C
306  C      WRITE(0,*)'CALL MEANDER; YCLR: ',YCLR
307      CALL MEANDER(XP,YP,XP2,YP2,NPOINT,YCLR,YDIST+YCLR-YP1,0.,
308      &  WNORM,LAMBDA,EPSR,.FALSE.)
309  C
310      IF(ITOP.NE.1)THEN
311          DO 5 N=1,NCOL
312              XX(1,N)=XO(1,N)-XP1
313          5  YY(1,N)=YO(1,1)-YDIST+YCLR
314      ELSE
315          DO 7 N=1,NCOL
316              XX(1,N)=XO(1,N)+XP1
317          7  YY(1,N)=YO(NROW,1)+YP1
318      ENDIF
319  C
320      CALL PATH(XX,YY,2,NCOL,XP,YP,0.0,0.0,NPOINT,WFEED,LTOP)
321      CALL PATH(XX,YY,2,NCOL,XP,YP,0.0,0.0,NPOINT,WFEED,LBOT)
322  C
323  C  DRAW THE T-SHAPED FEED LINE EXTENSIONS
324  C
325      CALL TEE(XO,YO,XP1,YP1,NROW,NCOL,YDIST,
326      &  YCLR,WFEED,LTOP,ITOP)
327      CALL TEE(XO,YO,XP1,YP1,NROW,NCOL,YDIST,
328      &  YCLR,WFEED,LBOT,ITOP)
329  C
330  C  DRAW THE MEANDERED LINE SECTIONS CONNECTING THE ANTENNA COLUMNS
331  C  SUBROUTINE MEANDER MUST BE CALLED TO CONSTRUCT A LINE OF DIFFERENT
332  C  PROPERTIES.
333  C
334      IF(NCOL.GT.1)THEN
335          XDIST=XO(1,2)-XO(1,1)
336  C
337          CALL MEANDER(XP,YP,XTMP,YTMP,NPOINT,YCLR,XDIST,0.,
338          &  WNORM,LAMBDA,EPSR,.TRUE.)
339  C
340          IF(ITOP.NE.1)THEN
341              DO 4 N=1,NCOL-1
342                  XX(1,N)=XO(1,N)+YCLR-XP1
343          4  YY(1,N)=YO(1,1)-YDIST
344  C  4  WRITE(0,*)'XX,YY: ',XX(1,N),YY(1,N)
345      ELSE

```



```

346          DO 6 N=1,NCOL-1
347          XX(1,N)=XO(1,N)+YCLR+XP1
348          YY(1,N)=YO(NROW,1)+YDIST
349 C          6      WRITE(0,*)'XX,YY: ',XX(1,N),YY(1,N)
350          ENDIF
351 C
352          CALL PATH(XX,YY,2,NCOL-1,XP,YP,0.0,0.0,NPOINT,WFEED,LTOP)
353          CALL PATH(XX,YY,2,NCOL-1,XP,YP,0.0,0.0,NPOINT,WFEED,LBOT)
354 C
355          ENDIF
356 C
357 C  ALL COORDINATES HAVE BEEN GENERATED. -- PLOT THE ANTENNA
358 C
359          CALL DRAWANT
360 C
361          WRITE(0,610)FACT
362 610  FORMAT(1H,6X,'Scale Factor of Plot: ',F8.3)
363 C
364          IF(ISWAP.EQ.1)THEN
365          WRITE(0,600)
366 600  FORMAT(/1H, 'Feed networks located on left or right side ',/1H,
367          &      'will plot with x- and y-coordinates interchanged.'/)
368          ENDIF
369 C
370 C
371          STOP
372          END
373 C
374 C
375          SUBROUTINE FEEDPNT(NROW,NCOL,XO,YO,MTYPE,EL1,EL2,EL3,
376          &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
377          &  YCLR,LAMBDA,ILOC,M)
378 C
379 C  THIS SUBROUTINE PLOTS THE MATCHING NETWORKS AT THE DIPOLE
380 C  FEEDPOINTS.
381          REAL LANT,LAMBDA
382          DIMENSION XO(20,20),YO(20,20),EL1(20,20)
383          DIMENSION EL2(20,20),EL3(20,20),MTYPE(20,20)
384 C
385 C  WRITE(0,*)'IN FEEDPNT; NROW,NCOL: ',NROW,NCOL
386 C
387          DO 1 M=1,NROW
388          DO 1 N=1,NCOL
389 C
390 C  WRITE(0,*)'Executing FEEDPNT, MTYPE(M,N): ',MTYPE(M,N)
391          IF(MTYPE(M,N).LT.9.OR.MTYPE(M,N).GT.16)GO TO 1
392 C
393          MM=MTYPE(M,N)-8
394          GOTO(9,10,11,12,13,14,15,16)MM
395 C
396          9  CALL NET09(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
397          &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
398          &  YCLR,LAMBDA,ILOC,M,NROW)
399          GO TO 1
400 C
401          10 CALL NET10(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
402          &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
403          &  YCLR,LAMBDA,ILOC,M,NROW)
404          GO TO 1
405 C
406          11 CALL NET11(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
407          &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
408          &  YCLR,LAMBDA,ILOC,M,NROW)
409          GO TO 1
410 C
411          12 CALL NET12(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
412          &  LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
413          &  YCLR,LAMBDA,ILOC,M,NROW)
414          GO TO 1

```

```

415 C
416 13 CALL NET13(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
417 & LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
418 & YCLR,LAMBDA,ILOC,M,NROW)
419 GO TO 1
420 C
421 14 CALL NET14(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
422 & LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
423 & YCLR,LAMBDA,ILOC,M,NROW)
424 GO TO 1
425 C
426 15 CALL NET15(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
427 & LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
428 & YCLR,LAMBDA,ILOC,M,NROW)
429 GO TO 1
430 C
431 16 CALL NET16(XO(M,N),YO(M,N),EL1(M,N),EL2(M,N),EL3(M,N),
432 & LANT,WANT,WFEED,THICK,EPSR,FTHICK,IROT,ANGLE,
433 & YCLR,LAMBDA,ILOC,M,NROW)
434 GO TO 1
435 C
436 1 CONTINUE
437 C WRITE(0,*)'YCLR: ',YCLR
438 RETURN
439 END
440 C
441 C
442 C
443 SUBROUTINE FEEDLIN(NROW,NCOL,XO,YO,WFEED,IROT,ANGLE,YCLR,
444 & ITOP,YDIST)
445 C
446 C SUBROUTINE DRAWS FEEDLINE STRUCTURE
447 DIMENSION XO(20,20),YO(20,20)
448 DATA LTOP/1/,LBOT/2/
449 C
450 DO 1 I=1,NROW
451 DO 1 J=1,NCOL
452 C
453 C DRAW THE FEED-LINE EXTENSION
454 IF(ITOP.NE.1)THEN
455 IF(I.NE.NROW)THEN
456 CALL BOX(XO(I,J),YO(I,J)-YCLR,2.*YCLR,WFEED,2,
457 & IROT,XO(I,J),YO(I,J),ANGLE,LBOT)
458 CALL BOX(XO(I,J),YO(I,J)-YCLR,2.*YCLR,WFEED,2,
459 & IROT,XO(I,J),YO(I,J),ANGLE,LTOP)
460 ELSE
461 CALL BOX(XO(I,J),YO(I,J)-YCLR,YCLR,WFEED,2,
462 & IROT,XO(I,J),YO(I,J),ANGLE,LBOT)
463 CALL BOX(XO(I,J),YO(I,J)-YCLR,YCLR,WFEED,2,
464 & IROT,XO(I,J),YO(I,J),ANGLE,LTOP)
465 ENDIF
466 C
467 ELSE
468 IF(I.NE.1)THEN
469 CALL BOX(XO(I,J),YO(I,J)-YCLR,2.*YCLR,WFEED,2,
470 & IROT,XO(I,J),YO(I,J),ANGLE,LBOT)
471 CALL BOX(XO(I,J),YO(I,J)-YCLR,2.*YCLR,WFEED,2,
472 & IROT,XO(I,J),YO(I,J),ANGLE,LTOP)
473 ELSE
474 CALL BOX(XO(I,J),YO(I,J),YCLR,WFEED,2,
475 & IROT,XO(I,J),YO(I,J),ANGLE,LBOT)
476 CALL BOX(XO(I,J),YO(I,J),YCLR,WFEED,2,
477 & IROT,XO(I,J),YO(I,J),ANGLE,LTOP)
478 ENDIF
479 C
480 ENDIF
481 C
482 1 CONTINUE
483 C

```

```
484 C
485     RETURN
486     END
487
488 C
489 C
490     SUBROUTINE BOX(XO,YO,LENG,WIDTH,ITYPE,IROT,RXO,RYO,ANGLE,LAYER)
491 C
492 C SUBROUTINE DRAWS A BOX AT ORIGIN XO,YO OF SIZE LENG BY WIDTH.
493 C IF IROT .NE. 0, THE BOX IS ROTATED ABOUT ORIGIN RXO,RYO.
494 C THE ORIENTATION OF THE BOX BEFORE ROTATION IS:
495 C     ITYPE=1, 0   DEGREES
496 C     ITYPE=2, 90  DEGREES
497 C     ITYPE=3, 180 DEGREES
498 C     ITYPE=4, 270 DEGREES
499 C
500 C
501     REAL LENG
502     DIMENSION X(5),Y(5),IP(5)
503     COMMON /COORD/NP1,NP2,NP3,X1(12000),X2(12000),X3(1100),
504 &          Y1(12000),Y2(12000),Y3(1100),
505 &          IP1(12000),IP2(12000),IP3(1100)
506 C
507 C
508     DATA LMIN/1/,LMAX/3/,EPS/1E-10/
509 C
510     IF(ITYPE.LT.1.OR.ITYPE.GT.4)THEN
511         ITYPE=1
512     ENDIF
513 C
514     IF(LAYER.LT.LMIN.OR.LAYER.GT.LMAX)THEN
515         LAYER=LMIN
516     ENDIF
517 C
518     W2=WIDTH/2.
519 C
520     GO TO (10,20,30,40)ITYPE
521 C
522 C 0 DEGREE ORIENTATION
523 C
524     10 X(1)=XO
525        Y(1)=YO-W2
526        IP(1)=3
527 C
528        X(2)=XO+LENG
529        Y(2)=Y(1)
530        IP(2)=2
531 C
532        X(3)=X(2)
533        Y(3)=Y(2)+WIDTH
534        IP(3)=2
535 C
536        X(4)=XO
537        Y(4)=Y(3)
538        IP(4)=2
539 C
540        X(5)=X(1)
541        Y(5)=Y(1)
542        IP(5)=2
543 C
544     GO TO 100
545 C
546 C 90 DEGREE ORIENTATION
547 C
548     20 X(1)=XO+W2
549        Y(1)=YO
550        IP(1)=3
551 C
552        X(2)=X(1)
```

```
553      Y(2)=Y0+LENG
554      IP(2)=2
555 C
556      X(3)=X0-W2
557      Y(3)=Y(2)
558      IP(3)=2
559 C
560      X(4)=X(3)
561      Y(4)=Y0
562      IP(4)=2
563 C
564      X(5)=X(1)
565      Y(5)=Y(1)
566      IP(5)=2
567 C
568      GO TO 100
569 C
570 C 180 DEGREE ORIENTATION
571 C
572 30 X(1)=X0
573      Y(1)=Y0+W2
574      IP(1)=3
575 C
576      X(2)=X0-LENG
577      Y(2)=Y(1)
578      IP(2)=2
579 C
580      X(3)=X(2)
581      Y(3)=Y(2)-WIDTH
582      IP(3)=2
583 C
584      X(4)=X0
585      Y(4)=Y(3)
586      IP(4)=2
587 C
588      X(5)=X(1)
589      Y(5)=Y(1)
590      IP(5)=2
591 C
592      GO TO 100
593 C
594 C
595 C 270 DEGREE ORIENTATION
596 C
597 40 X(1)=X0-W2
598      Y(1)=Y0
599      IP(1)=3
600 C
601      X(2)=X(1)
602      Y(2)=Y0-LENG
603      IP(2)=2
604 C
605      X(3)=X0+W2
606      Y(3)=Y(2)
607      IP(3)=2
608 C
609      X(4)=X(3)
610      Y(4)=Y0
611      IP(4)=2
612 C
613      X(5)=X(1)
614      Y(5)=Y(1)
615      IP(5)=2
616 C
617 C
618 100 CONTINUE
619 C
620 C
621 C THIS SECTION OF CODE ROTATES THE COORDINATES OF THE BOX ABOUT
```

```

622 C AN ARBITRARY POINT RXO, RYO. THE VARIABLE IROT IS SET TO ONE
623 C TO INDICATE ROTATION. THE ANGLE OF ROTATION IS IN RADIAN MEASURED
624 C IN THE NORMAL MATHEMATICAL SENSE.
625 C
626 C IF(IROT.EQ.1)THEN
627 C DO 2 J=1,5
628 C XH=X(J)
629 C YH=Y(J)
630 C RV=SQRT((X(J)-RXO)**2+(Y(J)-RYO)**2)
631 C THETA=ATAN2(Y(J)-RYO,X(J)-RXO+EPS)
632 C TNEW=THETA+ANGLE
633 C X(J)=RV*COS(TNEW)+RXO
634 C 2 Y(J)=RV*SIN(TNEW)+RYO
635 C WRITE(0,*)'NON-ROTATED COORDINATES: ',XH,YH
636 C 2 WRITE(0,*)'PRINTING ROTATED COORDINATES.....',X(J),Y(J)
637 C ENDF
638 C
639 C
640 C
641 C NOW THE DATA (ROTATED IF DESIRED) ARE WRITTEN INTO THREE
642 C ARRAYS CORRESPONDING TO THE THREE LAYERS: TOP LAYER, BOTTOM
643 C LAYER, AND VIA LAYER. PEN LIFT INFORMATION IS ALSO RECORDED
644 C IN AN ARRAY FOR EACH LAYER.
645 C
646 C DO 1 J=1,5
647 C
648 C GOTO(50,60,70)LAYER
649 C
650 C 50 X1(NP1)=X(J)
651 C Y1(NP1)=Y(J)
652 C IP1(NP1)=IP(J)
653 C NP1=NP1+1
654 C GO TO 1
655 C
656 C 60 X2(NP2)=X(J)
657 C Y2(NP2)=Y(J)
658 C IP2(NP2)=IP(J)
659 C NP2=NP2+1
660 C GO TO 1
661 C
662 C 70 X3(NP3)=X(J)
663 C Y3(NP3)=Y(J)
664 C IP3(NP3)=IP(J)
665 C NP3=NP3+1
666 C
667 C 1 CONTINUE
668 C
669 C II=II+1
670 C IF(II/100*100.EQ.II)THEN
671 C WRITE(0,*)'NP1,NP2,NP3 ',NP1,NP2,NP3
672 C ENDF
673 C
674 C RETURN
675 C END
676 C
677 C
678 C SUBROUTINE DRAWANT
679 C
680 C THIS SUBROUTINE PLOTS THE COORDINATES STORED IN THE
681 C COORDINATE ARRAYS X1,X2,X3,Y1,Y2, AND Y3 UNDER CONTROL
682 C OF THE PEN-LIFT PARAMETERS IN IP1,IP2, AND IP3.
683 C
684 C COMMON /COORD/NP1,NP2,NP3,X1(12000),X2(12000),X3(1100),
685 C & Y1(12000),Y2(12000),Y3(1100),
686 C & IP1(12000),IP2(12000),IP3(1100)
687 C COMMON /WINSIZ/WX1,WY1,WX2,WY2,FACT
688 C
689 C DATA XMAX/-1E10/,XMIN/1E10/,YMAX/-1E10/,YMIN/1E10/
690 C

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691      WRITE(0,100)
692 100 FORMAT(1H,'Plotting.... '/')
693 C
694 C
695      CALL COLOR(1,IERR)
696      DO 1 J=1, NP1-1
697          IF(X1(J).GE.XMAX)XMAX=X1(J)
698          IF(X1(J).LE.XMIN)XMIN=X1(J)
699          IF(Y1(J).GE.YMAX)YMAX=Y1(J)
700          IF(Y1(J).LE.YMIN)YMIN=Y1(J)
701          CALL PLOT(X1(J),Y1(J),IP1(J))
702 1 CONTINUE
703 C
704      CALL PLOT(0.0,0.0,-999)
705 C      WRITE(0,*)'WX1,WY1,WX2,WY2: ',WX1,WY1,WX2,WY2
706 C
707      BX1=WX1
708      BX2=WX2
709      BY1=WY1
710      BY2=WY2
711 C
712      CALL WINDOW(BX1,BY1,BX2,BY2)
713      CALL FACTOR(FACT)
714 C
715      CALL COLOR(2,IERR)
716 C
717      DO 2 J=1, NP2-1
718          CALL PLOT(X2(J),Y2(J),IP2(J))
719 2 CONTINUE
720 C
721      CALL PLOT(0.0,0.0,-999)
722 C
723      BX1=WX1
724      BX2=WX2
725      BY1=WY1
726      BY2=WY2
727 C
728 C      WRITE(0,*)'WX1,WY1,WX2,WY2: ',WX1,WY1,WX2,WY2
729      CALL WINDOW(BX1,BY1,BX2,BY2)
730      CALL FACTOR(FACT)
731 C
732      IF(NP3.GT.1)THEN
733          CALL COLOR(3,IERR)
734          DO 3 J=1, NP3-1
735              CALL PLOT(X3(J),Y3(J),IP3(J))
736 3 CONTINUE
737      ENDIF
738 C
739 777 CALL PLOT(0.,0.,999)
740 C
741      WRITE(0,110)NP1-1, NP2-1, NP3-1
742 110 FORMAT(1H,'Coordinates Plotted: '/1H ,
743      & 6X,'Top Layer: ',110/1H ,
744      & 6X,'Bottom Layer: ',110/1H ,
745      & 6X,'Cross-Over: ',110/)
746 C
747      WRITE(0,200)XMIN,XMAX,YMIN,YMAX
748 200 FORMAT(1H,6X,'Minimum X-Coordinate: ',F12.3/1H,
749      & 6X,'Maximum X-Coordinate: ',F12.3/1H,
750      & 6X,'Minimum Y-Coordinate: ',F12.3/1H,
751      & 6X,'Maximum Y-Coordinate: ',F12.3/)
752 C
753      RETURN
754      END
755 C
756 C
757      BLOCK DATA INITIL
758 C BLOCK DATA SUBPROGRAM TO INITILIZE COMMON BLOCK
759      COMMON /COORD/NP1,NP2,NP3,X1(12000),X2(12000),X3(1100),

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760      &                                Y1(12000),Y2(12000),Y3(1100),
761      &                                IP1(12000),IP2(12000),IP3(1100)
762      DATA NP1/1/,NP2/1/NP3/1/
763      END
764 C
765 C
766      SUBROUTINE MEANDER(X,Y,XP1,YP1,NPOINT,YCLR,YSPAC,ANGLE,
767      &                                WNORM,LAMBDA,EPSR,RFLAG)
768 C
769      LOGICAL RFLAG
770      DIMENSION X(30),Y(30),XM(30),YM(30)
771      REAL LD,LG,LAMBDA
772      DATA PIOVR2/1.570796327/,EPS/1E-15/
773 C
774 C THIS SUBPROGRAM DETERMINES THE DIMENSIONS OF A MEANDERING
775 C TRANSMISSION LINE OF THE LENGTH NEEDED TO MAKE THE SPACING
776 C BETWEEN ELEMENTS TO BE A MULTIPLE OF ONE-HALF WAVELENGTH.
777 C
778 C YSPAC IS THE DISTANCE BETWEEN ANTENNA CENTERS.
779 C YCLR IS THE FEED-LINE EXTENSION AT THE ANTENNA.
780 C DDIR IS THE DIRECT DISTANCE BETWEEN EXTENSIONS (ONE ANTENNA
781 C TO THE NEXT).
782 C DTOT IS THE TOTAL DIRECT PATH DISTANCE INCLUDING THE EXTENSIONS.
783 C
784 C
785      XP1=-YCLR*SIN(ANGLE)
786      YP1= YCLR*COS(ANGLE)
787      XP2=-XP1
788      YP2= YSPAC-YP1
789      DDIR=SQRT((XP2-XP1)**2+(YP2-YP1)**2)
790      DTOT=DDIR+2.*YCLR
791 C
792 C      WRITE(0,*)'YSPAC: ',YSPAC
793 C      WRITE(0,*)'XP1,XP2,YP1,YP2: ',XP1,XP2,YP1,YP2
794 C      WRITE(0,*)'DTOT: ',DTOT
795 C
796 C COMPARE THIS DISTANCE WITH THAT NEEDED TO MAKE INTEGRAL MULTIPLES
797 C OF ONE-HALF WAVE.
798 C
799 C CHECK THE SPECIAL CASE--IS THE LENGTH ALREADY WITHIN 1/100 WAVELENGTH
800 C OF THE CORRECT DISTANCE.
801 C
802 C LG IS THE WAVELENGTH ALONG THE TRANSMISSION LINE
803      LG=LAMBDA/SQRT(EPSR)
804 C WLIM IS THE MAXIMUM ALLOWABLE WIDTH OF THE MEANDER
805      WLIM=WNORM*LG
806 C
807 C      DO 1 N=1,10
808 C          IF(ABS(DTOT-FLOAT(N)*.5*LG).LE.0.01*LG)THEN
809 C              GO TO 100
810 C          ENDIF
811 C      1 CONTINUE
812 C
813 C      DO 2 N=1,10
814 C          LD=FLOAT(N)*.5*LG
815 C          WRITE(0,*)'N, DTOT, LG, LD: ',N,DTOT,LG,LD
816 C          IF(LD.GE.DTOT)THEN
817 C              GO TO 200
818 C          ENDIF
819 C      2 CONTINUE
820 C
821 C      STOP 'UNABLE TO EXTEND FEED LINE TO MULTIPLE OF HALF-WAVE.'
822 C
823 C CALCULATE PARAMETERS OF THE MEANDER LINE.
824      200 CONTINUE
825 C      WRITE(0,*)'N,DTOT,LG,LD,YCLR: ',N,DTOT,LG,LD,YCLR
826 C COMPUTE THE LENGTH OF THE MEANDERED SECTION OF THE LINE
827      DMEA=LD-2.*YCLR
828 C      WRITE(0,*)'MEANDERED LNG: ',DMEA

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829 C   WRITE(0,*)'DIRECT COURSE DISTANCE: ',DDIR
830 C
831 C   THE DIRECT COURSE DISTANCE IS DDIR
832 C
833 C       DO 3 N=4,20,4
834 C           W=2.*SQRT(DMEA**2-DDIR**2)/FLOAT(N)
835 C           WRITE(0,*)'DMEA, DDIR, W: ',DMEA,DDIR,W
836 C           IF(W.LE.WLIM)THEN
837 C               NSEGS=N
838 C               WRITE(0,*)'W,NSEGS: ',W,NSEGS
839 C               GO TO 300
840 C           ENDIF
841 C       3 CONTINUE
842 C
843 C       WRITE(0,*)'*** ERROR: Meander Line Exceeds 20 Segments.'
844 C
845 C   THIS CODE CREATES THE MEANDER LINE.
846 C   300 CONTINUE
847 C       WRITE(0,*)'SEGMENTS: ',NSEGS
848 C
849 C
850 C       W2=W/2.
851 C       DELTAX=DDIR/FLOAT(NSEGS)
852 C
853 C       WRITE(0,*)'DELTAX, W2: ',DELTAX,W2
854 C       DO 4 N=1,NSEGS+1
855 C
856 C   CODE TO MAKE TAKE-OFF FROM MATCHING NETWORK NOT PRALLEL TO ANTENNA.
857 C       IF(ANGLE.LT.0.)THEN
858 C           XM(N)=+W2*SIN(PIOVR2*FLOAT(N-1))
859 C       ELSE
860 C           XM(N)=-W2*SIN(PIOVR2*FLOAT(N-1))
861 C       ENDIF
862 C
863 C       YM(N)=DELTAX*(FLOAT(N-1))
864 C
865 C       WRITE(0,111)XM(N),YM(N)
866 C 111   FORMAT(1H,'COORDINATES: ',2F10.3)
867 C       4 CONTINUE
868 C
869 C       CALL PLOT(0.0,0.0,999)
870 C   ROTATE THE MEANDER LINE AT THE BOTTON END BY THE ANGLE
871 C   NECESSARY TO CONNECT TO THE NEXT FEED NETWORK.
872 C
873 C       IF(ABS(XP2-XP1).LE.1E-8)THEN
874 C           TH1=0.
875 C       ELSE
876 C           TH1=ATAN2(YP2-YP1,XP2-XP1)-PIOVR2
877 C       ENDIF
878 C
879 C       WRITE(0,*)'ANGLE TH1: ',TH1
880 C
881 C       WRITE(0,444)
882 C 444   FORMAT(1H,'ENTER ANGLE OF ROTATION: '\)
883 C       READ(0,*)TH1
884 C
885 C       IF(RFLAG)TH1=-PIOVR2
886 C
887 C       DO 5 N=1,NSEGS+1
888 C           RV=SQRT((XM(N)-XM(1))**2+(YM(N)-YM(1))**2)
889 C           TH2=ATAN2(YM(N)-YM(1)+EPS,XM(N)-XM(1)+EPS)
890 C           TNEW=TH2+TH1
891 C           X(N)=RV*COS(TNEW)+XM(1)
892 C           Y(N)=RV*SIN(TNEW)+YM(1)
893 C       5 CONTINUE
894 C
895 C   ZERO WIDTH MEANDER LINE HAS BEEN CREATED AND ROTATED.
896 C   A CALL TO THE SUBROUTINE PATH WILL CHANGE THIS ZERO
897 C   WIDTH LINE INTO A SERIES OF CONNECTED BOXES.

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898 C
899     NPOINT=NSEGS+1
900 C
901     RETURN
902     END
903 C
904 C
905     SUBROUTINE TEE(XO,YO,XP1,YP1,NROW,NCOL,YDIST,
906 &                 YCLR,WIDTH,LAYER,ITOP)
907 C
908     DIMENSION XO(20,20),YO(20,20)
909 C
910     WRITE(0,*)'IN SUBROUTINE TEE...'
911 C    DRAW THE T-CONNECTORS
912     DO 2 N=1,NCOL
913 C
914         IF(ITOP.EQ.1)THEN
915             XF=XO(NROW,N)+XP1
916             YF=YO(NROW,N)+YDIST
917 C
918             IF(N.NE.NCOL)THEN
919                 CALL BOX(XF,YF,YCLR,WIDTH,1,0,XF,YF,
920 &                     0.,LAYER)
921             ELSE
922                 CALL BOX(XF,YF,YCLR,WIDTH,1,0,XF,YF,
923 &                     0.,LAYER)
924             ENDIF
925 C
926             CALL BOX(XF,YF,YCLR,WIDTH,4,0,XF,YF,
927 C &                 0.,LAYER)
928 C
929             IF(N.NE.1)THEN
930                 CALL BOX(XF,YF,YCLR,WIDTH,3,0,XF,YF,
931 &                     0.,LAYER)
932 C
933             ENDIF
934 C
935         ELSE
936             XF=XO(1,N)-XP1
937             YF=YO(1,N)-YDIST
938 C
939             IF(N.NE.NCOL)THEN
940                 CALL BOX(XF,YF,YCLR,WIDTH,1,0,XF,YF,
941 &                     0.,LAYER)
942             ELSE
943 C             CALL BOX(XF,YF,YCLR,WIDTH,1,0,XF,YF,
944 C &                 0.,LAYER)
945             ENDIF
946 C
947             CALL BOX(XF,YF,YCLR,WIDTH,2,0,XF,YF,
948 &                 0.,LAYER)
949 C
950             IF(N.NE.1)THEN
951                 CALL BOX(XF,YF,YCLR,WIDTH,3,0,XF,YF,
952 &                     0.,LAYER)
953             ENDIF
954 C
955         ENDIF
956 C
957         IF(ITOP.NE.1)THEN
958             IF(N.EQ.NCOL/2+1)THEN
959                 CALL BOX(XF,YF,YCLR,WIDTH,4,0,XF,YF,0.,LAYER)
960             ENDIF
961         ELSE
962             IF(N.EQ.NCOL/2+1)THEN
963                 CALL BOX(XF,YF,YCLR,WIDTH,2,0,XF,YF,0.,LAYER)
964             ENDIF
965         ENDIF
966 C
```

```

967 C
968   2 CONTINUE
969 C
970   RETURN
971   END
972 C
973 C
974   SUBROUTINE PATH(XO,YO,NROW,NCOL,XP,YP,XP1,YP1,NPOINT,WIDTH,LAYER)
975 C
976 C SUBROUTINE DRAWS AN ANGLED BOX BETWEEN POINTS IN ARRAY XP,YP.
977 C REVISION OF 9/8/89
978 C
979   COMMON /COORD/NP1,NP2,NP3,X1(12000),X2(12000),X3(1100),
980   &      Y1(12000),Y2(12000),Y3(1100),
981   &      IP1(12000),IP2(12000),IP3(1100)
982 C
983   DIMENSION XP(NPOINT),YP(NPOINT)
984   DIMENSION XO(20,20),YO(20,20)
985 C
986   DATA LMIN/1/,LMAX/3/
987   DATA PI/3.141592654/,MAXSEG/8/
988 C
989 C   WRITE(0,*)'IN PATH, WIDTH, LAYER: ',WIDTH,LAYER
990   IF(LAYER.LT.LMIN.OR.LAYER.GT.LMAX)THEN
991     LAYER=LMIN
992   ENDIF
993 C
994 C   WRITE(0,*)'NPOINT: ',NPOINT
995 C   WRITE(0,*)'NROW,NCOL: ',NROW,NCOL
996   W2=WIDTH/2.
997 C
998   DO 2 I=1,NROW-1
999   DO 2 J=1,NCOL
1,000 C
1,001   DO 1 N=1,NPOINT-1
1,002 C   WRITE(0,*)'NP1,NP2,NP3: ',NP1,NP2,NP3
1,003 C
1,004   DX=XP(N+1)-XP(N)
1,005   DY=YP(N+1)-YP(N)
1,006 C
1,007   ANGLE=ATAN2(DY,DX)
1,008 C
1,009   COSA=W2*COS(ANGLE)
1,010   SINA=W2*SIN(ANGLE)
1,011 C
1,012   IF(LAYER.LT.1.OR.LAYER.GT.3)THEN
1,013     WRITE(0,*)'LAYER: ',LAYER,' IS OUT OF RANGE.'
1,014     LAYER=1
1,015   ENDIF
1,016 C
1,017 C   WRITE FEEDLINE MEANDER DATA INTO MEMORY
1,018 C
1,019   GO TO (10,20,30)LAYER
1,020 C
1,021 C
1,022   10 X1(NP1)=XO(I,J)+XP1+XP(N)+SINA
1,023     Y1(NP1)=YO(I,J)+YP1+YP(N)-COSA
1,024     IP1(NP1)=3
1,025     NP1=NP1+1
1,026 C
1,027   X1(NP1)=XO(I,J)+XP1+XP(N+1)+SINA
1,028   Y1(NP1)=YO(I,J)+YP1+YP(N+1)-COSA
1,029   IP1(NP1)=2
1,030   NP1=NP1+1
1,031 C
1,032   DO 3 K=1,MAXSEG
1,033     PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI
1,034     X1(NP1)=XO(I,J)+XP1+XP(N+1)+W2*SIN(PHI)
1,035     Y1(NP1)=YO(I,J)+YP1+YP(N+1)-W2*COS(PHI)

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```
1,036      IP1(NP1)=2
1,037      NP1=NP1+1
1,038      3 CONTINUE
1,039      C
1,040      X1(NP1)=XO(I,J)+XP1+XP(N)-SINA
1,041      Y1(NP1)=YO(I,J)+YP1+YP(N)+COSA
1,042      IP1(NP1)=2
1,043      NP1=NP1+1
1,044      C
1,045      DO 4 K=1,MAXSEG
1,046      PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI+PI
1,047      X1(NP1)=XO(I,J)+XP1+XP(N)+W2*SIN(PHI)
1,048      Y1(NP1)=YO(I,J)+YP1+YP(N)-W2*COS(PHI)
1,049      IP1(NP1)=2
1,050      NP1=NP1+1
1,051      4 CONTINUE
1,052      C
1,053      GO TO 1
1,054      C
1,055      C
1,056      20 X2(NP2)=XO(I,J)+XP1+XP(N)+SINA
1,057      Y2(NP2)=YO(I,J)+YP1+YP(N)-COSA
1,058      IP2(NP2)=3
1,059      NP2=NP2+1
1,060      C
1,061      X2(NP2)=XO(I,J)+XP1+XP(N+1)+SINA
1,062      Y2(NP2)=YO(I,J)+YP1+YP(N+1)-COSA
1,063      IP2(NP2)=2
1,064      NP2=NP2+1
1,065      C
1,066      DO 5 K=1,MAXSEG
1,067      PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI
1,068      X2(NP2)=XO(I,J)+XP1+XP(N+1)+W2*SIN(PHI)
1,069      Y2(NP2)=YO(I,J)+YP1+YP(N+1)-W2*COS(PHI)
1,070      IP2(NP2)=2
1,071      NP2=NP2+1
1,072      5 CONTINUE
1,073      C
1,074      X2(NP2)=XO(I,J)+XP1+XP(N)-SINA
1,075      Y2(NP2)=YO(I,J)+YP1+YP(N)+COSA
1,076      IP2(NP2)=2
1,077      NP2=NP2+1
1,078      C
1,079      DO 6 K=1,MAXSEG
1,080      PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI+PI
1,081      X2(NP2)=XO(I,J)+XP1+XP(N)+W2*SIN(PHI)
1,082      Y2(NP2)=YO(I,J)+YP1+YP(N)-W2*COS(PHI)
1,083      IP2(NP2)=2
1,084      NP2=NP2+1
1,085      6 CONTINUE
1,086      C
1,087      GO TO 1
1,088      C
1,089      C
1,090      30 X3(NP3)=XO(I,J)+XP1+XP(N)+SINA
1,091      Y3(NP3)=YO(I,J)+YP1+YP(N)-COSA
1,092      IP3(NP3)=3
1,093      NP3=NP3+1
1,094      C
1,095      X3(NP3)=XO(I,J)+XP1+XP(N+1)+SINA
1,096      Y3(NP3)=YO(I,J)+YP1+YP(N+1)-COSA
1,097      IP3(NP3)=2
1,098      NP3=NP3+1
1,099      C
1,100      DO 7 K=1,MAXSEG
1,101      PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI
1,102      X3(NP3)=XO(I,J)+XP1+XP(N+1)+W2*SIN(PHI)
1,103      Y3(NP3)=YO(I,J)+YP1+YP(N+1)-W2*COS(PHI)
1,104      IP3(NP3)=2
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```
1,105      NP3=NP3+1
1,106      7 CONTINUE
1,107 C
1,108      X3(NP3)=X0(I,J)+XP1+XP(N)-SINA
1,109      Y3(NP3)=Y0(I,J)+YP1+YP(N)+COSA
1,110      IP3(NP3)=2
1,111      NP3=NP3+1
1,112 C
1,113      DO 8 K=1,MAXSEG
1,114      PHI=ANGLE+FLOAT(K)/FLOAT(MAXSEG)*PI+PI
1,115      X3(NP3)=X0(I,J)+XP1+XP(N)+W2*SIN(PHI)
1,116      Y3(NP3)=Y0(I,J)+YP1+YP(N)-W2*COS(PHI)
1,117      IP3(NP3)=2
1,118      NP3=NP3+1
1,119      8 CONTINUE
1,120 C
1,121 C
1,122      1 CONTINUE
1,123      2 CONTINUE
1,124 C
1,125 C
1,126      RETURN
1,127 C
1,128      END
1,129 C
```

```

1 C
2 C ***** C
3 C
4 C           ELEMENT CALCULATION SUBROUTINES
5 C
6 C ***** C
7 C
8 C     SUBROUTINE SHUNTC(XORG,YORG,C,WCAP,WFEED,WMIN,
9 C     &                THICK,EPSR,IROT,ANGLE,CLR,ITYPE,YCLR)
10 C
11 C     THIS SUBROUTINE DRAWS A SHUNT CAPACITOR BETWEEN THE
12 C     ANTENNA ELEMENTS OR ACROSS THE FEEDLINE AS SELECTED
13 C     BY ITYPE.
14 C         ITYPE = 1   A CAPACITOR IS DRAWN ACROSS THE FEEDLINE.
15 C         ITYPE = 2   A CAPACITOR IS DRAWN BETWEEN THE ANTENNAS.
16 C
17 C     REAL L1,LSC,LSC1,LANT,LSC3,LCROS
18 C     DATA OL/.05/,LTOP/1/,LBOT/2/,LCRS/3/
19 C
20 C     IF(ITYPE.NE.1.AND.ITYPE.NE.2)RETURN
21 C
22 C     IF(ITYPE.EQ.1)THEN
23 C         CALL CAPVAL(WMIN,C,WSC,LSC,EPSR,THICK)
24 C
25 C         WSC2=WSC/2.
26 C         WF2=WFEED/2.
27 C         WC2=WCAP/2.
28 C
29 C     CAPACITOR PLATE CONNECTED TO TOP FEED LINE.
30 C         X1=XORG-WSC2-CLR-WF2
31 C         Y1=YORG+WC2-OL
32 C         LSC1=LSC+OL+CLR
33 C         CALL BOX(X1,Y1,LSC1,WSC,2,IROT,XORG,YORG,ANGLE,LTOP)
34 C
35 C     CAPACITOR PLATE ON RIGHT SIDE CONNECTED BY CROSS-OVER
36 C         X2=XORG+WSC2+CLR+WF2
37 C         Y2=YORG+WC2+CLR
38 C         CALL BOX(X2,Y2,LSC,WSC,2,IROT,XORG,YORG,ANGLE,LTOP)
39 C
40 C     CAPACITOR PLATE CONNECTED TO BOTTOM FEED LINE.
41 C         X3=XORG+WSC2+CLR+WF2
42 C         Y3=Y1
43 C         LSC3=LSC1
44 C         CALL BOX(X3,Y3,LSC3,WSC,2,IROT,XORG,YORG,ANGLE,LBOT)
45 C
46 C     CROSS-OVER ON LAYER 3 CONNECTING LEFT AND RIGHT TOP PLATES.
47 C
48 C         X4=XORG-WF2-CLR-WSC2
49 C         Y4=YORG+WC2+CLR+LSC/2.
50 C         LCROS=WFEED+2.*CLR+WSC
51 C         CALL BOX(X4,Y4,LCROS,LSC,1,IROT,XORG,YORG,ANGLE,LCRS)
52 C
53 C     ENDIF
54 C
55 C     IF(ITYPE.EQ.2)THEN
56 C         CALL CAPVAL(WMIN,C,WSC,LSC,EPSR,THICK)
57 C
58 C         WSC2=WSC/2.
59 C         WF2=WFEED/2.
60 C         WC2=WCAP/2.
61 C
62 C     CAPACITOR PLATE CONNECTED TO LEFT-HAND (BOTTOM) ANTENNA.
63 C         X1=XORG-WSC2-CLR-WF2
64 C         Y1=YORG-WC2+OL
65 C         LSC1=LSC+OL+CLR
66 C         CALL BOX(X1,Y1,LSC1,WSC,4,IROT,XORG,YORG,ANGLE,LBOT)
67 C
68 C     CAPACITOR PLATE CONNECTED TO RIGHT-HAND (TOP) ANTENNA.
69 C         X3=XORG+WSC2+CLR+WF2

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70      Y3=Y1
71      LSC3=LSC1
72      CALL BOX(X3,Y3,LSC3,WSC,4,IROT,XORG,YORG,ANGLE,LTOP)
73 C
74 C  CAPACITOR PLATE ON LEFT SIDE CONNECTED BY CROSS-OVER
75      X2=X1
76      Y2=YORG-WC2-CLR
77      CALL BOX(X2,Y2,LSC,WSC,4,IROT,XORG,YORG,ANGLE,LTOP)
78 C
79 C  CROSS-OVER ON LAYER 3 CONNECTING LEFT AND RIGHT TOP PLATES.
80 C
81      X4=XORG-WF2-CLR-WSC2
82      Y4=YORG-WC2-CLR-LSC/2.
83      LCROS=WFEED+2.*CLR+WSC
84      CALL BOX(X4,Y4,LCROS,LSC,1,IROT,XORG,YORG,ANGLE,LCRS)
85 C
86      ENDIF
87 C
88 C  DETERMINE LENGTH OF TLINE TO CLEAR ALL MATCHING ELEMENTS
89 C
90      YCL=WC2+CLR+LSC+WFEED
91 C
92      IF(YCL.GE.YCLR)YCLR=YCL
93 C
94      RETURN
95 C
96      END
97 C
98 C
99      SUBROUTINE CAPVAL(WANT,CC,WC,LC,EPSR,THICK)
100 C  THIS SUBROUTINE CALCULATES THE DIMENSIONS OF A METAL FOIL
101 C  CAPACITOR FROM GIVEN MILAR PROPERTIES.
102      REAL LC
103 C
104      DIMENSION WIDTHS(6)
105      DATA WIDTHS/.125,.25,.375,.5,.75,1.0/
106 C
107 C  WRITE(0,*)'EPSR, C (pF): ',EPSR,CC
108      C=CC*1E-12
109      TH=THICK*2.54E-5
110      A=C*TH/(8.854E-12*EPSR)
111      A=A/(.0254**2)
112 C
113      X=SQRT(A)
114 C  WRITE(0,*)'A,X ',A,X
115      IF(X.LE.WANT)THEN
116          WC=WANT
117          LC=A/WC
118          RETURN
119      ENDIF
120 C
121      DO 1 J=1,6
122      IF(X.LE.WIDTHS(J))THEN
123          WC=WIDTHS(J)
124          LC=A/WC
125 C  WRITE(0,*)'WIDTH/LENGTH OF LINE: ',WC,LC
126          RETURN
127      ENDIF
128      1 CONTINUE
129 C
130 C  USE LARGEST WIDTH MATERIAL
131      WC=WIDTHS(6)
132      LC=A/WC
133      RETURN
134      END
135 C
136 C
137      SUBROUTINE XNDVAL(L,O,D,LAMBDA,W,T)
138 C

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139 C CALLING FORM IN VARIOUS PARTS OF THESE PROGRAMS
140 C
141 C SUBROUTINE INDVAL(L,W,D,LAMBDA,WIND,FTHICK)
142 C
143 C L IS THE INDUCTANCE IN nH.
144 C O IS THE OUTSIDE DIMENSION OF THE HORSE SHOE.
145 C D IS THE DEPTH OF THE HORSE SHOE.
146 C W IS THE WIDTH OF THE STRIP.
147 C T IS THE THICKNESS OF THE METAL FOIL.
148 C LAMBDA IS THE WAVELENGTH AT THE FREQUENCY OF OPERATION.
149 C
150 C REAL L,LAMBDA
151 C DATA DELTAD/0.0005/,ERROR/0.001/,DMIN/0.01/
152 C
153 C NTRY=0
154 C GUESS A VALUE
155 C D1=L/20.
156 C
157 C 10 NTRY=NTRY+1
158 C U1=UIND(O,W,D1,T)
159 C Y1=L-U1
160 C U2=UIND(O,W,D1+DELTAD,T)
161 C Y2=L-U2
162 C IF(U1.LT.0..OR.U2.LT.0.)THEN
163 C D=DMIN
164 C WRITE(0,100)
165 C 100 FORMAT(1H , '*** WARNING - Inductance Too Small'/1H ,
166 C & ' ' ' 0.01 Inch U-Depth Used')
167 C
168 C RETURN
169 C ELSE
170 C D2=D1-DELTAD*Y1/(Y2-Y1)
171 C ENDIF
172 C WRITE(0,*)'D1,D2: ',D1,D2
173 C
174 C IF(ABS(D2-D1).LE.ERROR)THEN
175 C D=D2
176 C IF(D.LT.DMIN)THEN
177 C D=DMIN
178 C WRITE(0,100)
179 C ENDIF
180 C
181 C IF(D.GT.0.15*LAMBDA)THEN
182 C D=0.15*LAMBDA
183 C WRITE(0,200)
184 C 200 FORMAT(1H , '*** WARNING - Inductance Too Large'/1H ,
185 C & ' ' ' 0.15 Lambda Long Lines Used')
186 C ENDIF
187 C
188 C RETURN
189 C ELSE
190 C D1=D2
191 C GO TO 10
192 C ENDIF
193 C
194 C
195 C RETURN
196 C END
197 C
198 C
199 C REAL FUNCTION UIND(O,W,D,T)
200 C
201 C CALCULATION OF INDUCTANCE OF U-SHAPED COILS
202 C REAL L11,L12,L22,L33,IND
203 C
204 C O Is the outer dimensions of the U-shape.
205 C W Is the width of the flat strip conductor.
206 C D Is the depth of the U-shaped conductor. (inside the U)
207 C T Is the thickness of the flat conductor.

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208 C
209 C   WRITE(0,100)
210 C 100 FORMAT(1H,'Enter O,D,W,T:  '\)
211 C   READ(0,*)O,D,W,T
212 C
213 C   X1=D+W
214 C
215 C   CHECK TO SEE IF THE INDUCTANCE IS TOO SMALL TO BE REALIZED.
216 C
217 C   IF(X1.LE.0.)THEN
218 C     UIND=-1.
219 C     RETURN
220 C   ENDIF
221 C
222 C   X3=X1
223 C   X2=0-2*W
224 C
225 C   L11=5.08*X1*(LOG(2.*X1/(W+T)) + (W+T)/(3.*X1) + .50049)
226 C
227 C   L22=5.08*X2*(LOG(2.*X2/(W+T)) + (W+T)/(3.*X2) + .50049)
228 C
229 C   L33=5.08*X3*(LOG(2.*X3/(W+T)) + (W+T)/(3.*X3) + .50049)
230 C
231 C   X=(O-W)/W
232 C   GMDL=ALOG(X*W)-(1./(12.*X**2) + 1./(60.*X**4) + 1./(168.*X**6)
233 C   & + 1./(360.*X**8) + 1./(660.*X**10) )
234 C   GMD=EXP(GMDL)
235 C
236 C   Y=X1/GMD
237 C   Q=ALOG(Y + SQRT(1.+Y**2)) - SQRT(1.+1./Y**2) + 1./Y
238 C
239 C   L12=5.08*X1*Q
240 C
241 C   UIND=L11+L22+L33-2.*L12
242 C
243 C   WRITE(0,200)IND
244 C 200 FORMAT(1H,'Inductance (nH): ',1F8.1)
245 C
246 C   RETURN
247 C   END
248 C
249 C   SUBROUTINE INDVAL(L,O,D,LAMBDA,W,T)
250 C
251 C   L IS THE INDUCTANCE IN nH.
252 C   W IS THE OUTSIDE DIMENSION OF THE HORSE SHOE.
253 C   D IS THE DEPTH OF THE HORSE SHOE.
254 C   REAL L,LAMBDA
255 C   WRITE(0,*)'L,W: ',L,W
256 C
257 C   DETERMINE SLOPE AND INTERCEPT OF INDUCTANCE EQUATIONS
258 C   XINT=-2.655+13.861*W
259 C   SLOP= 7.659+40.38*W
260 C   CALCULATE DEPTH OF HORSE SHOE
261 C   D=(L-XINT)/SLOP
262 C   WRITE(0,*)'L, D ',L,D
263 C   IF(D.LE..025)D=.025
264 C   IF(D.GT.0.15*LAMBDA)D=0.15*LAMBDA
265 C
266 C   RETURN
267 C   END
268 C
269 C   SUBROUTINE SHUNT(L,XORG,YORG,WFEED,WIND,FTICK,WC,LC,
270 C   & CLR,L,LAMBDA,ITYPE,IROT,ANGLE,YCLR)
271 C
272 C   THIS SUBROUTINE DRAWS A SHUNT INDUCTOR BETWEEN THE
273 C   ANTENNA ELEMENTS OR ACROSS THE FEEDLINE AS SELECTED
274 C   BY ITYPE.
275 C   ITYPE = 1   AN INDUCTOR IS DRAWN ACROSS THE FEEDLINE.
276 C   ITYPE = 2   AN INDUCTOR IS DRAWN BETWEEN THE ANTENNAS.

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277 C
278     REAL LC,LC2,L,LAMBDA
279     DATA LTOP/1/,LBOT/2/,LBRD/3/
280 C
281 C   DRAW THE INDUCTORS
282 C
283     IF(ITYPE.NE.1.AND.ITYPE.NE.2.)RETURN
284 C
285     LC2=LC/2.
286     WF2=WFEED/2.
287     WIND2=WIND/2.
288     WIND4=WIND/4.
289     WC2=WC/2.
290 C
291     IF(ITYPE.EQ.2)THEN
292 C
293 C   DRAW THE ANTENNA INDUCTOR (BOTTOM)
294 C
295 C   GET THE PARAMETERS OF THE INDUCTOR
296     IF(L.LE.8.)THEN
297         X1=XORG-CLR-WF2-WIND2
298         X2=XORG+CLR+WF2+WIND2
299         CALL INDVAL(L,2.*(WF2+CLR)+WIND,D,LAMBDA,WIND,FTHICK)
300     ELSEIF(L.GT.8..AND.L.LE.20.)THEN
301         X1=XORG-WF2-CLR-LC2
302         X2=XORG+WF2+CLR+LC2
303         CALL INDVAL(L,X2-X1+WIND,D,LAMBDA,WIND,FTHICK)
304     ELSE
305         X1=XORG-WF2-CLR-LC2
306         X2=XORG+WF2+CLR+LC2
307         CALL INDVAL(L,X2-X1+WIND,D,LAMBDA,WIND,FTHICK)
308     ENDIF
309 C
310     Y1=YORG-WC2+WIND4
311     Y2=Y1
312     X3=X1-WIND2
313     Y3=YORG-WC2-D-WIND2
314 C
315     CALL BOX(X1,Y1,D+WIND+WIND4,WIND,4,IROT,XORG,YORG,ANGLE,LBOT)
316     CALL BOX(X2,Y1,D+WIND+WIND4,WIND,4,IROT,XORG,YORG,ANGLE,LTOP)
317     CALL BOX(X3,Y3,X2-X1+WIND,WIND,1,IROT,XORG,YORG,ANGLE,LBRD)
318 C
319 C   MAKE A VIA
320 C     CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
321 C
322     ENDIF
323 C
324     IF(ITYPE.EQ.1)THEN
325 C
326 C   DRAW THE FEEDLINE INDUCTOR (TOP)
327 C
328 C   GET THE PARAMETERS OF THE INDUCTOR
329     IF(L.LE.8.)THEN
330         X1=XORG+WF2+CLR+WIND2
331         X2=XORG-WF2-CLR-WIND2
332         CALL INDVAL(L,2.*(WF2+CLR)+WIND,D,LAMBDA,WIND,FTHICK)
333     ELSEIF(L.GT.8..AND.L.LE.20.)THEN
334         X1=XORG+WF2+CLR+LC2
335         X2=XORG-WF2-CLR-LC2
336         CALL INDVAL(L,X1-X2+WIND,D,LAMBDA,WIND,FTHICK)
337     ELSE
338         X1=XORG+WF2+CLR+LC2
339         X2=XORG-WF2-CLR-LC2
340         CALL INDVAL(L,X1-X2+WIND,D,LAMBDA,WIND,FTHICK)
341     ENDIF
342 C
343     Y1=YORG+WC2-WIND4
344     Y2=Y1
345     X3=X1+WIND2

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```
346          Y3=YORG+WC2+D+WIND2
347 C
348 C
349          CALL BOX(X1,Y1,D+WIND+WIND4,WIND,2,IROT,XORG,YORG,ANGLE,LBOT)
350          CALL BOX(X2,Y1,D+WIND+WIND4,WIND,2,IROT,XORG,YORG,ANGLE,LTOP)
351          CALL BOX(X3,Y3,X1-X2+WIND,WIND,3,IROT,XORG,YORG,ANGLE,LBRD)
352 C
353 C   MAKE A VIA
354 C       CALL VIA(X1-WIND2,Y1,IROT,ANGLE,LVIA)
355 C
356 C   ENDIF
357 C
358 C   DETERMINE LENGTH OF TLINE TO CLEAR ALL MATCHING ELEMENTS
359 C       YCL=AMAX1(WC2,YORG-Y3+WIND2,Y3-YORG+WIND2)+WFEED
360 C       YCL=AMAX1(WC1+D+WIND,WC2+D+WIND)+WFEED
361 C
362 C       IF(YCL.GE.YCLR)YCLR=YCL
363 C
364 C       RETURN
365 C       END
366 C
367 C   SUBROUTINE CAP11(WANT,CC,WC,LC,EPSR,THICK)
368 C   THIS SUBROUTINE CALCULATES THE DIMENSIONS OF A METAL FOIL
369 C   CAPACITOR FROM GIVEN MILAR PROPERTIES.  THIS SUBPROGRAM
370 C   DETERMINES THE PARAMETERS OF THE SHUNT-CONNECTED CAPACITORS
371 C   OF TYPE-11 AND RELATED NETWORKS.
372 C
373 C       REAL LC
374 C
375 C       C=CC*1E-12
376 C       TH=THICK*2.54E-5
377 C       A=C*TH/(8.854E-12*EPSR)
378 C       A=A/(.0254**2)
379 C
380 C       WC=WANT
381 C       LC=A/WC
382 C
383 C       IF(LC.GT.2.*WANT)THEN
384 C           WC=2.*WANT
385 C           LC=A/WC
386 C       ENDIF
387 C
388 C       RETURN
389 C       END
390 C
391 C
392 C   SUBROUTINE CAPAA(FL,WID,CC,EPSR,THICK)
393 C   THIS SUBROUTINE CALCULATES THE DIMENSIONS OF A METAL FOIL
394 C   CAPACITOR FROM GIVEN MILAR PROPERTIES.  THIS SUBPROGRAM
395 C   DETERMINES THE PARAMETERS OF THE SHUNT-CONNECTED CAPACITORS
396 C   OF TYPE-11 AND RELATED NETWORKS.
397 C
398 C
399 C       C=CC*1E-12
400 C       TH=THICK*2.54E-5
401 C       A=C*TH/(8.854E-12*EPSR)
402 C       A=A/(.0254**2)
403 C
404 C       WID=A/FL
405 C
406 C       RETURN
407 C       END
408 C
409 C
410 C   REAL FUNCTION LSTRIP(L,W)
411 C   REAL L
412 C
413 C   DATA DELTAX/3E-4/,ERROR/1E-3/
414 C
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415 C STATEMENT FUNCTION FOR INDUCTANCE OF A STRIP.
416     AINDUCT(X,W)=5.08*X*(LOG(2.+X/W)+.5)
417 C
418 C GUESS A VALUE
419     X1=L/20.
420 C
421     10 Y1=L-AINDUCT(X1,W)
422     Y2=L-AINDUCT(X1+DELTAX,W)
423     X2=X1-DELTAX*Y1/(Y2-Y1)
424     IF(ABS(X2-X1).LE.ERROR)THEN
425         LSTRIP=X2
426         RETURN
427     ELSE
428         X1=X2
429         GO TO 10
430     ENDIF
431 C
432     END
433 C
434 C
435 C
436 C ***** C
437 C
438 C             MATCHING NETWORK DESIGN AND LAYOUT
439 C
440 C ***** C
441 C
442     SUBROUTINE NET09(XORG,YORG,L1,C2,C3,LANT,WANT,WFEED,THICK,EPSR,
443     & FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
444 C
445 C THIS SUBROUTINE DRAWS A TYPE-9 NETWORK.
446 C THE TYPE-9 NETWORK IS A HIGH-PASS FORM WITH A CAPACITOR IN SERIES WITH
447 C EACH ANTENNA ELEMENT, A SHUNT CAPACITOR BETWEEN ANTENNAS AND A SHUNT
448 C INDUCTOR ACROSS THE FEEDLINE. L1 IS THE SHUNT INDUCTOR, C2 IS THE
449 C SHUNT INDUCTOR AND C3 IS THE SERIES CAPACITOR.
450 C
451     REAL L1
452     REAL LC,LC2,LANT
453     REAL LAMBDA
454 C
455     DATA LTOP/1/,LBOT/2/,LBRD/3/
456     DATA CLR/.05/
457     DATA WIND/.125/,WMIN/.125/
458 C
459 C DETERMINE THE DIMENSIONS OF THE SERIES CAPACITORS.
460 C
461     CALL CAPVAL(WANT,C3,WC,LC,EPSR,THICK)
462 C
463 C EVALUATE SOME CONSTANTS NEEDED LATER
464     LC2=LC/2.
465     WF2=WFEED/2.
466     XANT=LANT-(CLR+WF2+LC2)
467 C
468 C DRAW THE RIGHT-HAND (TOP LAYER) ANTENNA AND SERIES CAPACITOR.
469 C
470     CALL BOX(XORG,YORG,LC+WF2+CLR,WC,3,IROT,XORG,YORG,ANGLE,LTOP)
471     CALL BOX(XORG+WF2+CLR,YORG,LC,WC,1,IROT,XORG,YORG,ANGLE,LTOP)
472     CALL BOX(XORG+CLR+WF2+LC2,YORG,XANT,WANT,1,IROT,XORG,YORG,
473     & ANGLE,LTOP)
474 C
475 C DRAW THE LEFT-HAND (BOTTOM LAYER) ANTENNA AND SERIES CAPACITOR.
476 C
477     CALL BOX(XORG,YORG,LC+WF2+CLR,WC,1,IROT,XORG,YORG,ANGLE,LBOT)
478     CALL BOX(XORG-WF2-CLR,YORG,LC,WC,3,IROT,XORG,YORG,ANGLE,LBOT)
479     CALL BOX(XORG-CLR-WF2-LC2,YORG,XANT,WANT,3,IROT,XORG,YORG,
480     & ANGLE,LBOT)
481 C
482 C DRAW THE INDUCTORS
483 C

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484 C CALCULATE AND DRAW THE INDUCTOR ACROSS THE FEEDLINE.
485 C
486 C     IF(L1.GE.0.)THEN
487 C         CALL SHUNTL(XORG,YORG,WFEED,WIND,FTHICK,WC,LC,
488 C             &         CLR,L1,LAMBDA,1,IROT,ANGLE,YCL)
489 C     ENDIF
490 C
491 C MAKE A VIA
492 C     CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
493 C
494 C CALCULATE AND DRAW THE CAPACITOR ACROSS THE ANTENNA.
495 C
496 C     IF(C2.GE.0.)THEN
497 C         CALL SHUTC(XORG,YORG,C2,WC,WFEED,WMIN,
498 C             &         THICK,EPSR,IROT,ANGLE,CLR,2,YCLR)
499 C     ENDIF
500 C
501 C MAKE A VIA
502 C     CALL VIA(X1-WIND2,Y1,IROT,ANGLE,LVIA)
503 C
504 C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
505 C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
506 C ALL ELEMENTS IN THE MATCHING NETWORKS.
507 C
508 C     IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
509 C     IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
510 C
511 C     IF(YCL.GE.YCLR)YCLR=YCL
512 C
513 C     RETURN
514 C     END
515 C
516 C
517 C     SUBROUTINE NET10(XORG,YORG,L1,L2,C3,LANT,WANT,WFEED,THICK,EPSR,
518 C         &         FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
519 C
520 C THIS SUBROUTINE DRAWS A TYPE-10 NETWORK.
521 C THE TYPE-10 NETWORK IS A HIGH-PASS FORM WITH A CAPACITOR IN SERIES WITH
522 C EACH ANTENNA ELEMENT AND SHUNT INDUCTORS ACROSS THE ANTENNAS AND
523 C FEEDLINE, RESPECTIVELY. L1 AND L2 ARE THE INDUCTORS ACROSS THE FEEDLINE
524 C AND ANTENNAS, RESPECTIVELY. THE TWO CAPACITORS HAVE VALUE C.
525 C
526 C     REAL L1,L2
527 C     REAL LC,LC2,LANT
528 C     REAL LAMBDA
529 C
530 C     DATA LTOP/1/,LBOT/2/,LBRD/3/
531 C     DATA CLR/.05/
532 C     DATA WIND/.125/
533 C
534 C DETERMINE THE DIMENSIONS OF THE SERIES CAPACITORS.
535 C
536 C     CALL CAPVAL(WANT,C3,WC,LC,EPSR,THICK)
537 C
538 C EVALUATE SOME CONSTANTS NEEDED LATER
539 C     LC2=LC/2.
540 C     WF2=WFEED/2.
541 C     XANT=LANT-(CLR+WF2+LC2)
542 C
543 C DRAW THE RIGHT-HAND (TOP LAYER) ANTENNA AND SERIES CAPACITOR.
544 C
545 C     CALL BOX(XORG,YORG,LC+WF2+CLR,WC,3,IROT,XORG,YORG,ANGLE,LTOP)
546 C     CALL BOX(XORG+WF2+CLR,YORG,LC,WC,1,IROT,XORG,YORG,ANGLE,LTOP)
547 C     CALL BOX(XORG+CLR+WF2+LC2,YORG,XANT,WANT,1,IROT,XORG,YORG,
548 C         &         ANGLE,LTOP)
549 C
550 C DRAW THE LEFT-HAND (BOTTOM LAYER) ANTENNA AND SERIES CAPACITOR.
551 C
552 C     CALL BOX(XORG,YORG,LC+WF2+CLR,WC,1,IROT,XORG,YORG,ANGLE,LBOT)

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553      CALL BOX(XORG-WF2-CLR,YORG,LC,WC,3,IROT,XORG,YORG,ANGLE,LBOT)
554      CALL BOX(XORG-CLR-WF2-LC2,YORG,XANT,WANT,3,IROT,XORG,YORG,
555      &          ANGLE,LBOT)
556 C
557 C DRAW THE INDUCTORS
558 C
559 C CALCULATE AND DRAW THE INDUCTOR ACROSS THE FEEDLINE.
560 C
561      IF(L1.GE.0.)THEN
562          CALL SHUNT1(XORG,YORG,WFEED,WIND,FTHICK,WC,LC,
563          &          CLR,L1,LAMBDA,1,IROT,ANGLE,YCL)
564      ENDIF
565 C
566 C MAKE A VIA
567 C      CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
568 C
569 C CALCULATE AND DRAW THE INDUCTOR ACROSS THE TWO ANTENNAS.
570 C
571      IF(L2.GE.0.)THEN
572          CALL SHUNT1(XORG,YORG,WFEED,WIND,FTHICK,WC,LC,
573          &          CLR,L2,LAMBDA,2,IROT,ANGLE,YCL)
574      ENDIF
575 C
576 C MAKE A VIA
577 C      CALL VIA(X1-WIND2,Y1,IROT,ANGLE,LVIA)
578 C
579 C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
580 C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
581 C ALL ELEMENTS IN THE MATCHING NETWORKS.
582 C
583      IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
584      IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
585 C
586      IF(YCL.GE.YCLR)YCLR=YCL
587 C
588      RETURN
589      END
590 C
591 C
592      SUBROUTINE NET11(XORG,YORG,C1,C2,L3,LANT,WANT,WFEED,THICK,EPSR,
593      &          FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
594 C
595 C THIS SUBROUTINE DRAWS A TYPE-11 NETWORK.
596 C THE TYPE-11 NETWORK IS A LOW-PASS FORM WITH AN INDUCTOR IN SERIES WITH
597 C EACH ANTENNA ELEMENT AND SHUNT CAPACITORS ACROSS THE ANTENNAS AND
598 C FEEDLINE, RESPECTIVELY. C1 AND C2 ARE THE CAPACITORS ACROSS THE FEEDLINE
599 C AND ANTENNAS, RESPECTIVELY. THE TWO INDUCTORS HAVE VALUE L3.
600 C
601      REAL L3,LIND
602      REAL LC,LC2,LANT
603      REAL LAMBDA,LSTRIP
604 C
605      DATA LTOP/1/,LBOT/2/,LBRD/3/
606      DATA CLR/.05/,OL/.05/,WSRIND/.025/,WX/.20/
607 C
608 C DETERMINE THE DIMENSIONS OF THE SERIES INDUCTORS.
609 C
610      NOTUSE=LAMBDA
611 C
612      LIND= LSTRIP(L3,WSRIND)
613 C
614 C GET THE DIMENSIONS OF THE CAPACITORS ACROSS FEED LINE
615 C ONE-HALF OF CAPACITANCE ON EACH SIDE
616 C
617      CALL CAP11(WANT,C1/2.,WC,LC,EPSR,THICK)
618 C
619 C EVALUATE SOME CONSTANTS NEEDED LATER
620      WF2=WFEED/2.
621      XANT=LANT-(LIND+WF2+LC)
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622 C
623 C   DRAW THE RIGHT-HAND (TOP) ANTENNA AND SERIES INDUCTOR.
624 C
625     CALL BOX(XORG+LC+WF2-OL,YORG,LIND+2.*OL,WSRIND,1,IROT,XORG,
626             &   YORG,ANGLE,LTOP)
627     CALL BOX(XORG+LIND+LC+WF2,YORG,XANT,WANT,1,IROT,XORG,YORG,
628             &   ANGLE,LTOP)
629 C
630 C   DRAW THE LEFT-HAND (BOTTOM) ANTENNA AND SERIES INDUCTOR.
631 C
632     CALL BOX(XORG-LC-WF2+OL,YORG,LIND+2.*OL,WSRIND,3,IROT,XORG,
633             &   YORG,ANGLE,LBOT)
634     CALL BOX(XORG-LIND-LC-WF2,YORG,XANT,WANT,3,IROT,XORG,YORG,
635             &   ANGLE,LBOT)
636 C
637 C   DRAW THE CAPACITORS SHUNTING THE FEED LINE.
638 C
639     IF(C1.GT.0.)THEN
640 C
641         CALL BOX(XORG+WF2-OL,YORG,LC+OL,WC,1,IROT,XORG,YORG,
642             &   ANGLE,LTOP)
643         CALL BOX(XORG+WF2-OL,YORG,LC+OL,WC,1,IROT,XORG,YORG,
644             &   ANGLE,LBOT)
645         CALL BOX(XORG-WF2+OL,YORG,LC+OL,WC,3,IROT,XORG,YORG,
646             &   ANGLE,LTOP)
647         CALL BOX(XORG-WF2+OL,YORG,LC+OL,WC,3,IROT,XORG,YORG,
648             &   ANGLE,LBOT)
649 C
650     ENDIF
651 C
652 C
653 C   CALCULATE AND DRAW THE CAPACITOR BETWEEN THE ANTENNAS.
654 C
655     WC2=WC/2.
656     DC=WX+CLR+WC2+WANT/2.-OL
657 C
658     IF(C2.GE.0.)THEN
659 C
660         CALL CAPAA(DC,X,C2,EPSR,THICK)
661 C
662 C   DRAW THE LEFT-HAND PLATE CONNECTED TO THE ANTENNA (BOTTOM SIDE)
663     CALL BOX(XORG-WF2-LC-LIND-X/2.,YORG-WC2-CLR-WX,DC,X,2,IROT,
664             &   XORG,YORG,ANGLE,LBOT)
665 C
666 C   DRAW THE RIGHT-HAND PLATE CONNECTED TO THE ANTENNA (TOP SIDE)
667     CALL BOX(XORG+WF2+LC+LIND+X/2.,YORG-WC2-CLR-WX,DC,X,2,IROT,
668             &   XORG,YORG,ANGLE,LYOP)
669 C
670 C   DRAW THE LEFT-HAND PLATE CONNECTED TO THE CROSSOVER (TOP SIDE).
671     CALL BOX(XORG-WF2-LC-LIND-X/2.,YORG-WC2-CLR-WX,DC,X,2,IROT,
672             &   XORG,YORG,ANGLE,LTOP)
673 C
674 C   DRAW THE CROSS-OVER CONNECTING THE TOP PLATES ON BOTH SIDES
675     CALL BOX(XORG+WF2+LC+LIND+X/2.,YORG-WC2-CLR-WX/2.,
676             &   2.*(WF2+LC+LIND+X/2.),WX,3,IROT,XORG,YORG,ANGLE,LBRD)
677 C
678     ENDIF
679 C
680 C   MAKE A VIA
681     CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
682 C
683 C   KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
684 C   THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
685 C   ALL ELEMENTS IN THE MATCHING NETWORKS.
686 C
687     IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
688     IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
689     YCL=WC2+CLR+WX+WFEED
690     IF(YCL.GT.YCLR)YCLR=YCL

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691 C
692     RETURN
693     END
694 C
695     SUBROUTINE NET12(XORG,YORG,C1,L2,L3,LANT,WANT,WFEED,THICK,EPSR,
696     &    FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
697 C
698 C   THIS SUBROUTINE DRAWS A TYPE-12 NETWORK.
699 C   THE TYPE-12 NETWORK IS A LOW-PASS FORM WITH AN INDUCTOR IN SERIES WITH
700 C   EACH ANTENNA ELEMENT, SHUNT CAPACITOR ACROSS THE FEED LINE AND
701 C   A SHUNT INDUCTOR ACROSS THE TWO ANTENNAS. C1 IS THE CAPACITOR ACROSS
702 C   THE FEEDLINE, L2 IS THE INDUCTOR ACROSS THE ANTENNAS, AND L3 IS THE
703 C   INDUCTOR IN SERIES WITH EACH ANTENNA ELEMENT.
704 C
705     REAL L2,L3,LIND
706     REAL LC,LC2,LANT
707     REAL LAMBDA,LSTRIP
708 C
709     DATA LTOP/1/,LBOT/2/,LBRD/3/
710     DATA CLR/.05/,OL/.05/,WSRIND/.05/,WX/.25/,WIND/.125/
711 C
712 C   DETERMINE THE DIMENSIONS OF THE SERIES INDUCTORS.
713 C
714     NOTUSE=LAMBDA
715 C
716     LIND= LSTRIP(L3,WSRIND)
717 C
718 C   GET THE DIMENSIONS OF THE CAPACITORS ACROSS FEED LINE
719 C   ONE-HALF OF CAPACITANCE ON EACH SIDE
720 C
721     CALL CAP11(WANT,C1/2.,WC,LC,EPSR,THICK)
722 C
723 C   EVALUATE SOME CONSTANTS NEEDED LATER
724     WF2=WFEED/2.
725     XANT=LANT-(LIND+WF2+LC)
726 C
727 C   DRAW THE RIGHT-HAND (TOP) ANTENNA AND SERIES INDUCTOR.
728 C
729     CALL BOX(XORG+LC+WF2-OL,YORG,LIND+2.*OL,WSRIND,1,IROT,XORG,
730     &    YORG,ANGLE,LTOP)
731     CALL BOX(XORG+LIND+LC+WF2,YORG,XANT,WANT,1,IROT,XORG,YORG,
732     &    ANGLE,LTOP)
733 C
734 C   DRAW THE LEFT-HAND (BOTTOM LAYER) ANTENNA AND SERIES INDUCTOR.
735 C
736     CALL BOX(XORG-LC-WF2+OL,YORG,LIND+2.*OL,WSRIND,3,IROT,XORG,
737     &    YORG,ANGLE,LBOT)
738     CALL BOX(XORG-LIND-LC-WF2,YORG,XANT,WANT,3,IROT,XORG,YORG,
739     &    ANGLE,LBOT)
740 C
741 C   DRAW THE CAPACITORS SHUNTING THE FEED LINE.
742 C
743     CALL BOX(XORG+WF2-OL,YORG,LC+OL,WC,1,IROT,XORG,YORG,
744     &    ANGLE,LTOP)
745     CALL BOX(XORG+WF2-OL,YORG,LC+OL,WC,1,IROT,XORG,YORG,
746     &    ANGLE,LBOT)
747     CALL BOX(XORG-WF2+OL,YORG,LC+OL,WC,3,IROT,XORG,YORG,
748     &    ANGLE,LTOP)
749     CALL BOX(XORG-WF2+OL,YORG,LC+OL,WC,3,IROT,XORG,YORG,
750     &    ANGLE,LBOT)
751 C
752 C   CALCULATE AND DRAW THE INDUCTOR BETWEEN THE ANTENNAS.
753 C
754     OW2=WF2+LC+LIND+WIND
755     OW=2.*OW2
756     WC2=WC/2.
757     WANT2=WANT/2.
758     WIND2=WIND/2.
759 C

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760      IF(L2.GT.0.)THEN
761      CALL INDVAL(L2,OW,D,LAMBDA,WIND,FTHICK)
762  C
763      IF(WC2-WANT2.GT.D)THEN
764          D=WC2-WANT2+CLR
765      ENDIF
766  C
767  C
768      CALL BOX(XORG-OW2+WIND2,YORG-WANT2+OL,D+WIND+OL,WIND,4,IROT,
769      &        XORG,YORG,ANGLE,LBOT)
770      CALL BOX(XORG+OW2-WIND2,YORG-WANT2+OL,D+WIND+OL,WIND,4,IROT,
771      &        XORG,YORG,ANGLE,LTOP)
772      CALL BOX(XORG-OW2,YORG-WANT2-D-WIND2,OW,WIND,1,IROT,
773      &        XORG,YORG,ANGLE,LBRD)
774  C
775      ENDIF
776  C
777  C MAKE A VIA
778  C   CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
779  C
780  C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
781  C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
782  C ALL ELEMENTS IN THE MATCHING NETWORKS.
783  C
784      IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
785      IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
786      YCL=WC2+CLR+WX+WFEED
787      IF(YCL.GT.YCLR)YCLR=YCL
788  C
789      RETURN
790      END
791  C
792  C
793      SUBROUTINE NET13(XORG,YORG,C1,L2,C3,LANT,WANT,WFEED,THICK,EPSR,
794      &    FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
795  C
796  C THIS SUBROUTINE DRAWS A TYPE-13 NETWORK.
797  C THE TYPE-13 NETWORK IS A HIGH-PASS FORM WITH A CAPACITOR IN SERIES WITH
798  C EACH ANTENNA ELEMENT, A SHUNT CAPACITOR ACROSS THE FEEDLINE, AND
799  C A SHUNT INDUCTOR BETWEEN ANTENNAS. C1 IS THE CAPACITOR ACROSS THE
800  C FEEDLINE, L2 IS THE INDUCTOR BETWEEN THE ANTENNAS, AND C3 IS
801  C THE CAPACITOR IN SERIES WITH EACH ANTENNA.
802  C
803      REAL L2
804      REAL LC,LC2,LANT
805      REAL LAMBDA
806  C
807      DATA LTOP/1/,LBOT/2/,LBRD/3/
808      DATA CLR/.05/
809      DATA WIND/.125/,WMIN/.125/
810  C
811  C DETERMINE THE DIMENSIONS OF THE SERIES CAPACITORS.
812  C
813      CALL CAPVAL(WANT,C3,WC,LC,EPSR,THICK)
814      YCL=WC/2.+WIND
815  C
816  C EVALUATE SOME CONSTANTS NEEDED LATER
817      LC2=LC/2.
818      WF2=WFEED/2.
819      XANT=LANT-(CLR+WF2+LC2)
820  C
821  C DRAW THE RIGHT-HAND (TOP LAYER) ANTENNA AND SERIES CAPACITOR.
822  C
823      CALL BOX(XORG,YORG,LC+WF2+CLR,WC,3,IROT,XORG,YORG,ANGLE,LTOP)
824      CALL BOX(XORG+WF2+CLR,YORG,LC,WC,1,IROT,XORG,YORG,ANGLE,LTOP)
825      CALL BOX(XORG+CLR+WF2+LC2,YORG,XANT,WANT,1,IROT,XORG,YORG,
826      &        ANGLE,LTOP)
827  C
828  C DRAW THE LEFT-HAND (BOTTOM LAYER) ANTENNA AND SERIES CAPACITOR.

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829 C
830 CALL BOX(XORG,YORG,LC+WF2+CLR,WC,1,IROT,XORG,YORG,ANGLE,LBOT)
831 CALL BOX(XORG-WF2-CLR,YORG,LC,WC,3,IROT,XORG,YORG,ANGLE,LBOT)
832 CALL BOX(XORG-CLR-WF2-LC2,YORG,XANT,WANT,3,IROT,XORG,YORG,
833 & ANGLE,LBOT)
834 C
835 C DRAW THE INDUCTORS
836 C
837 C CALCULATE AND DRAW THE INDUCTOR ACROSS THE ANTENNA.
838 C
839 IF(L2.GE.0.)THEN
840 CALL SHUNT1(XORG,YORG,WFEED,WIND,FTHICK,WC,LC,
841 & CLR,L2,LAMBDA,2,IROT,ANGLE,YCL)
842 ENDIF
843 C
844 C MAKE A VIA
845 C CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
846 C
847 C CALCULATE AND DRAW THE CAPACITOR ACROSS THE FEED LINE.
848 C
849 IF(C1.GE.0.)THEN
850 CALL SHUNT2(XORG,YORG,C1,WC,WFEED,WMIN,
851 & THICK,EPSR,IROT,ANGLE,CLR,1,YCL)
852 ENDIF
853 C
854 C MAKE A VIA
855 C CALL VIA(X1-WIND2,Y1,IROT,ANGLE,LVIA)
856 C
857 C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
858 C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
859 C ALL ELEMENTS IN THE MATCHING NETWORKS.
860 C
861 C WRITE(0,*)'IN NET13; YCL,YCLR: ',YCL,YCLR
862 C
863 IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
864 IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
865 IF(YCL.GE.YCLR)YCLR=YCL
866 C
867 RETURN
868 END
869 C
870 C
871 SUBROUTINE NET14(XORG,YORG,L1,C2,L3,LANT,WANT,WFEED,THICK,EPSR,
872 & FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
873 C
874 C THIS SUBROUTINE DRAWS A TYPE-14 NETWORK.
875 C THE TYPE-14 NETWORK IS A LOW-PASS FORM WITH AN INDUCTOR IN SERIES WITH
876 C EACH ANTENNA ELEMENT, A SHUNT INDUCTOR ACROSS THE FEEDLINE, AND A
877 C SHUNT CAPACITOR ACROSS THE ANTENNAS. THE INDUCTOR ACROSS THE FEEDLINE
878 C HAS VALUE L1, THE CAPACITOR C2 AND THE INDUCTOR IN SERIES WITH EACH
879 C ELEMENT IS L3. IF THE ELEMENT VALUE IS ZERO OR NEGATIVE, SHUNT ELEMENTS
880 C ARE NOT DRAWN.
881 C
882 REAL L1,L3,LIND
883 REAL LC,LC2,LANT
884 REAL LAMBDA,LSTRIP
885 C
886 DATA LTOP/1/,LBOT/2/,LBRD/3/
887 DATA CLR/.05/,OL/.05/,WSRIND/.025/,WX/.20/,WIND/.125/
888 C
889 C IF L1 IS POSITIVE, DRAW THE INDUCTOR SHUNTING THE FEED LINE.
890 IF(L1.GE.0.)THEN
891 C
892 C LOGIC TO DECIDE WIDTH OF FEEDLINE CONNECTION
893 C
894 IF(L1.GT.0..AND.L1.LT.10.)THEN
895 OM2=0.25
896 H=0.25
897 ELSEIF(L1.GE.10..AND.L1.LT.50.)THEN

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898         OW2=0.375
899         H=0.375
900     ELSE
901         OW2=0.75
902         H=0.75
903     ENDIF
904 C
905 C DRAW FEED-LINE CONNECTION
906 C
907     CALL BOX(XORG,YORG,OW2,H,3,IROT,XORG,YORG,
908 &           ANGLE,LBOT)
909     CALL BOX(XORG,YORG,OW2,H,1,IROT,XORG,YORG,
910 &           ANGLE,LTOP)
911 C
912     WIND2=WIND/2.
913     H2=H/2.
914 C
915     CALL INDVAL(L1,2.*OW2,D,LAMBDA,WIND,FTHICK)
916 C
917     CALL BOX(XORG-OW2+WIND2,YORG+H2-OL,D+WIND+OL,WIND,2,IROT,
918 &           XORG,YORG,ANGLE,LBOT)
919     CALL BOX(XORG+OW2-WIND2,YORG+H2-OL,D+WIND+OL,WIND,2,IROT,
920 &           XORG,YORG,ANGLE,LTOP)
921     CALL BOX(XORG-OW2,YORG+H2+D+WIND2,2.*OW2,WIND,1,IROT,
922 &           XORG,YORG,ANGLE,LBRD)
923 C
924 C
925     ENDIF
926 C
927 C DETERMINE THE DIMENSIONS OF THE SERIES INDUCTORS.
928 C
929     LIND= LSTRIP(L3,WSRIND)
930 C
931 C EVALUATE SOME CONSTANTS NEEDED LATER
932     WF2=WFEED/2.
933     XANT=LANT-(LIND+WF2+OW2)
934 C
935 C DRAW THE RIGHT-HAND (TOP) ANTENNA AND SERIES INDUCTOR.
936 C
937     CALL BOX(XORG+OW2+WF2-OL,YORG,LIND+2.*OL,WSRIND,1,IROT,XORG,
938 &           YORG,ANGLE,LTOP)
939     CALL BOX(XORG+LIND+OW2+WF2,YORG,XANT,WANT,1,IROT,XORG,YORG,
940 &           ANGLE,LTOP)
941 C
942 C DRAW THE LEFT-HAND (BOTTOM) ANTENNA AND SERIES INDUCTOR.
943 C
944     CALL BOX(XORG-OW2-WF2+OL,YORG,LIND+2.*OL,WSRIND,3,IROT,XORG,
945 &           YORG,ANGLE,LBOT)
946     CALL BOX(XORG-LIND-OW2-WF2,YORG,XANT,WANT,3,IROT,XORG,YORG,
947 &           ANGLE,LBOT)
948 C
949 C
950 C IF C2 IS POSITIVE, CALCULATE AND DRAW THE CAPACITOR BETWEEN THE ANTENNAS.
951 C
952     IF(C2.GT.0.)THEN
953 C
954         DC=WX+CLR+H2+WANT/2.-OL
955 C
956         CALL CAPAA(DC,X,C2,EPSR,THICK)
957 C
958 C DRAW THE LEFT-HAND PLATE CONNECTED TO THE ANTENNA (BOTTOM SIDE)
959     CALL BOX(XORG-WF2-OW2-LIND-X/2.,YORG-H2-CLR-WX,DC,X,2,IROT,
960 &           XORG,YORG,ANGLE,LBOT)
961 C
962 C DRAW THE RIGHT-HAND PLATE CONNECTED TO THE ANTENNA (TOP SIDE)
963     CALL BOX(XORG+WF2+OW2+LIND+X/2.,YORG-H2-CLR-WX,DC,X,2,IROT,
964 &           XORG,YORG,ANGLE,LTOP)
965 C
966 C DRAW THE LEFT-HAND PLATE CONNECTED TO THE CROSSOVER (TOP SIDE).

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967      CALL BOX(XORG-WF2-OW2-LIND-X/2.,YORG-H2-CLR-WX,DC,X,2,IROT,
968      &          XORG,YORG,ANGLE,LTOP)
969 C
970 C  DRAW THE CROSS-OVER CONNECTING THE TOP PLATES ON BOTH SIDES
971      CALL BOX(XORG+WF2+OW2+LIND+X/2.,YORG-H2-CLR-WX/2.,
972      &          2.*(WF2+OW2+LIND+X/2.),WX,3,IROT,XORG,YORG,ANGLE,LBRD)
973 C
974      ENDIF
975 C
976 C
977 C  MAKE A VIA
978      CALL VIA(X1+WIND2,Y1,IROT,ANGLE,LVIA)
979 C
980 C  KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
981 C  THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
982 C  ALL ELEMENTS IN THE MATCHING NETWORKS.
983 C
984      IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
985      IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
986      YCL=WC2+CLR+WX+WFEED
987      IF(YCL.GT.YCLR)YCLR=YCL
988 C
989      RETURN
990      END
991 C
992 C
993      SUBROUTINE NET15(XORG,YORG,C1,C2,C3,LANT,WANT,WFEED,THICK,EPSR,
994      &      FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
995 C
996 C  Written 10/04/89
997 C  THIS SUBROUTINE DRAWS A TYPE-15 NETWORK.
998 C  THE TYPE-15 NETWORK IS A PI-TYPE NETWORK WITH ONLY CAPACITORS.
999 C  A CAPACITOR IS IN SERIES WITH EACH ANTENNA AND CAPACITORS ARE
1,000 C  CONNECTED ACROSS THE FEEDLINE AND ANTENNAS, RESPECTIVELY.
1,001 C  C1 AND C2 ARE CONNECTED ACROSS THE FEEDLINE AND CAPACITORS, RESPECTIVELY,
1,002 C  WHILE C3 IS THE SERIES CAPACITOR.
1,003 C
1,004      REAL LC,LC2,LANT
1,005      REAL LAMBDA
1,006 C
1,007      DATA LTOP/1/,LBOT/2/,LBRD/3/
1,008      DATA CLR/.05/
1,009      DATA WIND/.125/,WMIN/.125/
1,010 C
1,011 C  DETERMINE THE DIMENSIONS OF THE SERIES CAPACITORS.
1,012 C
1,013      CALL CAPVAL(WANT,C3,WC,LC,EPSR,THICK)
1,014 C
1,015 C  EVALUATE SOME CONSTANTS NEEDED LATER
1,016      LC2=LC/2.
1,017      WF2=WFEED/2.
1,018      XANT=LANT-(CLR+WF2+LC2)
1,019 C
1,020 C  DRAW THE RIGHT-HAND (TOP LAYER) ANTENNA AND SERIES CAPACITOR.
1,021 C
1,022      CALL BOX(XORG,YORG,LC+WF2+CLR,WC,3,IROT,XORG,YORG,ANGLE,LTOP)
1,023      CALL BOX(XORG+WF2+CLR,YORG,LC,WC,1,IROT,XORG,YORG,ANGLE,LTOP)
1,024      CALL BOX(XORG+CLR+WF2+LC2,YORG,XANT,WANT,1,IROT,XORG,YORG,
1,025      &          ANGLE,LTOP)
1,026 C
1,027 C  DRAW THE LEFT-HAND (BOTTOM LAYER) ANTENNA AND SERIES CAPACITOR.
1,028 C
1,029      CALL BOX(XORG,YORG,LC+WF2+CLR,WC,1,IROT,XORG,YORG,ANGLE,LBOT)
1,030      CALL BOX(XORG-WF2-CLR,YORG,LC,WC,3,IROT,XORG,YORG,ANGLE,LBOT)
1,031      CALL BOX(XORG-CLR-WF2-LC2,YORG,XANT,WANT,3,IROT,XORG,YORG,
1,032      &          ANGLE,LBOT)
1,033 C
1,034 C
1,035 C  CALCULATE AND DRAW THE CAPACITOR ACROSS THE FEED LINE.

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1,036 C
1,037     IF(C1.GE.0.)THEN
1,038         CALL SHUNTC(XORG,YORG,C1,WC,WFEED,WMIN,
1,039             &          THICK,EPSR,IROT,ANGLE,CLR,1,YCLR)
1,040     ENDIF
1,041 C
1,042 C MAKE A VIA
1,043 C     CALL VIA(X1-WIND2,Y1,IROT,ANGLE,LVIA)
1,044 C
1,045 C CALCULATE AND DRAW THE CAPACITOR ACROSS THE ANTENNA.
1,046 C
1,047     IF(C2.GE.0.)THEN
1,048         CALL SHUNTC(XORG,YORG,C2,WC,WFEED,WMIN,
1,049             &          THICK,EPSR,IROT,ANGLE,CLR,2,YCLR)
1,050     ENDIF
1,051 C
1,052 C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
1,053 C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
1,054 C ALL ELEMENTS IN THE MATCHING NETWORKS.
1,055 C
1,056     IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
1,057     IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
1,058     IF(YCL.GE.YCLR)YCLR=YCL
1,059 C
1,060     RETURN
1,061     END
1,062 C
1,063 C
1,064     SUBROUTINE NET16(XORG,YORG,L1,L2,L3,LANT,WANT,WFEED,THICK,EPSR,
1,065         &          FTHICK,IROT,ANGLE,YCLR,LAMBDA,ILOC,M,NROW)
1,066 C
1,067 C THIS SUBROUTINE DRAWS A TYPE-16 NETWORK.
1,068 C THE TYPE-16 NETWORK IS A PI-NEWTORK WITH ONLY INDUCTORS.
1,069 C L1 IS THE INDUCTOR ACROSS THE FEEDLINE, L2 IS THE INDUCTOR BETWEEN
1,070 C ANTENNAS, AND L3 IS THE INDUCTOR IN SERIES WITH EACH ANTENNA.
1,071 C IF L1 OR L2 ARE NEGATIVE, THE CORRESPONDING ELEMENT IS NOT DRAWN.
1,072 C
1,073     REAL L1,L2,L3,LIND
1,074     REAL LC,LC2,LANT
1,075     REAL LAMBDA,LSTRIP
1,076 C
1,077     DATA LTOP/1/,LBOT/2/,LBRD/3/
1,078     DATA CLR/.05/,OL/.05/,WSRIND/.025/,WX/.20/,WIND/.125/
1,079 C
1,080 C IF L1 IS POSITIVE, DRAW THE INDUCTOR SHUNTING THE FEED LINE.
1,081     IF(L1.GE.0.)THEN
1,082 C
1,083 C LOGIC TO DECIDE WIDTH OF FEEDLINE CONNECTION
1,084 C
1,085         IF(L1.GT.0..AND.L1.LT.10.)THEN
1,086             OW2=0.25
1,087             H=0.25
1,088         ELSEIF(L1.GE.10..AND.L1.LT.50.)THEN
1,089             OW2=0.375
1,090             H=0.375
1,091         ELSE
1,092             OW2=0.75
1,093             H=0.75
1,094         ENDIF
1,095 C
1,096 C DRAW FEED-LINE CONNECTION
1,097 C
1,098     CALL BOX(XORG,YORG,OW2,H,3,IROT,XORG,YORG,
1,099         &          ANGLE,LBOT)
1,100     CALL BOX(XORG,YORG,OW2,H,1,IROT,XORG,YORG,
1,101         &          ANGLE,LTOP)
1,102 C
1,103     WIND2=WIND/2.
1,104     H2=H/2.

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1,105 C
1,106 CALL INDVAL(L1,2.*OW2,D,LAMBDA,WIND,FTHICK)
1,107 C
1,108 CALL BOX(XORG-OW2+WIND2,YORG+H2-OL,D+WIND+OL,WIND,2,IROT,
1,109 & XORG,YORG,ANGLE,LBOT)
1,110 CALL BOX(XORG+OW2-WIND2,YORG+H2-OL,D+WIND+OL,WIND,2,IROT,
1,111 & XORG,YORG,ANGLE,LTOP)
1,112 CALL BOX(XORG-OW2,YORG+H2+D+WIND2,2.*OW2,WIND,1,IROT,
1,113 & XORG,YORG,ANGLE,LBRD)
1,114 C
1,115 C
1,116 ENDIF
1,117 C
1,118 C DETERMINE THE DIMENSIONS OF THE SERIES INDUCTORS.
1,119 C
1,120 LIND= LSTRIP(L3,WSRIND)
1,121 C
1,122 C EVALUATE SOME CONSTANTS NEEDED LATER
1,123 WF2=WFEED/2.
1,124 XANT=LANT-(LIND+WF2+OW2)
1,125 C
1,126 C DRAW THE RIGHT-HAND (TOP) ANTENNA AND SERIES INDUCTOR.
1,127 C
1,128 CALL BOX(XORG+OW2+WF2-OL,YORG,LIND+2.*OL,WSRIND,1,IROT,XORG,
1,129 & YORG,ANGLE,LTOP)
1,130 CALL BOX(XORG+LIND+OW2+WF2,YORG,XANT,WANT,1,IROT,XORG,YORG,
1,131 & ANGLE,LTOP)
1,132 C
1,133 C DRAW THE LEFT-HAND (BOTTOM) ANTENNA AND SERIES INDUCTOR.
1,134 C
1,135 CALL BOX(XORG-OW2-WF2+OL,YORG,LIND+2.*OL,WSRIND,3,IROT,XORG,
1,136 & YORG,ANGLE,LBOT)
1,137 CALL BOX(XORG-LIND-OW2-WF2,YORG,XANT,WANT,3,IROT,XORG,YORG,
1,138 & ANGLE,LBOT)
1,139 C
1,140 C
1,141 C
1,142 C CALCULATE AND DRAW THE INDUCTOR BETWEEN THE ANTENNAS.
1,143 C
1,144 OW2=WF2+LC+LIND+WIND
1,145 OW=2.*OW2
1,146 WC2=WC/2.
1,147 WANT2=WANT/2.
1,148 WIND2=WIND/2.
1,149 C
1,150 IF(L2.GT.0.)THEN
1,151 CALL INDVAL(L2,OW,D,LAMBDA,WIND,FTHICK)
1,152 C
1,153 IF(WC2-WANT2.GT.D)THEN
1,154 D=WC2-WANT2+CLR
1,155 ENDIF
1,156 C
1,157 C
1,158 CALL BOX(XORG-OW2+WIND2,YORG-WANT2+OL,D+WIND+OL,WIND,4,IROT,
1,159 & XORG,YORG,ANGLE,LBOT)
1,160 CALL BOX(XORG+OW2-WIND2,YORG-WANT2+OL,D+WIND+OL,WIND,4,IROT,
1,161 & XORG,YORG,ANGLE,LTOP)
1,162 CALL BOX(XORG-OW2,YORG-WANT2-D-WIND2,OW,WIND,1,IROT,
1,163 & XORG,YORG,ANGLE,LBRD)
1,164 C
1,165 ENDIF
1,166 C
1,167 C
1,168 C MAKE A VIA
1,169 CALL VIA(X1ZWIND2,Y1,IROT,ANGLE,LVIA)
1,170 C
1,171 C KEEP TRACK OF THE SPACE OCCUPIED BY THE SHUNT INDUCTORS SO
1,172 C THAT THE FEEDLINE EXTENSIONS CAN BE MADE LONG ENOUGH TO CLEAR
1,173 C ALL ELEMENTS IN THE MATCHING NETWORKS.

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1,174 C
1,175 IF(ILOC.EQ.1.AND.M.EQ.NROW.AND.NROW.NE.1)RETURN
1,176 IF(ILOC.EQ.2.AND.M.EQ.1.AND.NROW.NE.1)RETURN
1,177 YCL=WC2+CLR+WX+WFEED
1,178 IF(YCL.GT.YCLR)YCLR=YCL
1,179 C
1,180 RETURN
1,181 END
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